

Building the pre-eminent vertically integrated **Lithium** business in Ontario, Canada

SEYMOUR PROJECT VARIABILITY TESTWORK CONFIRMS HIGH QUALITY SPODUMENE CONCENTRATE PRODUCTION

HIGHLIGHTS

- Metallurgical testwork results validate production of 5.5%-6.0% spodumene concentrate with low impurities and at industry comparable recoveries from a DMS only processing circuit
 - HLS testwork demonstrated production of low iron spodumene concentrates with recoveries in line with previously reported test work
 - DMS testwork produced a Spodumene Concentrate at 6.1% Li₂O, 0.9% Fe₂O₃ and 61.9% Li₂O recovery after application of magnetic separation
- Ore Sorting preliminary test work demonstrated good segregation between spodumene and waste rock can be achieved
- Variability program further extends Seymour orebody knowledge and supports GT1's project development strategy for a simple, DMS only plant flowsheet

Green Technology Metals Limited (ASX: GT1) (GT1 or the Company), a Canadian-focused multi-asset lithium business, is pleased to provide an update on metallurgical testwork undertaken for the Seymour project located in Ontario, Canada.

"The results from ore sorting and variability DMS test work have strengthened our understanding of the Seymour orebody, further reducing risks associated with our flowsheet and project development. The spodumene concentrate grade and lithium recovery achieved are consistent with our previous test work and comparable to some of the world's leading hard rock spodumene lithium projects.

These results confirm the viability of our simple, modular DMS processing facility design for the Seymour Project, supporting ongoing work for our feasibility study."

-GT1 Managing Director, Cameron Henry

Testwork Program Overview

The metallurgical test work program undertaken builds on previously reported test 2022 and 2023 test work programs¹, with the aim to further investigate orebody variability, particularly at lower plant feed grades, as well as establish ore sorting amenability, particularly for gangue rejection in DMS plant feed from lower grade, high dilution ores.

¹ Refer to ASX announcements "DMS test work yield exceptional 71.6% recovery to a high-quality spodumene concentrate grading up to 6.8% Li₂O" dated 15 November 2023. "PEA Delivers strong economics & Seymour mining lease granted" dated 7 December 2023.

Previous test work did not include consideration of mine dilution, whereas testwork performed in this campaign included mine dilution material in testwork composites.

Further, the testwork provides additional required information and detail to support the Seymour project feasibility study, specifically with process flowsheet selection and design to produce a target 5.5% Spodumene Concentrate (**SC**) from the Seymour Project.

The program was developed by GT1 Geological and Metallurgical staff in collaboration with Primero Group Ltd, who have significant expertise in lithium processing, metallurgy, and process plant design. Primero assisted to manage the testwork program and to provide results review and interpretation. Testwork was performed at SGS Lakefield Ltd, Canada, who have extensive experience in performing testwork programs of this nature.

Key components of the testwork program include:

1. Metallurgical Testwork Variability program: comprising testing of three (3) composites prepared from diamond drill core sourced from the North Aubry deposit at Seymour, for the purposes of furthering the understanding of metallurgical response to **HLS** and **DMS** techniques to concentrate spodumene ore.
2. Ore Sorting: two (2) variability composites prepared from drill core material and two (2) composites prepared from bulk ore samples collected from the North Aubry orebody were prepared and investigated for their amenability to commercially available ore sorting techniques for elimination of gangue materials. The composites were tested by Steinert US at their Kentucky, USA facilities.

Ore Sorting

Composite blends were initially prepared at SGS Lakefield, including stage screening to remove fines (between <0.5-1.0" composite dependent), and generate two size fractions at a 3:1 size ratio for ore sorting (coarse -9"/+3", fine -3"/+1"). The composite blends minus fines (<1.0") fraction were sent to the Steinert facility in the USA for Ore sorting testing.

Reference samples from the received composites were scanned by Steinert using a combination sensor sorter taking measurements from four sensors:

- XRT - detection of x-ray attenuation differences
- Laser - laser object and brightness recognition
- Colour - colour camera recognition
- Induction - detection of conductive and magnetic properties

The scan data was used to develop a bespoke separation program with evaluations conducted for all sensors. The most effective sensors for sorting were the laser and XRT. The XRT was used to determine the density of the material to whilst the laser was used as a secondary sensor to get a reading of the laser width of the rocks to distinguish between lithium bearing ore (whiter colour) and waste rocks (darker colour).

The composite selection considered material that may be below LOM average for some periods in the mine plan, with the aim to confirm sufficient lithium upgrade is possible in plant feed to maintain production targets. There was also an opportunity to consider adjustments to the mine cut-off grade. The blends are summarised in Table 1.

For Comp 24-2 and 24-4, a single cut point (0.5"-3") was applied on the ROM samples, yielding respective product and waste fractions, whilst for Comp 24-5 and 24-6, two cut points (3"-9" and 1"-3" respectively) were applied, yielding respective product and waste fractions.

Ore Sorting Results

The results across the suite of tests confirmed that the material was sufficiently liberated to selectively ore sort with mass splits and grades aligning with dilution calculations, from drilling and analytical data.

Composite	Feed Assay Li ₂ O Grade (%)	Feed Assay Fe ₂ O ₃ Grade (%)	Mass Rejection (%)	Product Grade [^] (Li ₂ O)	Product Grade (Fe ₂ O ₃)	Recovery [^] Li ₂ O (%)	Rejection [^] Fe ₂ O ₃ (%)
24-2 (LOM/Low Li, Diln 15%)	0.87	3.91	24.8	1.07	0.94	92.6	81.8
24-4 (LOM/Low Li, Diln 60%)	0.27	9.27	67.1	0.55	2.49	68.5	91.2
24-5 (LOM Li, Diln 15%)*	1.04	2.61	19.5	1.22	2.04	93.8	37.1
24-6 (Low Li, Diln 33%)*	0.29	7.01	31.3	0.46	2.61	88.0	36.6

*Applied Ore Sorting Pass 2 Data

[^]Based on a 50% Coarse, 25% Fines and Ultrafines

Table 1 – Metallurgical Program Ore Sorting Summary

The composites generally achieved a mass split that aligned with the gangue dilution, with exception of 24-6 which was an extreme case of very low contained Li₂O in spodumene mineralogy (other lithium bearing minerals present) and high dilution of waste rock. This material was in a zone that was under investigation for mine plan purposes so tested as mentioned to challenge the status quo.

Composite	Mass Distribution (%)	Ratio Li/ Fe	Assay Li ₂ O Grade (%)	Assay Fe ₂ O ₃ Grade (%)	Distribution Li ₂ O (%)	Distribution Fe ₂ O ₃ (%)
24-2 Head	100	0.22	0.87	3.91	100	100
Fines	74.4	1.18	1.08	0.91	92.0	17.3
Ultra Fines*	100	0.18	0.71	3.96	-	-
24-4 Head	100	0.03	0.27	9.27	100	100
Fines	40.5	0.42	0.62	1.47	60.5	4.1
Ultra Fines*	100	0.05	0.30	6.17	-	-
24-5 Head	100	0.40	1.04	2.61	100	100
Coarse [^]	81.0	1.59	1.34	0.85	93.0	45.5
Fines [^]	59.5	3.94	1.94	0.50	92.2	11.6
Ultra Fines*	100	0.13	0.60	4.71	-	-
24-6 Head	100	0.08	0.29	7.01	100	100
Coarse [^]	64.4	0.14	0.27	2.00	76.9	27.9
Fines [^]	39.1	2.29	1.19	0.52	86.3	4.9
Ultra Fines*	100	0.11	0.45	3.97	-	-

*Ultrafines is Ore Sort Bypass

[^]Coarse and Fines Ore Sorter mass split achieved based on unit feed rate

Table 2 – Ore Sorting Feed Upgrade and Distribution (Individual Streams)

The LOM composite with higher contained iron of 3.91% (Comp 24-2) achieved an 81.8% iron rejection with <10% Li₂O loss and a 25% mass rejection. Lithia grade increased from 0.87% to 1.08%. This was also enhanced by having a very low fines fraction as seen with the grade distribution.

This correlated well with the second LOM sample with 15% dilution (Comp 24-5) and confirms that with ore sorting a nominal 20% of the feed was rejected with less than 10% of the lithium loss, but over 50% of the iron removed. Grades increased from 1.04 to over 1.34% Li_2O with Fe_2O_3 grade reducing from 2.61% to <0.85%.

The low lithium high iron grade composite (Comp 24-4) achieved an upgrade of almost 100% (Li_2O 0.27% to 0.62%) with a 40% mass reporting to final product and 60% of the lithium.

Ore Sorting Conclusions

The conclusions from the test program are:

- Ore Sorting mass splits generally aligned with the dilution ratios applied
- Life of Mine (LOM) material (Comp 24-2) with high iron grade (3.9% Fe_2O_3) achieved a reduction in iron grade of over 80% with less than 10% Li_2O loss and a 25.6% mass reduction.
- The second LOM composite with 2.61% Fe_2O_3 also confirmed with a nominal 20% mass rejection over 50% of the iron was rejected with <10% Li_2O loss.
- High iron does not exclude all ore zones with Li_2O recoveries between 60-86% being achieved, with 40-60% mass rejection, at grades around 0.3% Li_2O (near cut-off grade range), for those samples with a nominal 0.3% Li_2O feed grade and 7-9% Fe_2O_3 grade (Comps 24-4 and 24-6).
- Iron grades were reduced on all samples, as stated, the iron in the ultra-fines still has the biggest impact to the DMS Feed grades. Any reduction in this fraction is advantageous.
- Further testwork on the Ore Sorting products to validate the DMS design is in progress and incomplete at time of reporting.
- As further granularity in the mine plan is developed then integration of the ore sorting technology will be considered.

Variability Testwork

Variability testwork program has been undertaken in two phases between 2023 and 2024. Previous testwork reported in the Company's 2023 PEA² included HLS and DMS testwork, as well as initial flotation testwork that could improve overall recovery. From this, ore processing through a simple, robust DMS flowsheet was identified as a suitable strategy for the project, with opportunity to consider future retreatment of bypassed fines material.

The current testwork program objective was to further the understanding of metallurgical response to **HLS** and **DMS** techniques to concentrate spodumene ore from composite samples representing ore grades within the ore block model and preliminary mine plan, and to assess effects of mine dilution not previously tested.

Composite preparation and Head characterisation

Three composites were prepared for the program as outlined in Table 3. Material selection was based on review of the intended mine plan, available drill-core mass and to include varying amounts of mine dilution to assess recovery performance and ability to produce low iron/impurity concentrates.

Composite	Description	Li_2O (%)	Fe_2O_3 (%)	SiO_2 (%)	Al_2O_3 (%)	MgO (%)	CaO (%)	Na_2O (%)	K_2O (%)
24-2	Below design feed grade with high iron dilution	0.84	3.58	67.1	15.8	1.65	3.24	3.70	1.98

² Refer to ASX announcement "PEA Delivers strong economics & Seymour mining lease granted" dated 7 December 2023.

24-7	Low Li ₂ O Grade, testing near approx. mine cut-off grade*	0.39	2.61	68.4	15.5	1.35	2.25	3.74	2.72
24-8	LOM design feed grade	1.05	2.83	68.7	15.7	1.38	2.78	3.22	2.53

Table 3 – Metallurgical Program Composite Summary & Sample assays

Head samples of Comp 24-2, 24-7, and 24-8 were submitted for Semi-Quantitative XRD analysis, with results shown in Table 4.

Mineral	Composition	Comp 24-2	Comp 24-7	Comp 24-8
Albite	NaAlSi ₃ O ₈	31.9	33.1	27.1
Quartz	SiO ₂	23.4	27.8	28.6
Microcline	KAlSi ₃ O ₈	9.3	7.5	10.2
Muscovite	KAl ₂ (AlSi ₃ O ₁₀)(OH) ₂	7.2	10.8	8.0
Spodumene	LiAlSi ₂ O ₆	9.0	4.5	12.1
Magnesiohornblende	Ca ₂ (Mg,Fe) ₅ Si ₈ O ₂₂ (OH) ₂	8.7	7.9	7.1
Epidote	Ca ₂ (Al,Fe)Al ₂ O(SiO ₄)(Si ₂ O ₇)(OH)	3.5	2.7	3.0
Holmquistite	Li ₂ (Mg,Fe) ₃ (Al,Fe ³⁺) ₂ Si ₈ O ₂₂ (OH) ₂	3.9	3.2	1.0
Diopside	CaMgSi ₂ O ₆	1.6	1.4	1.8
Calcite	CaCO ₃	0.9	0.4	0.7
Clinochlore	(Fe,Mg) ₅ Al(Si ₃ Al)O ₁₀ (OH) ₈	0.5	0.6	0.4
TOTAL		100	100	100

Table 4 – Semi-Quantitative XRD Results

The main lithium-bearing mineral is Spodumene ranging from 4.5% to 12.1%. The results show the lithium based minerals are predominantly Spodumene and Holmquistite.. Major gangue minerals were albite (27.1-33.1%) and quartz (23.4-28.6%) with moderate levels of microcline, muscovite and magnesiohornblende. There was no evidence of Petalite which is less conducive to DMS separation, and generally impacts lithium recovery

Grindability Testwork

Grindability testwork was performed on Comps 24-7 and 24-8, with the results (Table 5) showing that they were generally classified as medium abrasive as defined by the abrasion index (Ai).

Composite	Ai (g)	Classification
24-7	0.265	Medium
24-8	0.263	Medium

Table 5 – Grindability testwork results for Comps 24-7 and 24-8

HLS Testwork

HLS Testing was performed on each of the three composites 24-2, 24-7, and 24-8, with samples crushed to --9.5 mm top size and screened into two size fractions, nominally -9.5/+3.3mm and -3.3/0.85mm, with the -0.85 mm fraction removed prior to HLS testing. Magnetic separation also performed on HLS sinks (SG 2.85-3.00).

HLS results for SC6 and interpolated for SC5.5 are reported in Table 6 show good separation of spodumene and gangue minerals and ability to remove a large portion of contained Fe₂O₃, whilst achieving SC6 grade at recoveries similar to those achieved in previously testwork on the North Aubry Deposit.

Composite	Feed Assay Li ₂ O Grade (%)	Feed Assay Fe ₂ O ₃ Grade (%)	Fe ₂ O ₃ % Assay in SC6	Fe ₂ O ₃ Assay in SC5.5	HLS Recovery (SC6)	HLS Recovery (SC5.5)
24-2 (High dilution)	0.84	3.58	1.21	1.39	57.9%	60.5%
24-7 (Low Li₂O Grade)	0.39	2.61	1.39	1.64	29.9%	34.3%
24-8 (LOM)	1.05	2.83	1.26	1.5	71.3%	73.1%

Table 6 – HLS Test Results on Variability Composites 24-2, 24-7, and 24-8

Whilst the low-grade composite 24-7 recoveries are low they are in line with those previously predicted and the sample is likely to be near to the expected mine cut-off grade being assessed in the project feasibility mine design.

Magnetic Separation Testwork

The HLS Sinks were upgraded via magnetic separation work. The weight distribution of magnetic rejects range around 16.1-19.3% of the feed (Table 7).

Stream/Parameter		24-2		24-7		24-8	
		Non_Mag Mass (%)	Magnetic Mass (%)	Non Mag Mass (%)	Magnetic Mass (%)	Non Mag Mass (%)	Magnetic Mass (%)
HLS Sinks	3.00SG	6.0	14.6	8.3	13.5	1.7	11.2
HLS Sinks	2.95SG	0.6	1.7	0.6	1.0	0.1	1.7
HLS Sinks	2.90SG	0.5	1.6	0.5	0.5	0.2	1.3
HLS Sinks	2.85SG	0.6	1.4	1.0	1.2	0.3	2.4
HLS Floats - Mids	2.60-2.80SG	44.9		42.5		54.8	
HLS Floats	<2.60	7.8		14.8		10.9	
Bypass Fraction	-0.85mm	20.3		16.2		15.4	

Table 7 – Magnetic Separation results on composite samples

Mica Reflux Classifier Test

Mica Reflux Classifier tests were conducted on the -3/0.85mm fraction of Composite 24-8 DMS Feed. The Mica Reflux classification testwork demonstrates that particles containing lower amounts of lithium were removed, leading to a 5% reduction in upgrade ratio for Potassium/Iron/Mg while Li was increased by 1%. This indicates that mica can be removed within range of design if this technology is employed within the plant flowsheet.

DMS Testwork

The test program undertaken by SGS utilised their DMS pilot facility which more closely replicates DMS cyclone sizes used in operational facilities. The closed loop arrangement allows the unit to be set-up to reach SG cut-point targets, prior to the feed addition. Feed is then fed a suitable rate. The floats and sinks report to the respective section of a dewatering screen and the media is washed off and sample material collected, for metallurgical accounting.

This is repeated as necessary to align with the proposed flowsheet design, i.e. include any middling generation etc

There is also both a wet and dry magnetic unit in place to perform magnetic separation and achieve the final upgrade as generally considered in DMS flowsheets. For this program the dry magnets were used.

The variability program flowsheet is shown in Figure 1, together with the test apparatus.

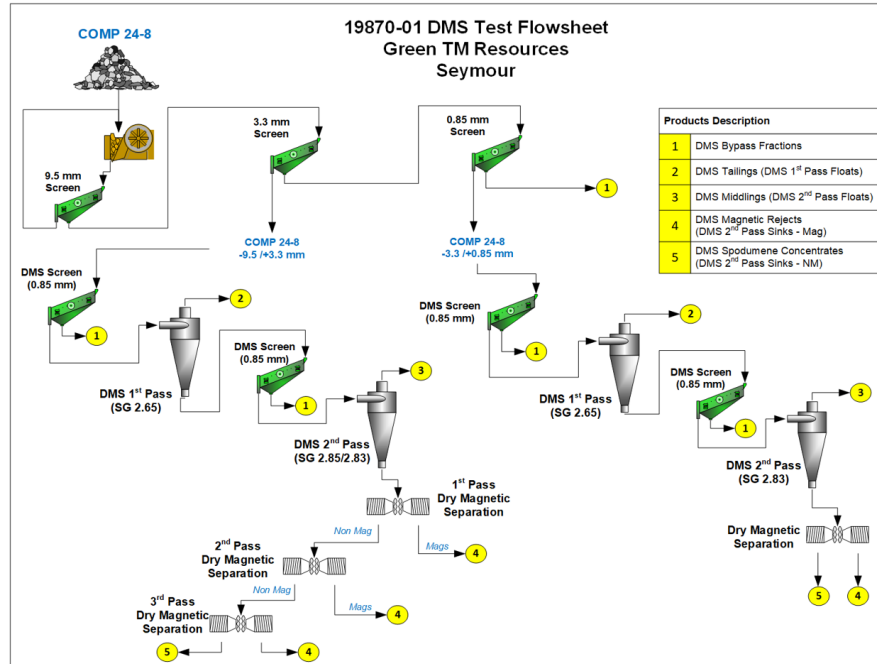


Figure 1 - Variability Program DMS Flowsheet and Laboratory configuration

DMS testwork was performed on Composite 24-8 (Life of Mine bulk composite), including magnetic separation, and performed separately on coarse (-9.5/+3.3 mm) and fine (-3.3/+0.85 mm) fractions in two passes. DMS 1st pass of both coarse and fine fractions were performed at an SG cut of 2.65, whilst DMS 2nd pass of the coarse fraction was performed with an SG cut of 2.85 on the first 10-minute run then continued with an SG cut of 2.83 for the remaining 45-minute run. Finally, the 2nd pass of the DMS fine fraction was performed with an SG cut of 2.83 on the entire 14-minute run.

Magnetic separation was then performed on DMS 2nd pass sink products of each coarse and fine fraction.

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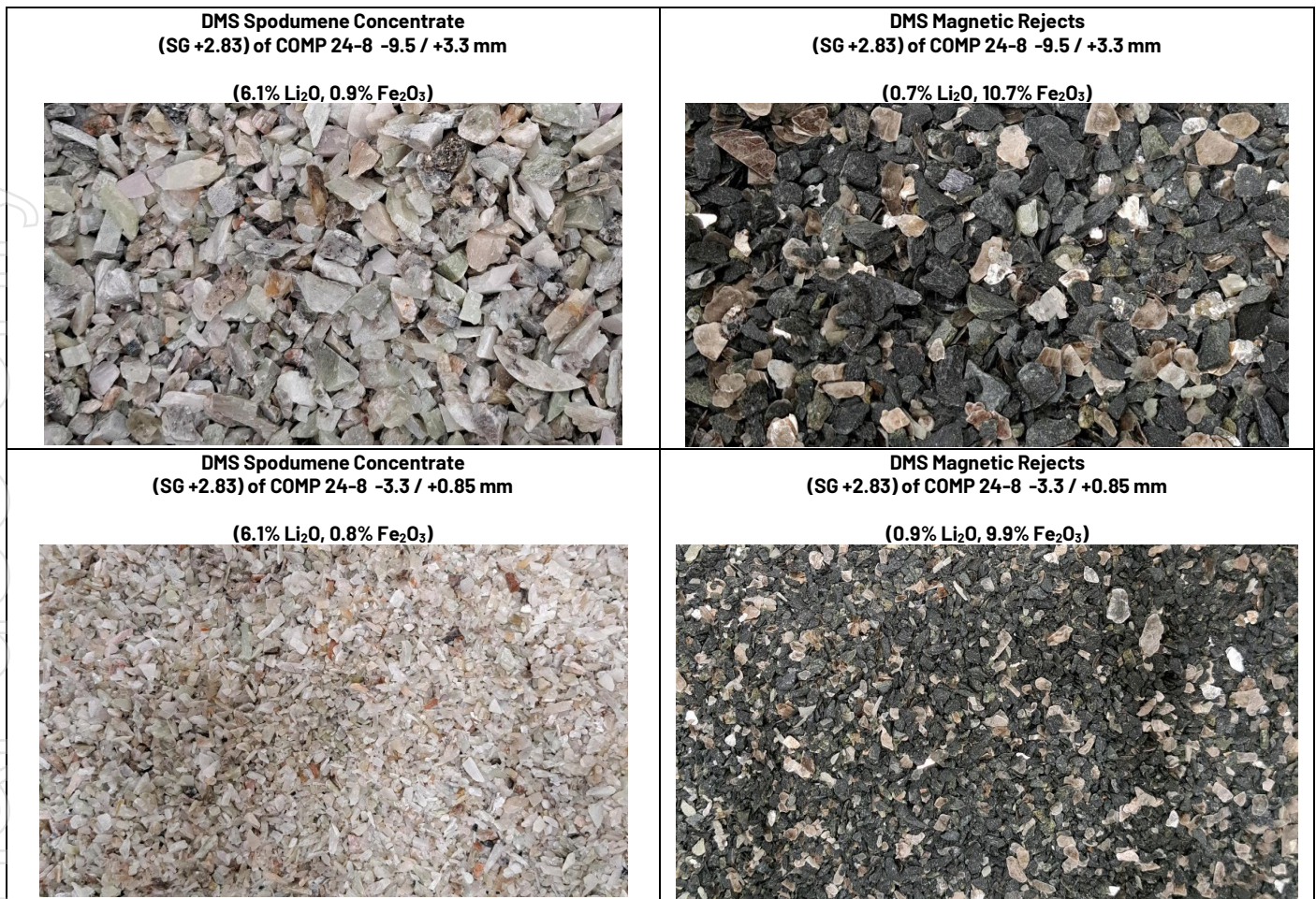


Figure 2 – Comp 24-8 2nd Pass Sinks pre and post magnetic separation

DMS testing results (Table 8) show that a 6.1% Li₂O concentrate with low impurities at 0.9% Fe₂O₃ (after magnetic separation) could be produced at a global lithium recovery of 61.9%.

This result was 9% lower than the HLS result at the similar 6.1% Li₂O grade (Table 6), mainly due to higher lithium loss to the magnetic rejects but similar to HLS/DMS recovery comparisons seen in previous testwork. It however demonstrates the ability produce a low impurity spodumene concentrate with recoveries on par with other global hard rock spodumene Lithium projects.

	Products	DMS SG Cut	Material SG	Weight	Assay (%)		Distribution (%)	
					Li ₂ O	Fe ₂ O ₃	Li ₂ O	Fe ₂ O ₃
		(g/cm ³)	(g/cm ³)	(%)				
Combined (-9.5mm)	DMS Spodumene Concentrate	+2.83 & +2.85	3.06	9.6	6.10	0.93	61.9	3.1
	DMS Magnetic Reject		3.05	18.8	0.77	10.6	15.2	69.4
	DMS Middlings	-2.84 + 2.65	2.69	21.7	0.51	1.27	11.7	9.6
	DMS Tailings	-2.65	2.62	36.8	0.057	0.29	2.2	3.8
-0.85 mm	DMS Bypass Fraction	-0.85mm	-	13.1	0.64	3.09	8.9	14.1
	Head Calculation				0.95	2.86	100	100
	Head Assay				1.05	2.83		

Table 8 –DMS (with magnetic separation) Test Results for Comp 24-8

The final recovery results from the HLS and DMS work in this program are presented in Figure 3 and are compared to testwork results reported previously in the 2023 PEA and a modelled predicted recovery curve for Seymour.

Seymour 2024 Recovery Curve

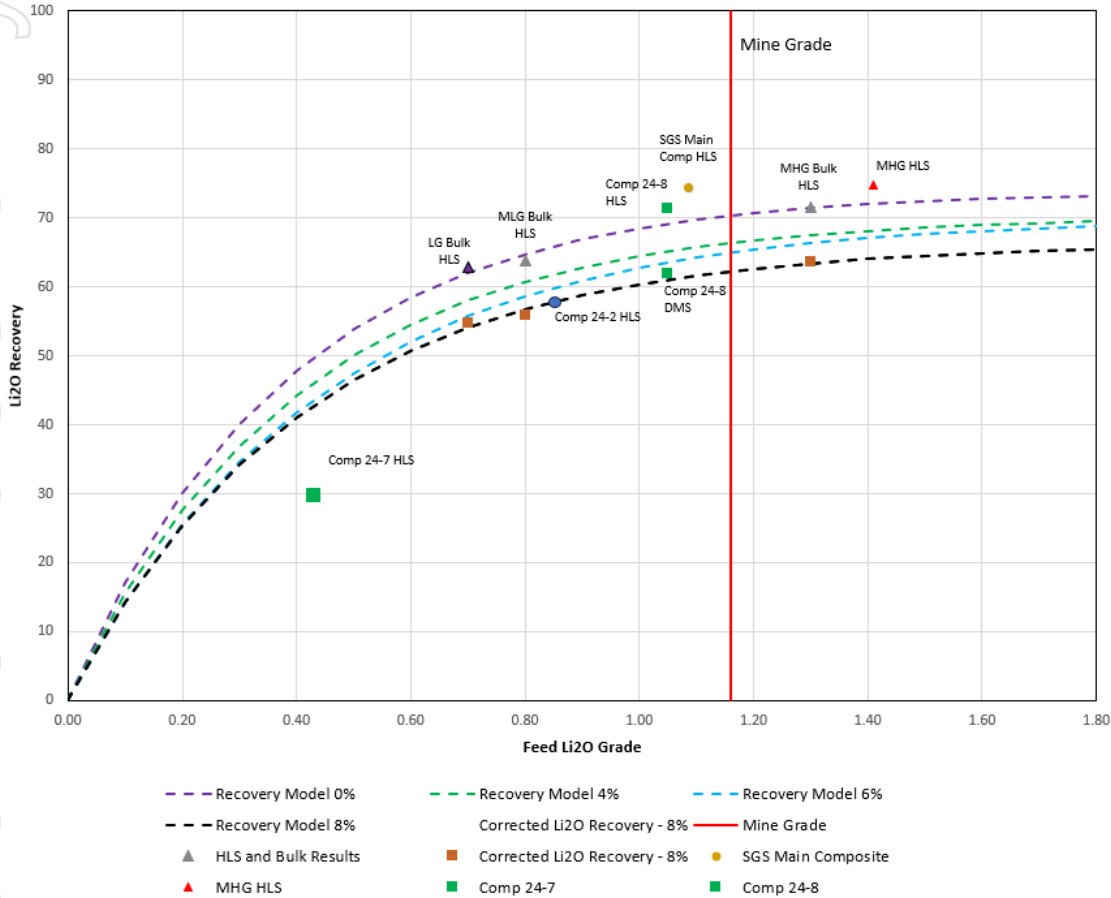


Figure 3 - Comparison of DMS/HLS results (with magnetic separation) for SC6 and modelled recovery curve for Seymour

Conclusions

The positive results of the variability testwork program confirm metallurgical performance comparable with that previously seen in testing programmes for North Aubry Ore deposit, confirming that the proposed plant DMS flowsheet incorporating two-stage coarse and fine DMS can be implemented.

Preliminary ore sorting results show good separation of gangue materials and potential for inclusion in the flowsheet to enable processing of either higher spodumene grade or iron grade feed materials, above the current LOM average.

Further work

The company is currently completing outstanding laboratory tests including:

- HLS testing & magnetic separation on DMS Middling's of -9.5/+3.3 mm Coarse Fraction Feed after crushing to -3.3/+0.85 mm
- HLS tests on a new composite being made from Ore Sorting Accepts materials to verify recovery performance.
- Gravity separation tests for tantalum recovery on DMS magnetic fine rejects (-3.3/+0.85 mm) as a future opportunity for project value addition.
- Thickening and filtration test work for the purposes of sizing process equipment for the Seymour plant flowsheet.

Indigenous Partner Acknowledgement

We would like to say Gchi Miigwech to our Indigenous partners. GT1 appreciates the opportunity to work in the Traditional Territory and remains committed to the recognition and respect of those who have lived, travelled, and gathered on the lands since time immemorial. Green Technology Metals is committed to stewarding Indigenous heritage and remains committed to building, fostering, and encouraging a respectful relationship with Indigenous Peoples based upon principles of mutual trust, respect, reciprocity, and collaboration in the spirit of reconciliation.

This announcement was authorised for release by the Board of Directors

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APPENDIX A: IMPORTANT NOTICES

Competent Person's Statements

The information in this report relating to Metallurgical results is based on information reviewed by Mr Andrew Siemon (Member AusIMM). Mr Siemon has sufficient experience which is relevant to the treatment of the deposit(s) under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined by the 2012 Edition of the Australasian Code for reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr Siemon consents to the inclusion of the data in the form and context in which it appears in this release. Mr Siemon is the Principal Process Metallurgist of the Consulting Company and does not hold securities in the Company.

No new information

Except where explicitly stated, this announcement contains references to prior exploration results, all of which have been cross-referenced to previous market announcements made by the Company. The Company confirms that it is not aware of any new information or data that materially affects the information included in the relevant market announcements.

The information in this report relating to the Mineral Resource estimate for the Seymour Project is extracted from the Company's ASX announcement dated 21 November 2023. GT1 confirms that it is not aware of any new information or data that materially affects the information included in the original announcement and that all material assumptions and technical parameters underpinning the Mineral Resource estimate continue to apply.

The information in this report relating to the Mineral Resource estimate for the Root Project is extracted from the Company's ASX announcements dated 18 October 2023. GT1 confirms that it is not aware of any new information or data that materially affects the information included in the original announcement and that all material assumptions and technical parameters underpinning the Mineral Resource estimate continue to apply.

Forward Looking Statements

Certain information in this document refers to the intentions of Green Technology Metals Limited (ASX: GT1), however these are not intended to be forecasts, forward looking statements or statements about the future matters for the purposes of the Corporations Act or any other applicable law. Statements regarding plans with respect to GT1's projects are forward looking statements and can generally be identified by the use of words such as 'project', 'foresee', 'plan', 'expect', 'aim', 'intend', 'anticipate', 'believe', 'estimate', 'may', 'should', 'will' or similar expressions. There can be no assurance that the GT1's plans for its projects will proceed as expected and there can be no assurance of future events which are subject to risk,

uncertainties and other actions that may cause GT1's actual results, performance or achievements to differ from those referred to in this document. While the information contained in this document has been prepared in good faith, there can be given no assurance or guarantee that the occurrence of these events referred to in the document will occur as contemplated. Accordingly, to the maximum extent permitted by law, GT1 and any of its affiliates and their directors, officers, employees, agents and advisors disclaim any liability whether direct or indirect, express or limited, contractual, tortious, statutory or otherwise, in respect of, the accuracy, reliability or completeness of the information in this document, or likelihood of fulfilment of any forward-looking statement or any event or results expressed or implied in any forward-looking statement; and do not make any representation or warranty, express or implied, as to the accuracy, reliability or completeness of the information in this document, or likelihood of fulfilment of any forward-looking statement or any event or results expressed or implied in any forward-looking statement; and disclaim all responsibility and liability for these forward-looking statements (including, without limitation, liability for negligence).

Green Technology Metals (ASX:GT1)

GT1 is a North American-focused lithium exploration and development business with a current global Mineral Resource estimate of 24.9Mt at 1.13% Li₂O.

Project	Tonnes (Mt)	Li ₂ O (%)
Root Project		
<i>Root Bay</i>		
Indicated	9.4	1.30
Inferred	0.7	1.14
<i>McCombe</i>		
Inferred	4.5	1.01
Total	14.6	1.21
Seymour Project		
<i>North Aubry</i>		
Indicated	6.1	1.25
Inferred	2.1	0.8
<i>South Aubry</i>		
Inferred	2.0	0.6
Total	10.3	1.03
Combined Total	24.9	1.13

The Company's main 100% owned Ontario lithium projects comprise high-grade, hard rock spodumene assets (Seymour, Root, Junior and Wisa) and lithium exploration claims (Allison, Falcon, Gathering, Pennock and Superb) located on highly prospective Archean Greenstone tenure in north-west Ontario, Canada. All sites are proximate to excellent existing infrastructure (including clean hydro power generation and transmission facilities), readily accessible by road, and with nearby rail delivering transport optionality. Targeted exploration across all three projects delivers outstanding potential to grow resources rapidly and substantially.



For full details of the Seymour Mineral Resource estimate, see GT1 ASX release dated 21 November 2023, *Seymour Resource Confidence Increased - Amended*. For full details of the Root Mineral Resource estimate, see GT1 ASX release 18 October 2023, *Significant resource and confidence level increase at Root, Global Resource Inventory now at 24.5Mt*. The Company confirms that it is not aware of any new information or data that materially affects the information in that release and that the material assumptions and technical parameters underpinning this estimate continue to apply and have not materially change

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APPENDIX A: JORC CODE, 2012 EDITION – Table 1 Report

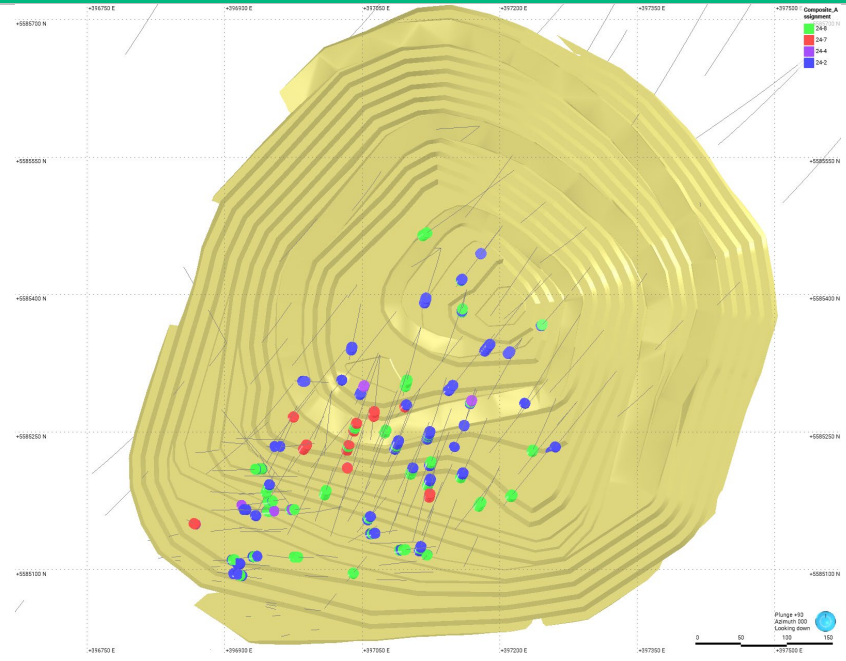
JORC Code, 2012 Edition – Table 1 report template

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. 	<p>No drilling is reported in this release.</p> <p>Metallurgy</p> <p>Metallurgical samples (24-2, 24-4, 24-7 and 24-8) were extracted from the North Aubry deposit within a USD2500 pit design from 65 historic and GT1 drill hole ¼ diamond core reserves for 655m.</p> <p>Drilling methodology aligned with previous drilling practices which are considered standard.</p> <p>Head assays were back calculated post testing and compared with the head sample submitted, with the lithium and iron grades within suitable tolerance.</p> <p>Ore Sorting</p> <p>Ore Sorting samples were obtained as follows:</p> <p>(i) samples from two composites 24-2 and 24-4 prepared as outlined above, and</p> <p>(ii) samples for two composites 24-5 and 24-6 that were extracted from material obtained from trench sampling, which is considered suitable for representative bulk sample testwork. The trenches (Trench Ids: GTTR-23-01, GTTR-23-10, GTTR-23-11, GTTR-23-12) were located within the mine pit shell where the primary outcrop existed, and incorporated sufficient host rock for dilution impacts to be investigated. Over 80 tonne was collected from which two 700kg composites were generated, on a weighted for size distribution based on the crushing model.</p> <p>The 4 composites above were prepared by SGS Lakefield for Ore Sorting with a coarse (-9/+3") and a fine (-3/+1") fraction for each.</p> <p>Head assays were back calculated post testing and compared with the head sample submitted, generally the lithium grade was within tolerance, the iron grades had some variability due to the coarse material size and the significant variability between the ore and host material.</p> <p>The -1" fraction was then removed and retained at SGS, whilst the ore sorting samples were sent to Steinert USA. The samples were scanned by Steinert using a combination sensor sorter testing different sorting techniques, with laser and XRT proving the most effective. Li₂O product grades increased, and iron grades reduced in line with ore sorter upgrade and mass rejection predictions and aligned with dilution ratios applied.</p>

Criteria	JORC Code explanation	Commentary
Drilling techniques	<ul style="list-style-type: none"> Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). 	No drilling is reported in this release.
Drill sample recovery	<ul style="list-style-type: none"> Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	No drilling is reported in this release.
Logging	<ul style="list-style-type: none"> Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged. 	No drilling is reported in this release.
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. Whether sample sizes are appropriate to the grain size of the material being sampled. 	No drilling is reported in this release.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established. 	<p>For metallurgical testwork:</p> <ul style="list-style-type: none"> Test work program was conducted at SGS Lakefield Laboratories Ltd, a reputable mineral processing laboratory, who has stringent analytical structures. Analytical reconciliation for tests were with acceptable tolerances for the material tested. Test flowsheet reflected the proposed commercial design all material was stage crushed to -10 mm and screened at 6.3 mm and 0.85 mm, generating a coarse (-10 to 6.3 mm) and fine (-6.3 to 0.85 mm) size fraction for gravity separation and a fines bypass fraction (-0.85 mm) which reported to tailings. Two-stage gravity separation was performed at a primary specific gravity (SG) of 2.65 and secondary SG of 2.90. Middlings are material which sinks at SG 2.65 but floats at SG 2.90 and may contain significant lithium content; the coarse middlings were re-crushed to -6.3 mm to improve liberation. The re-crushed middlings were subsequently screened at 0.85 mm for fines bypass and with the plus size fraction being passed through two-stage gravity separation again, to reflect the proposed flowsheet. The coarse size fractions were processed using a pilot scale DMS plant, as per noted flowsheet.

Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	<ul style="list-style-type: none"> ▪ <i>The verification of significant intersections by either independent or alternative company personnel.</i> ▪ <i>The use of twinned holes.</i> ▪ <i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i> ▪ <i>Discuss any adjustment to assay data.</i> 	<ul style="list-style-type: none"> ▪ However, the fine size fractions and the entirety of the LG composite masses were insufficient to use the pilot scale DMS plant, therefore bulk HLS testing was used, for interpreting the potential lithium recovery, with a discount applied. ▪ The majority of laboratory assay results have been sourced directly from the laboratory and the laboratory file directly imported into GT1's SQL database. ▪ All recent north seeking gyroscope surveys are uploaded directly from the survey tool output file and visually validated. ▪ Geological logs and supporting data are uploaded directly to the database using custom built importers to ensure no chance of typographical errors. ▪ No adjustment to laboratory assay data was made.
Location of data points	<ul style="list-style-type: none"> ▪ <i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i> ▪ <i>Specification of the grid system used.</i> ▪ <i>Quality and adequacy of topographic control.</i> 	<ul style="list-style-type: none"> ▪ A GPS reading was taken for each sample location using UTM NAD83 Zone16 (for Seymour); waypoint averaging or dGPS was performed when possible. ▪ The project area was flown using LIDAR equipment in October 2021 by KBM Resources Group Inc. from Thunder Bay using a Riegl 680i LiDAR system, coupled to a Applanix POSAV 510 positioning system. The topographic mapping produced is extremely accurate and well suited for resource modelling. ▪ All drilling collars coordinates were compared to the Lidar elevation data to ensure no erroneous coordinates were present in the database. Some collar RL's were adjusted to the Lidar elevation where they differed by more than 3m. GT1 employed a calibrated Reflex SprintIQ North Seeking Gyroscopic tool on all 2021 and 2022 drill holes and surveyed the holes in their entirety with readings downhole every 5m. North Seeking gyroscopes have a typical azimuth accuracy of +/-0.75 degrees and +/-0.15 degrees for dip. <p>Metallurgy</p> <p>Location of the North Aubry metallurgical samples coloured by assigned ore type within a USD2500 pit design:</p>

Criteria	JORC Code explanation	Commentary
		
Data spacing and distribution	<ul style="list-style-type: none"> ▪ Data spacing for reporting of Exploration Results. ▪ Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. ▪ Whether sample compositing has been applied. 	Metallurgy <ul style="list-style-type: none"> ▪ All available historic and more recent GT1 drill core was used to provide metallurgical testwork samples. The samples were distributed roughly on a 50m SE x 100m NW grid with closer spaced shallower samples.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> ▪ Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. ▪ If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	<ul style="list-style-type: none"> ▪ GT1 drill samples were drilled close to perpendicular to the strike of the pegmatite unit and sampled the entire length of the pegmatite as well including several metres into the mafic country rock either side of the pegmatite.
Sample security	<ul style="list-style-type: none"> ▪ The measures taken to ensure sample security. 	<ul style="list-style-type: none"> ▪ All core and samples were supervised and secured in a locked vehicle, warehouse, or container until delivered to Actlabs in Thunder Bay for cutting, preparation and analysis. Metallurgy <ul style="list-style-type: none"> ▪ Historic and GT1 ½ core was either cut in GT1's Thunder Bay core storage facility or delivered under GT1 supervision to Diamond Daves', Thunder Bay, a core cutting contractor. Samples were ¼ core cut using a diamond saw and composited into nominally 1m lengths retained in numbered calico bags themselves grouped into labelled poly weave bags for delivery to the metallurgical laboratory.

Criteria	JORC Code explanation	Commentary
Audits or reviews	<ul style="list-style-type: none"> The results of any audits or reviews of sampling techniques and data. 	No drilling is reported in this release.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

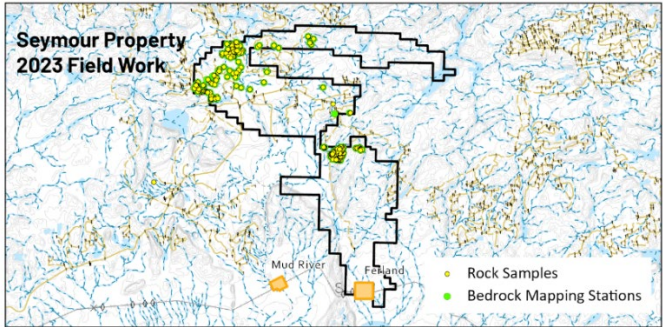
Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area. 	<ul style="list-style-type: none"> Green Technology Metals (ASX:GT1) owns 100% interest in the Ontario Lithium Projects (Seymour, Junior, Root and Wisa). Seymour Lithium Asset consists of 744 Cell Claims (Exploration Licences) with a total claim area of 15,140 ha. GT1 have acquired several additional claims around Seymour, Root, Allison Lake and Landore since listing on the ASX. As of the effective date of this report, all subject lands are in good standing and all claims are currently held 100% by Green TM Resources (Canada) Ltd (a subsidiary of Green Technology Metals Ltd). As the claims are on Crown Land, surface access is guaranteed under the Mining Act of Ontario. All Cell Claims are in good standing An Active Exploration Permit exists over the Seymour Lithium Assets An Exploration Agreement is current with the Whitesand First Nation who are supportive of GT1 exploration activities
Exploration done by other parties	<ul style="list-style-type: none"> Acknowledgment and appraisal of exploration by other parties. 	<ul style="list-style-type: none"> Regional exploration for lithium deposits commenced in the 1950's. In 1957, local prospector, Mr Nelson Aubry, discovered the North Aubry and the South Aubry pegmatites. Geological mapping by the Ontario Department of Mines commenced in 1959 and was completed in 1962 (Pye, 1968), with the publication of "Map 2100 Crescent Lake Area" in 1965. From the late 1950's to 2002, exploration by the Ontario Department of Mines was generally restricted to geological mapping and surface sampling, although some minor drilling was completed to test the North Aubry pegmatite in late 1957 (Rees, 2011). In 2001, Linear Resources Inc. ("Linear Resources") obtained the Seymour Lake Project with an initial focus on the project's tantalum potential. In 2002, a 23-diamond drill-hole campaign was completed at North Aubry, and a further 8 diamond drill-holes at South Aubry. In 2008, Linear Resources completed a regional soil-sampling program which resulted in the identification of a number soil geochemical anomalies. Based on these anomalies, another drilling campaign (completed in 2009), with 12 diamond drill-holes at North Aubry, 2 diamond drill-holes at South Aubry, and further 5 diamond drill-holes peripheral to the Aubry prospects designed to test the main 2008 soil geochemical anomalies. Little work was undertaken between 2010 and 2016 until Ardiden acquired the project from Linear Resources in 2016. Further drilling was carried out by Ardiden between 2017 and 2018 resulting in the completion of an updated mineral resource estimate of the Aubry pegmatites in 2018. Ground Penetrating Radar (GPR) was also undertaken by Ardiden in 2018 to test any further exploration potential beyond the current Aubry pegmatite delineating numerous targets.
Geology	<ul style="list-style-type: none"> Deposit type, geological setting and style of mineralisation. 	<ul style="list-style-type: none"> Regional Geology: The general geological setting of the Seymour Lithium Asset consists of the Precambrian Canadian Shield that underlies approximately 60% of Ontario. The Shield can be divided into three major geological and physiographic regions, from the oldest in the northwest to the

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		<p>youngest in the southeast.</p> <ul style="list-style-type: none"> ▪ Local Geology: The Seymour Lithium Asset is located within the eastern part of the Wabigoon Subprovince, near the boundary with the English River Subprovince to the north. These subprovinces are part of the Superior Craton, comprised mainly of Archaean rocks but also containing some Mesoproterozoic rocks such as the Nipigon Diabase. ▪ Bedrock Geology: The bedrock is best exposed along the flanks of steep-sided valleys scoured by glaciers during the recent ice ages. The exposed bedrock is commonly metamorphosed basaltic rock, of which some varieties have well-preserved pillows that have been intensely flattened in areas of high tectonic strain. Intercalated between layers of basalt are lesser amounts of schists derived from sedimentary rocks and lesser rocks having felsic volcanic protoliths. These rocks are typical of the Wabigoon Subprovince, host to most of the pegmatites in the region. ▪ Ore Geology: Pegmatites are reasonably common in the region intruding the enclosing host rocks after metamorphism, evident from the manner in which the pegmatites cut across the well-developed foliation within the metamorphosed host rocks. This post-dating relationship is supported by radiometric dating; an age of 2666 ± 6 Ma is given for the timing of intrusion of the pegmatites (Breaks, et al., 2006). ▪ The pegmatites in North Aubry have a northeast plunge direction varying from 10 to 35 degrees from horizontal some 800m downdip extent and 250-300m strike. The North Upper and North Upper high-grade component within, appears to wedge towards the south east and is still open down dip and to the north west. ▪ Southern pegmatites are thinner and less well developed with higher muscovite content and appear to have a more north to north-westerly trend and dip more shallowly to the east. These pegmatites are also hosted in pillow basalts. ▪ The pegmatites are zoned with better developed spodumene crystal appearing as bands, often at an acute angle to the general trend of the pegmatite. ▪ The dominant economic minerals are spodumene with varying proportions of muscovite, microcline, and minor petalite and lepidolite. ▪ The adjacent pillow basalts contain minor disseminated pyrite and pyrrhotite. 																																																																													
<p>Drill hole information</p>	<ul style="list-style-type: none"> ▪ A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> ○ easting and northing of the drill hole collar ○ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ○ dip and azimuth of the hole ○ down hole length and interception depth ○ hole length. ▪ If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. 	<p>Metallurgy</p> <p>65 holes within the North Aubry USD2500 pit design were used for metallurgical work, with the following collar coordinates:</p> <table border="1" data-bbox="1094 1032 1692 1471"> <thead> <tr> <th>Holeid</th> <th>Northing</th> <th>Easting</th> <th>RL</th> <th>Depth</th> <th>Azi</th> <th>Dip</th> </tr> </thead> <tbody> <tr> <td>ASD001</td> <td>5585210</td> <td>397034</td> <td>395</td> <td>158</td> <td>89</td> <td>-89</td> </tr> <tr> <td>ASD003</td> <td>5585336</td> <td>397067</td> <td>375</td> <td>201</td> <td>202</td> <td>-73</td> </tr> <tr> <td>ASD004</td> <td>5585364</td> <td>397114</td> <td>379</td> <td>228</td> <td>195</td> <td>-71</td> </tr> <tr> <td>ASD006</td> <td>5585298</td> <td>397174</td> <td>388</td> <td>200</td> <td>201</td> <td>-75</td> </tr> <tr> <td>ASD007</td> <td>5585297</td> <td>397173</td> <td>388</td> <td>251</td> <td>201</td> <td>-85</td> </tr> <tr> <td>ASD009</td> <td>5585353</td> <td>397225</td> <td>390</td> <td>258</td> <td>219</td> <td>-85</td> </tr> <tr> <td>ASD011</td> <td>5585405</td> <td>397164</td> <td>391</td> <td>330</td> <td>196</td> <td>-86</td> </tr> <tr> <td>ASD012</td> <td>5585334</td> <td>397069</td> <td>375</td> <td>201</td> <td>197</td> <td>-54</td> </tr> <tr> <td>ASD013</td> <td>5585334</td> <td>397069</td> <td>375</td> <td>189</td> <td>185</td> <td>-61</td> </tr> <tr> <td>ASD015</td> <td>5585111</td> <td>397116</td> <td>386</td> <td>96</td> <td>52</td> <td>-85</td> </tr> </tbody> </table>	Holeid	Northing	Easting	RL	Depth	Azi	Dip	ASD001	5585210	397034	395	158	89	-89	ASD003	5585336	397067	375	201	202	-73	ASD004	5585364	397114	379	228	195	-71	ASD006	5585298	397174	388	200	201	-75	ASD007	5585297	397173	388	251	201	-85	ASD009	5585353	397225	390	258	219	-85	ASD011	5585405	397164	391	330	196	-86	ASD012	5585334	397069	375	201	197	-54	ASD013	5585334	397069	375	189	185	-61	ASD015	5585111	397116	386	96	52	-85
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Data aggregation methods	<ul style="list-style-type: none"> In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated. 	No drilling is reported in this release.																																																																																																																																																																	
Relationship between mineralisation	<ul style="list-style-type: none"> These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill 	No drilling is reported in this release.																																																																																																																																																																	

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widths and intercept lengths	<p>hole angle is known, its nature should be reported.</p> <ul style="list-style-type: none"> If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known'). 	
Diagrams	<ul style="list-style-type: none"> Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views. 	See attached Figures
Balanced reporting	<ul style="list-style-type: none"> Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results. 	No drilling is reported in this release.
Other substantive exploration data	<ul style="list-style-type: none"> Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density; groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances. 	<ul style="list-style-type: none"> GT1 completed a fixed wing single sensor magnetic/radiometric/VLF airborne geophysical survey. Survey details, 1191 line-km, 75m line spacing, direction 90 degrees to cross cut pegmatite strike, 70m altitude. Final images have been received for Total Count Radiometric, Total Magnetism and VLF from MPX. Interpretation has been by Southern Geoscience Green Technology Metals conducted geological field investigations and mapping on the Seymour property throughout the second half of the 2023 field season. Efforts were focused on finding new pegmatite occurrences, while mapping the bedrock geology, minerals and structure, across the property. A crew of four collected 194 rock samples and mapped 196 outcrop stations, mainly in the north half of the Seymour property as well as the area immediately NW of the North Aubry deposit. No significant discoveries were made.  <p>The map, titled 'Seymour Property 2023 Field Work', shows a topographic map of the Seymour property area. It features a black outline of the property boundary. Numerous green dots are scattered across the property, representing 'Rock Samples' and 'Bedrock Mapping Stations'. A legend in the bottom right corner identifies these symbols. The map also shows the 'Mud River' and 'Ferland' locations.</p>
Further work	<ul style="list-style-type: none"> The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive. 	<ul style="list-style-type: none"> Further Geological field mapping of anomalies and associated pegmatites at Seymour and regional claims incorporating auger sampling to better test bedrock potential. Drilling has commenced around neighbouring tenements (Junior Lake) following successful exploration reconnaissance work in 2024. Continuation of detailed mining studies