ASX ANNOUNCEMENT

20 March 2025

2024 Exploration Program results for the Northern Silica Project

- The 2024 drilling was completed in late December 2024, with 3,420 metres drilled across 154 holes at the Si2 deposit.
- The program was designed to complete infill and extensional drilling and collection of samples for ongoing metallurgical testwork and optimisation.
- New assaying regime developed focusing on the 0.71mm to 0.106mm fraction to enable better predictability of production quality and alignment with end-user product requirements.
- The 2024 samples as well as 683 composite samples produced from the 2023 program, were screened and assayed using the newly developed methods.
- 2024 drilling results will now be assessed and form the basis for a Mineral Resource Estimate update for the Si2 deposit as the project works towards delivering maiden Ore Reserves for the project.

Emerging silica sands developer, Diatreme Resources Limited (ASX:DRX) is pleased to provide an update on its recent drilling program and ongoing development milestones at the Northern Silica Project, underscoring the Company's progress toward delivering high-purity, low-iron silica for the expanding global photovoltaic glass market.

Diatreme's CEO, Neil McIntyre commented: *"Completion of the 2024 drilling program safely and on time marks another important milestone for the project. Results continue to confirm an extraordinary silica deposit highly amenable for on-site processing , high product recoveries and use as a direct feed product by photovoltaic grade glass manufacturers"*

"The 2024 drilling results will now be used for an updated Mineral Resource Estimate at the Si2 deposit, which is fundamental as we work towards delivering the maiden Ore Reserves and final stage Feasibility Study for the NSP. Diatreme also looks forward to results due in April from the 1-tonne bulk testwork at Mineral Technologies, which will further validate the product's quality and support commercial discussions.

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"The Company continues to advance this important project for Queensland's critical minerals industry, which will help power global decarbonisation while delivering valuable new jobs and investment for Hope Vale and the Far North Queensland region."

EXPLORATION UPDATE

The 2024 drilling program was successfully completed with 3,420 metres of air core drilling across 154 drillholes (*Figure 1*), delivering encouraging results that underscores Mineral Resource upgrade potential. Strategic infill drilling targeted zones requiring increased geological and grade continuity for mineral resource upgrades, while step-out holes tested a southeastern area that could open the door to further resource expansion beyond the current model.

This campaign was planned to further our understanding of dune sand thickness, continuity, and quality in key regions that hold the greatest promise for development of the Northern Silica Project. The 2024 exploration program concluded before the onset of the wet season (late December), ensuring field operations remained safe and efficient.

During the 2024 campaign, Diatreme changed the sampling methodology by collecting 1,152 three-metre composites, rather than 1m intervals. With assays on both head grade samples and a -<0.71mm >0.106mm fraction representative of product specification requirements, and the amount of -<0.71mm >0.106mm material in a bulk fraction. This approach ensures a comprehensive understanding of processing amenability, while targeting both overall deposit characteristics and the specific criteria required by end-users seeking low iron - high-purity silica. In addition, 683 composited intervals from the 2023 drilling program were characterised using the same analysis methodology (Appendix 1)

The -<0.71mm >0.106mm fraction from these samples underwent ME-ICP64 analysis at ALS Brisbane to pinpoint impurity levels and potential ferrous and clay contaminants. In parallel, head grade samples were assayed by ME-XRF26, to aid in refining process flowsheets and confirming alignment with market specifications.

Across 154 holes drilled, mineralised intercepts averaged around 20m in thickness, highlighting solid continuity of silica-rich material. Notably, a 48m drillhole Si220097 tapped into 46m of high-quality silica sand, with **96.7%** falling within -<0.71mm >0.106mm fraction, with an average grade of 0.082% Fe_2O_3 on the -<0.71mm >0.106mm fraction and 0.11% Fe_2O_3 on the raw sample, across the mineralised interval. These results reinforce both the scale and consistency of the resource and further bolster Diatreme's confidence in the project's commercial potential, paving the way for future resource updates and feasibility studies. All results, and locations are reported in **Appendix 1.**

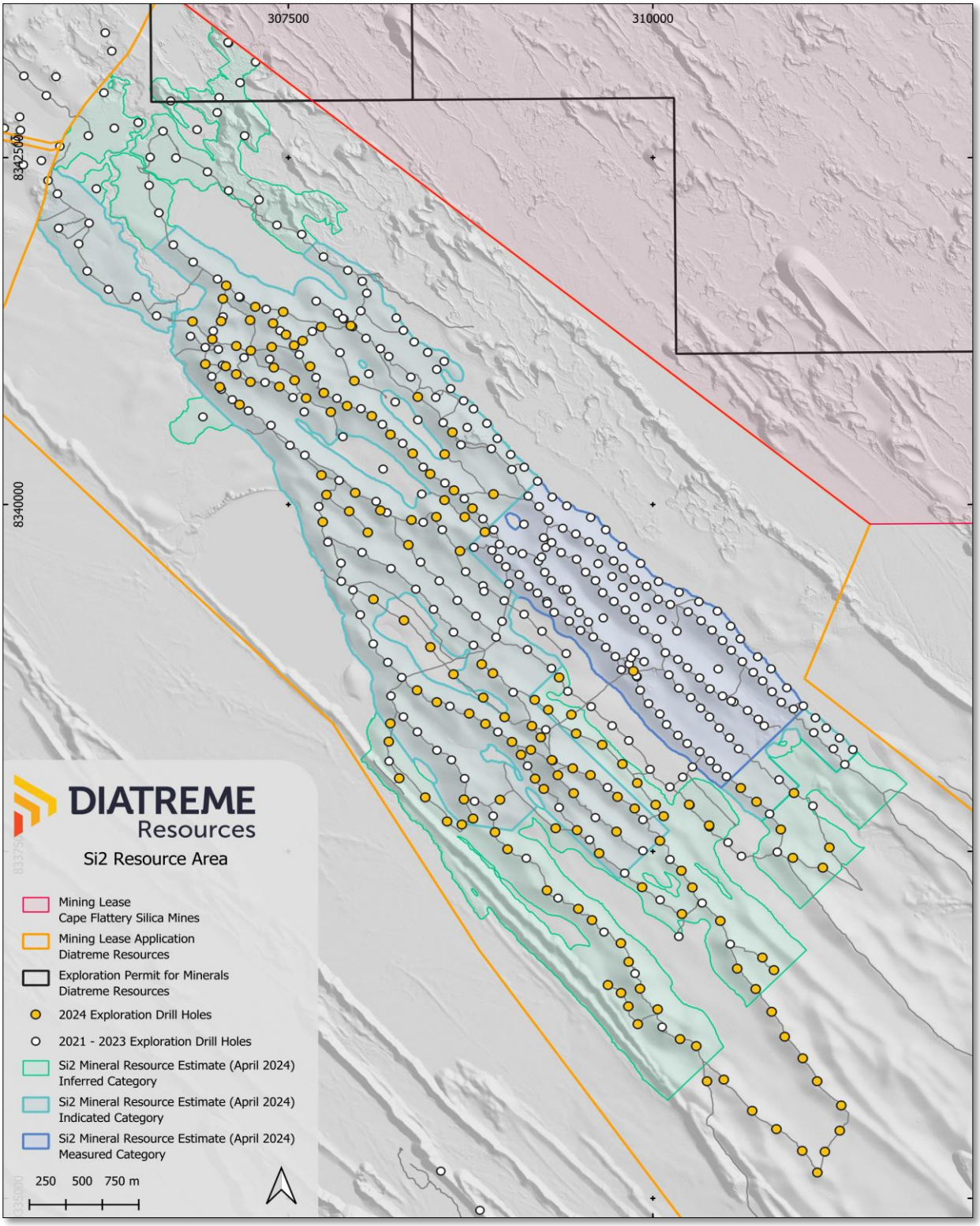

Figure 1: Si2 Exploration to Date

PROCESSING TESTWORK UPDATE

Recent benchtop characterisation tests on a subset of the 1-tonne bulk sample at Mineral Technologies have confirmed the ability to produce a low-iron, high-purity silica sand with Fe_2O_3 grade at 100ppm—directly meeting the specification under Chinese National Industrial Standard JC/T2314–2015.

Chinese National Standard Criteria		Benchtop Characterisation Results
Fe_2O_3	≤100ppm	**100ppm**
TiO_2	≤300ppm	**140ppm**
Cr_2O_3	≤5ppm	**2ppm**
0.104mm Fraction	≤5%	**0.3%**

Achieving these standards confirms the project's capacity to meet the PV glass market's expectations on our silica sand and showcases a strong **94.8%** recovery rate using the benchtop characterisation test from a subset of the bulk feed.

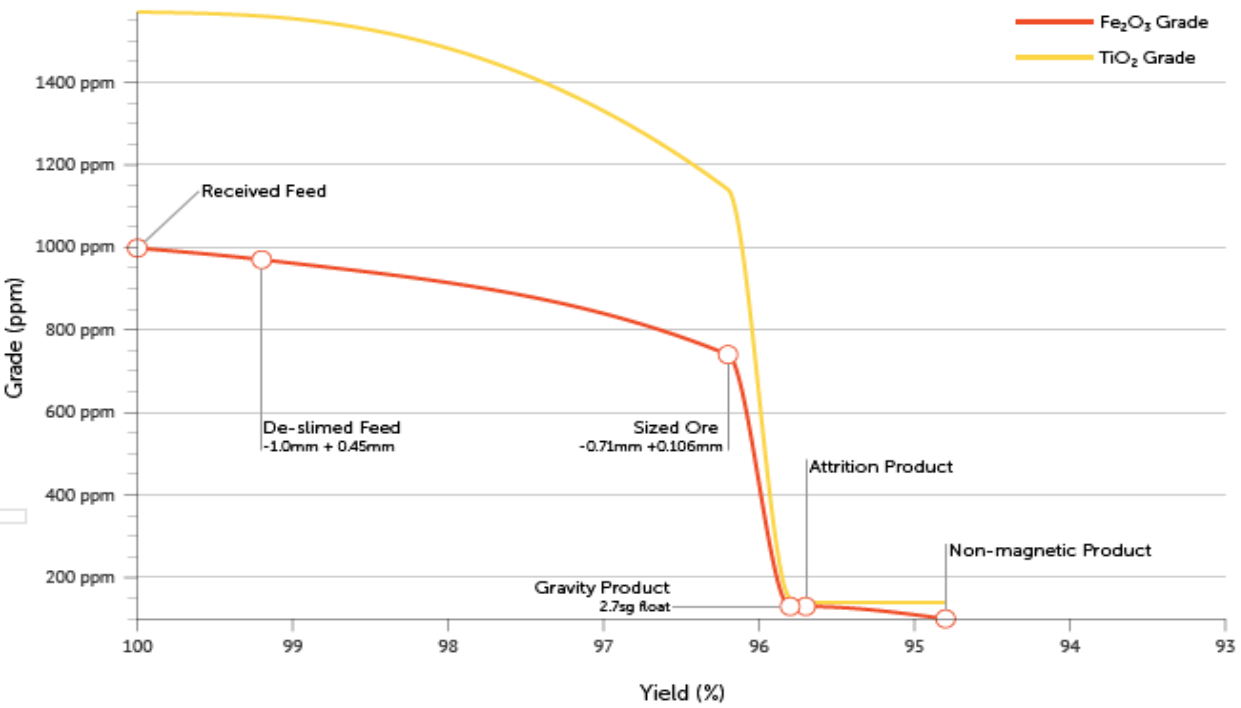

Figure 2: Fe2O3 and TiO2 performance through benchtop characterisation

By meeting the rigorous JC/T2314–2015 standards and achieving such a high recovery rate, Diatreme is well positioned to engage with prospective PV glass manufacturers on offtake agreements. The Company looks forward to the results of the 1-tonne bulk test work at Mineral Technologies, which will further validate the product's quality and support commercial discussions in the expanding photovoltaic market.

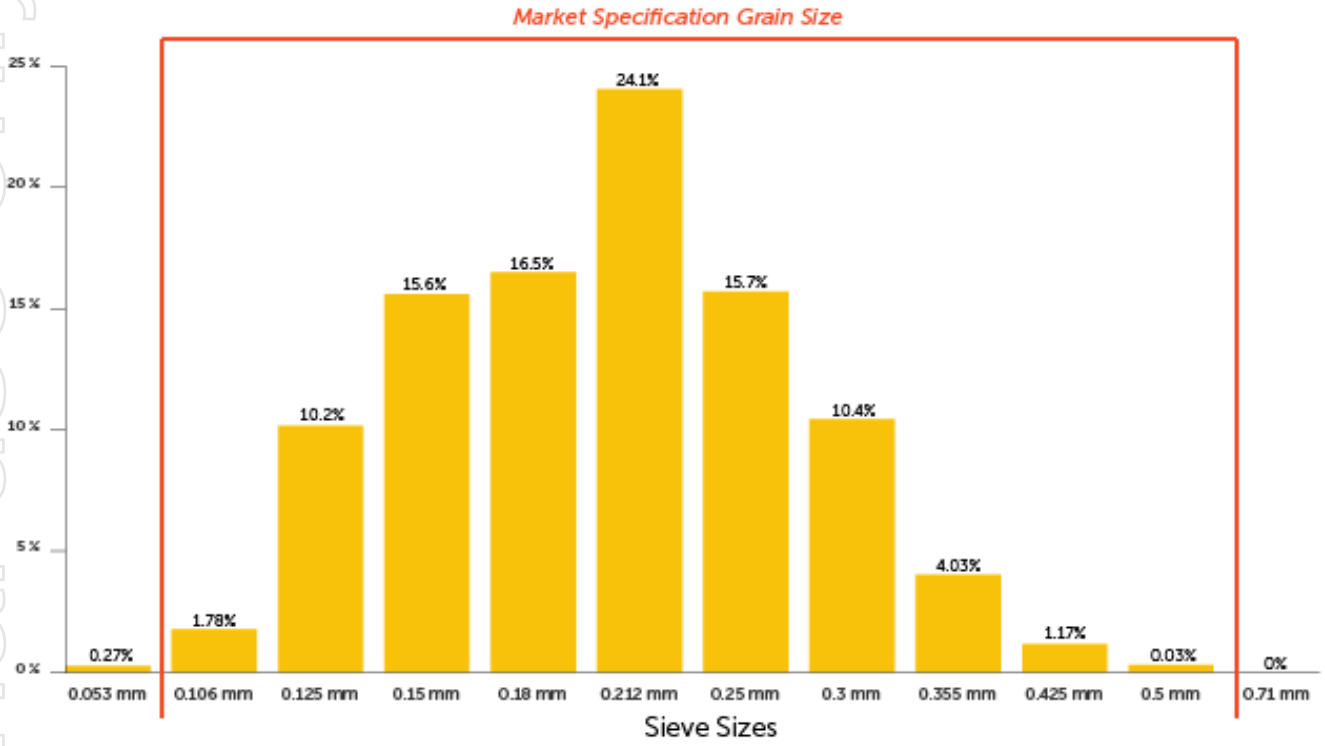

Figure 3: NSP Product Grain Size

NEXT STEPS

Ongoing bulk test work with Mineral Technologies in Carrara is focused on producing demonstrative product from sands at the Northern Silica Project. This work includes a 1-tonne bulk sample program, with results due in April 2025. These findings will validate the proposed flow sheet at scale, providing material suitable for securing offtake agreements.

Building on recent drilling and metallurgical data, Diatreme plans to undertake an updated Mineral Resource Estimate (MRE) in Q2 2025. This update will refine the geological model, incorporate the latest assay results, extents of environmental and cultural constraints identified during the ongoing EIS, and metallurgical test results to form the basis for subsequent development milestones.

Upon completion of the MRE update and bulk metallurgical test work Diatreme will then focus on delivering maiden Ore Reserves and next phase of Feasibility Study for the Northern Silica Project. Diatreme also continues to advance the environmental approvals process for the NSP, following receipt of the final Terms of Reference from the Office of the Coordinator-General (refer ASX release 22 January 2025).

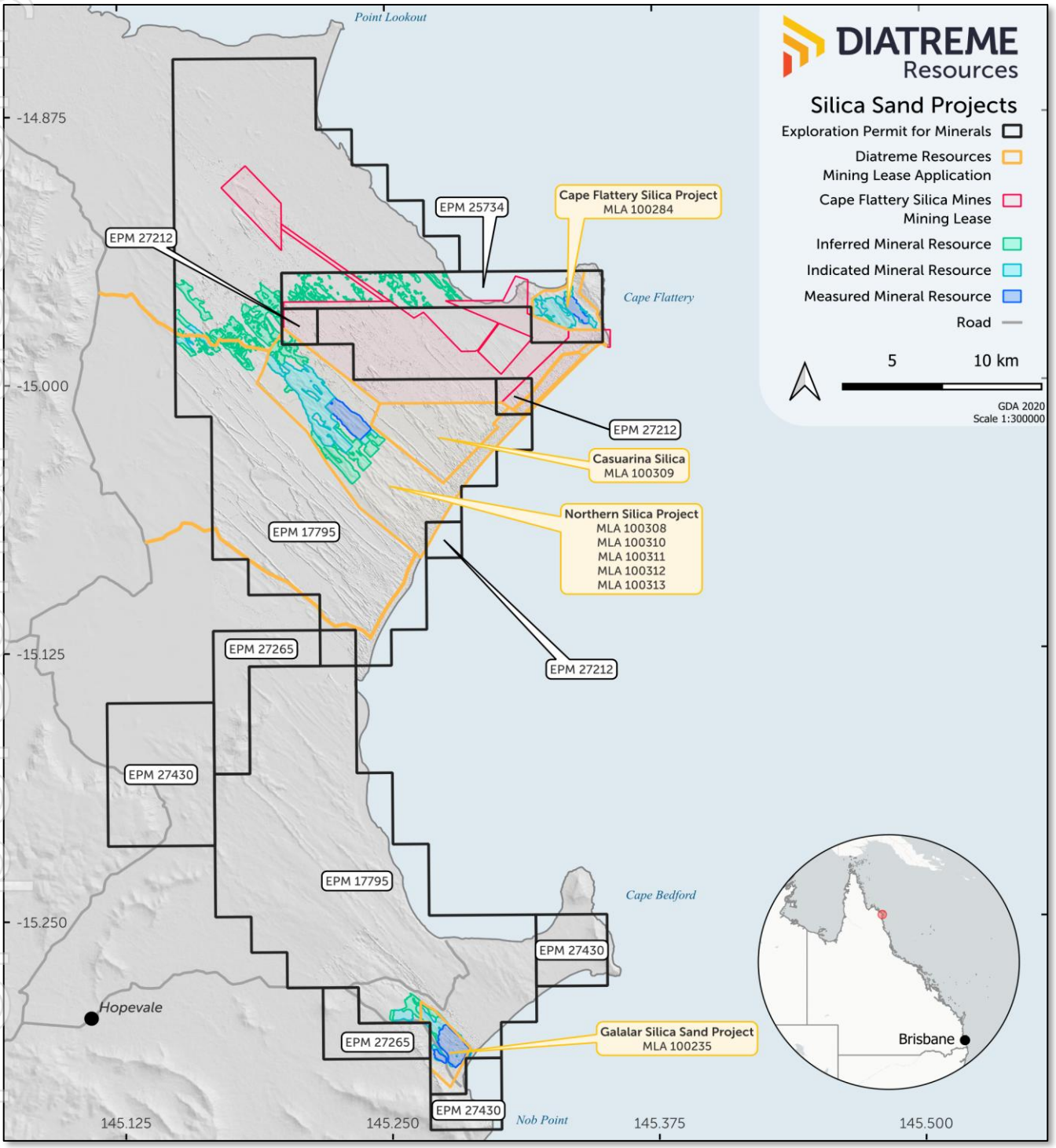

Figure 4: Diatreme's regional silica sand projects in FNQ

This announcement is authorised for release by the Board.

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About Diatreme Resources

Diatreme Resources (ASX:DRX) is an emerging Australian producer of mineral and silica sands based in Brisbane. Our key projects comprise the Northern Silica Project and Galalar Silica Sand Project in Far North Queensland, located next to the world's biggest silica sand mine at Cape Flattery, together with the recently acquired Cape Flattery Silica Project.

Both the Northern Silica and Cape Flattery projects have been designated “Coordinated Projects” by the Queensland Government and are strategically located near the export focused Cape Flattery Port.

In Western Australia’s Eucla Basin, Diatreme’s Cyclone Zircon Project is considered one of a handful of major zircon-rich discoveries of the past decade. Diatreme also owns 100% of the Clermont Copper-Gold Project in central Queensland.

Global material solutions group Sibelco is Diatreme’s development partner on its Queensland silica projects portfolio. Sibelco has completed an investment of circa $49 million into both the silica sands projects and Diatreme at the corporate level.

Diatreme’s silica sand resources will contribute to global decarbonisation by providing the necessary high-grade, premium-quality silica for use in the solar PV industry. The Company has a strong focus on ESG, working closely with its local communities and all other key stakeholders to ensure the long-term sustainability of our operations, including health, safety and environmental stewardship.

Diatreme has an experienced Board and management, with expertise across all stages of project exploration, mine development and project financing together with strong community and government engagement skills.

For more information, please visit www.diatreme.com.au

ASX releases referenced for this release:

- Quarterly Activities/Appendix 5B Cash Flow Report – 31 January 2025
- NSP environmental studies progress to final stages – 22 January 2025
- Mineral Resource upgrade paves way for Northern Silica Project PFS – 17 April 2024.

The above referenced announcement is available to view on both the Diatreme and ASX Websites. Diatreme Resources Limited confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and, in the case of estimates of Mineral Resources or Ore Reserves, that all material assumptions and technical parameters underpinning the estimates in the relevant market announcements continue to apply and have not materially changed. Diatreme Resources Limited confirms that the form and context in which the Competent Persons findings are presented have not been materially modified from the original market announcements.

COMPETENT PERSONS STATEMENT

The information in this report that relates to Exploration Results is based on information compiled by Mr Frazer Watson, a Competent Person who is a Member of the Australasian Institute of Mining and Metallurgy, and the Australian Institute of Geoscientists. Mr Watson is a full-time employee of Diatreme Resources Limited. Mr Watson has sufficient experience that is relevant to the style of mineralisation and the type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' Mr Watson consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The information in this report that relates to the processing of samples from the Galalar Silica Project is based on information provided by Mineral Technologies in Carrara. The information has been reviewed by Mr Phillip McMurtrie, a Competent Person who is a Member of the Australasian Institute of Mining and Metallurgy. Mr McMurtrie is a director of Tisana Pty Ltd, and is a technical consultant to Diatreme Resources Limited. Mc McMurtrie has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to quality as a Competent Person as defined in the 2012 edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr McMurtrie consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

APPENDIX 1: ASX Listing Rule 5.7 Summary

Table of Material Drillholes and Results

Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI21001 *	8339979	309213	53	0°	-90°	30	1	30	0.1	95.2	4.6	0.069	0.106	#					
SI21002 *	8339831	309383	61	0°	-90°	39	1	37	0.1	96.3	3.7	0.060	0.097	#					
SI21003 *	8339731	309562	60.3	0°	-90°	36	1	36	0.2	97.0	2.8	0.065	0.104	#					
SI21004 *	8339590	309728	51.8	0°	-90°	27	1	27	0.1	97.3	2.6	0.059	0.072	#					
SI21005 *	8339460	309875	50.8	0°	-90°	27	1	27	0.4	97.1	2.5	0.056	0.065	#					
SI21006 *	8339317	310036	48.5	0°	-90°	24	1	24	0.1	97.1	3.0	0.068	0.091	#					
SI21007 *	8339233	310245	44.1	0°	-90°	21	1	21	0.1	97.4	2.6	0.081	0.103	#					
SI21008 *	8339094	310405	55.5	0°	-90°	33	1	33	0.1	96.0	4.0	0.091	0.172	#					
SI21009 *	8338948	310535	44.5	0°	-90°	24	1	24	0.1	96.6	3.4	0.075	0.124	#					
SI21010 *	8338784	310685	47.6	0°	-90°	30	1	30	0.1	97.0	2.9	0.118	0.112	#					
SI21011	8338651	310818	40.1	0°	-90°	24	1	24	0.1	97.3	2.7	0.095	0.109	#					
SI21012	8338525	310962	35.4	0°	-90°	15	1	15	0.1	97.0	2.9	0.099	0.128	#					
SI21013 *	8338672	310392	65.8	0°	-90°	40	1	36	0.2	96.9	2.9	0.065	0.084	#					
SI21014 *	8338826	310239	56.3	0°	-90°	33	1	33	0.1	95.4	4.6	0.105	0.090	#					
SI21015 *	8338932	310086	58.2	0°	-90°	34	1	32	0.1	96.4	3.6	0.062	0.089	#					
SI21016 *	8339096	309940	53	0°	-90°	30	1	30	0.4	94.3	5.3	0.175	0.102	#					
SI21017 *	8339240	309811	56.5	0°	-90°	33	1	33	0.9	96.2	3.0	0.087	0.071	#					
SI21018 *	8339370	309660	59.6	0°	-90°	42	1	39	0.1	95.8	4.1	0.072	0.085	#					
SI21019 *	8339515	309541	58.2	0°	-90°	36	1	36	0.1	96.6	3.3	0.099	0.071	#					
SI21020 *	8339650	309367	60.1	0°	-90°	36	1	36	0.2	96.5	3.3	0.061	0.097	#					
SI21021 *	8339760	309253	69.6	0°	-90°	45	1	45	0.2	95.9	4.0	0.068	0.108	#					
SI21022 *	8339691	309266	66.9	0°	-90°	42	1	39	0.2	96.0	3.8	0.062	0.086	#					
SI21023 *	8339591	309216	63.4	0°	-90°	33	1	28	0.1	95.5	4.5	0.144	0.192	#					
SI21024 *	8339643	309105	62.4	0°	-90°	27	1	24	0.1	93.1	6.9	0.083	0.117	#					
SI21025 *	8339674	309035	58.9	0°	-90°	21	1	20	0.2	96.0	3.8	0.107	0.155	#					
SI21026	8339818	308909	52.4	0°	-90°	15	1	15	0.3	97.2	2.6	0.076	0.102	#					
SI21027	8339668	308894	64.2	0°	-90°	24	1	24	0.1	96.5	3.4	0.101	0.134	#					
SI21028 *	8339552	308992	55.2	0°	-90°	30	1	15	0.2	95.7	4.1	0.081	0.089	#					
SI21029 *	8339495	309084	60.4	0°	-90°	21	1	16	0.1	97.6	2.4	0.085	0.064	#					
SI21030 *	8339360	309205	59	0°	-90°	21	1	16	0.1	98.0	2.0	0.063	0.045	#					
SI21031 *	8339223	309323	48.8	0°	-90°	9	1	6	0.1	98.0	2.0	0.080	0.052	#					
SI21032 *	8339093	309504	55.3	0°	-90°	24	1	18	0.1	97.7	2.3	0.072	0.062	#					
SI21033 *	8338969	309674	59.3	0°	-90°	32	1	27	0.1	97.9	2.1	0.066	0.055	#					
SI21034 *	8338808	309776	60.9	0°	-90°	30	1	30	0.1	97.9	2.0	0.071	0.053	#					
SI21035 *	8338897	309851	70.5	0°	-90°	45	1	42	0.1	97.8	2.1	0.072	0.085	#					
SI21036 *	8339158	309562	56.2	0°	-90°	27	1	25	0.1	97.4	2.6	0.074	0.087	#					

Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI21037 *	8339224	309498	55.8	0°	-90°	36	1	25	0.2	96.9	3.0	0.086	0.151	#					
SI21038	8339305	309438	56.5	0°	-90°	27	1	24	0.1	97.4	2.5	0.094	0.121	#					
SI21039 *	8339386	309386	60.4	0°	-90°	27	1	23	0.2	98.1	1.7	0.083	0.088	#					
SI21040	8339452	309303	63.2	0°	-90°	30	1	26	0.1	97.2	2.7	0.073	0.082	#					
SI21041 *	8339512	309259	64.5	0°	-90°	30	1	28	0.1	96.7	3.3	0.107	0.155	#					
SI21042	8338756	309887	62.8	0°	-90°	33	1	30	0.1	97.2	2.8	0.099	0.115	#					
SI21043	8338846	309829	66.5	0°	-90°	39	1	36	0.1	97.4	2.6	0.076	0.094	#					
SI21044 *	8338660	309909	58.9	0°	-90°	24	1	20	0.1	96.2	3.8	0.070	0.098	#					
SI21045 *	8338489	310044	56.3	0°	-90°	21	1	20	0.1	97.3	2.6	0.064	0.057	#					
SI21046 *	8338336	310171	52.7	0°	-90°	24	1	20	0.2	97.7	2.1	0.055	0.047	#					
SI21047 *	8338217	310321	49.1	0°	-90°	15	1	12	0.1	98.2	1.8	0.061	0.043	#					
SI21048 *	8338146	310386	49.1	0°	-90°	15	1	13	0.1	98.9	1.1	0.063	0.033	#					
SI21049 *	8338099	310439	48	0°	-90°	15	1	10	0.1	98.6	1.4	0.075	0.063	#					
SI21050 *	8338869	309942	62.2	0°	-90°	39	1	34	0.1	96.9	3.1	0.090	0.104	#					
SI21051 *	8338673	310174	53.5	0°	-90°	24	1	21	0.1	96.5	3.5	0.075	0.074	#					
SI21052 *	8338533	310327	40.2	0°	-90°	12	1	7	0.4	94.2	5.6	0.068	0.077	#					
SI21053 *	8338390	310455	38.1	0°	-90°	18	1	15	0.4	97.1	2.6	0.200	0.108	#					
SI21054 *	8338324	310529	33.3	0°	-90°	12	1	12	0.2	94.4	5.5	0.074	0.046	#					
SI21055 *	8338577	310556	43.4	0°	-90°	21	1	20	0.2	98.2	1.6	0.065	0.035	#					
SI21056	8338516	310650	38.5	0°	-90°	16	1	15	0.1	98.3	1.7	0.105	0.073	#					
SI21057	8338450	310720	36.4	0°	-90°	15	1	12	0.1	97.9	2.1	0.084	0.083	#					
SI21058	8338406	310764	34.5	0°	-90°	15	1	12	0.1	98.1	1.9	0.148	0.044	#					
SI21059	8338236	311235	40.9	0°	-90°	21	1	21	0.1	96.4	3.6	0.149	0.139	#					
SI21060	8338109	310272	36.3	0°	-90°	12	No mineralisation intercepted. #												
SI21061	8338036	310205	38	0°	-90°	18	No mineralisation intercepted. #												
SI21062	8337830	310250	37.3	0°	-90°	15	1	3	0.3	97.0	2.7	0.082	0.042	#					
SI21063	8337561	310510	46.9	0°	-90°	16	No mineralisation intercepted. #												
SI21064	8338092	309981	37.3	0°	-90°	15	No mineralisation intercepted. #												
SI21065	8338406	309721	39.6	0°	-90°	14	No mineralisation intercepted. #												
SI21066	8338656	309418	38.1	0°	-90°	18	No mineralisation intercepted. #												
SI21067	8338951	309137	33.1	0°	-90°	12	No mineralisation intercepted. #												
SI21068	8339158	308966	31.7	0°	-90°	9	1	7	0.1	96.4	3.5	0.076	0.037	#					
SI21069	8339209	309117	34.7	0°	-90°	14	1	3	0.3	92.1	7.6	0.096	0.052	#					
SI21070	8339087	309240	33.9	0°	-90°	12	1	4	0.5	96.4	3.1	0.463	0.065	#					
SI21071	8338926	309406	34.9	0°	-90°	12	No mineralisation intercepted. #												
SI21072 *	8339428	309014	43.9	0°	-90°	9	1	9	0.8	97.4	1.8	0.926	0.338	#					
SI21073	8339307	308981	37.2	0°	-90°	9	1	7	0.2	97.0	2.8	0.071	0.033	#					
SI21074	8339415	308835	34.7	0°	-90°	12	1	6	0.2	98.3	1.6	0.091	0.027	#					
SI21075	8339516	308716	31.9	0°	-90°	12	1	10	0.3	97.6	2.0	0.109	0.030	#					
SI21076	8339450	308535	32.4	0°	-90°	12	1	10	0.5	96.5	3.0	0.121	0.054	#					
SI21077	8339192	308783	42.3	0°	-90°	23	1	15	0.1	97.5	2.5	0.117	0.073	#					

Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI21078	8339080	308633	45.9	0°	-90°	19	1	10	0.3	97.2	2.5	0.087	0.057	#					
SI21079	8339386	308370	43.6	0°	-90°	9	1	6	0.1	97.3	2.7	0.082	0.067	#					
SI21080	8339651	308002	59.5	0°	-90°	30	1	27	0.1	98.4	1.6	0.071	0.088	#					
SI21081	8339574	307851	49.5	0°	-90°	18	1	18	0.1	97.6	2.4	0.088	0.098	#					
SI21082	8339444	307858	51	0°	-90°	21	1	21	0.1	97.6	2.4	0.066	0.087	#					
SI21083	8339206	307991	43.3	0°	-90°	15	1	15	0.2	97.5	2.3	0.065	0.055	#					
SI21084	8338858	308178	57.2	0°	-90°	24	1	24	0.1	95.6	4.4	0.076	0.151	#					
SI21085	8338615	308194	57.6	0°	-90°	27	1	27	0.2	97.7	2.1	0.062	0.058	#					
SI21086	8338361	308383	52.7	0°	-90°	21	1	21	0.1	96.9	3.1	0.057	0.050	#					
SI21087	8338160	308619	62.7	0°	-90°	27	1	23	0.3	97.8	2.0	0.061	0.070	#					
SI21088	8337859	308773	62.1	0°	-90°	30	1	27	0.3	97.3	2.4	0.068	0.055	#					
SI220001	8339318	308084	40.7	0°	-90°	12	1	12	0.4	94.5	5.0	0.098	0.043	98.74	0.13	0.07	0.11	0.23	99.39
SI220002	8339166	308293	40.4	0°	-90°	15	No mineralisation intercepted.												
SI220003	8338973	308474	38.2	0°	-90°	15	No mineralisation intercepted.												
SI220004	8338777	308633	40.3	0°	-90°	15	No mineralisation intercepted.												
SI220005	8338609	308836	44.3	0°	-90°	12	No mineralisation intercepted.												
SI220006	8338468	308983	48.7	0°	-90°	9	1	4	0.3	94.7	4.9	0.085	0.049	98.84	0.08	0.07	0.10	0.15	99.33
SI220007	8338405	309170	84.3	0°	-90°	39	1	37	0.1	95.6	4.3	0.061	0.086	99.05	0.07	0.15	0.18	0.12	99.68
SI220008	8338323	309232	79.5	0°	-90°	34	1	32	0.2	96.6	3.2	0.066	0.058	98.97	0.07	0.09	0.09	0.14	99.44
SI220009	8338050	309348	85.2	0°	-90°	42	1	42	0.2	96.4	3.4	0.132	0.087	99.00	0.12	0.13	0.15	0.14	99.64
SI220010	8337920	309457	78.4	0°	-90°	36	1	30	0.2	96.5	3.3	0.137	0.094	98.91	0.18	0.14	0.17	0.14	99.66
SI220011	8337643	309751	67.9	0°	-90°	23	1	16	0.3	97.2	2.6	0.080	0.058	98.91	0.09	0.08	0.07	0.13	99.37
SI220012	8338099	309451	79.2	0°	-90°	41	1	33	0.1	95.8	4.1	0.073	0.080	98.83	0.10	0.10	0.11	0.15	99.38
SI220013	8338051	309572	78.9	0°	-90°	57	1	36	0.1	95.4	4.5	0.074	0.100	98.86	0.09	0.12	0.15	0.16	99.49
SI220014	8337894	309758	70.6	0°	-90°	39	1	30	0.2	95.0	4.9	0.115	0.146	98.62	0.14	0.18	0.21	0.16	99.44
SI220015	8337808	309872	64.8	0°	-90°	30	1	24	0.2	95.8	4.0	0.185	0.107	98.65	0.20	0.13	0.14	0.18	99.42
SI220016	8337577	310047	55.5	0°	-90°	30	1	10	0.1	95.4	4.5	0.084	0.057	98.94	0.09	0.08	0.12	0.16	99.47
SI220017	8337361	310196	65.4	0°	-90°	27	1	13	0.1	95.8	4.1	0.116	0.147	98.69	0.13	0.19	0.29	0.15	99.58
SI220018	8337241	310271	66.4	0°	-90°	27	1	9	0.1	95.1	4.8	0.109	0.121	98.34	0.16	0.18	0.29	0.15	99.25
SI220019	8336999	310463	71.6	0°	-90°	24	1	13	0.1	93.3	6.7	0.101	0.131	98.49	0.14	0.21	0.33	0.12	99.43
SI220020	8337049	310199	72.6	0°	-90°	18	1	9	0.1	96.0	3.9	0.086	0.086	98.75	0.14	0.12	0.13	0.15	99.41
SI220021	8337242	309926	67.6	0°	-90°	12	1	5	0.3	93.2	6.5	0.222	0.212	98.29	0.29	0.29	0.28	0.27	99.56
SI220022	8337487	309632	73.7	0°	-90°	24	1	15	0.2	94.4	5.5	0.115	0.165	98.54	0.18	0.26	0.35	0.15	99.66
SI220023	8337653	309480	77.5	0°	-90°	24	1	18	0.3	94.0	5.7	0.112	0.112	98.73	0.17	0.17	0.23	0.16	99.60
SI220024	8337951	309252	54.6	0°	-90°	18	1	5	0.3	93.0	6.8	0.168	0.089	98.62	0.20	0.14	0.18	0.19	99.46
SI220025	8338024	309192	53.6	0°	-90°	12	1	5	0.5	93.5	5.9	0.127	0.049	98.68	0.23	0.08	0.13	0.40	99.66
SI220026	8338197	309096	64.3	0°	-90°	18	1	15	0.1	94.8	5.2	0.090	0.066	98.83	0.11	0.08	0.12	0.17	99.41
SI220027	8338232	309163	69.5	0°	-90°	24	1	21	0.2	95.8	4.0	0.076	0.066	99.19	0.10	0.08	0.10	0.15	99.72
SI220028	8338290	309034	70.7	0°	-90°	25	1	23	0.5	95.9	3.6	0.147	0.139	98.78	0.16	0.15	0.11	0.22	99.54
SI220029	8338420	308852	64.7	0°	-90°	21	1	17	0.1	94.6	5.3	0.102	0.128	98.82	0.12	0.17	0.25	0.12	99.60
SI220030	8338495	308740	60.6	0°	-90°	21	1	17	0.2	95.5	4.3	0.075	0.078	98.99	0.12	0.11	0.17	0.13	99.62

Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI220031	8338576	308518	56.3	0°	-90°	24	1	18	0.1	96.9	3.1	0.103	0.066	98.84	0.13	0.09	0.09	0.16	99.37
SI220032	8338662	308383	58.8	0°	-90°	30	1	28	1.7	95.4	2.9	0.081	0.057	99.20	0.10	0.08	0.08	0.20	99.72
SI220033	8338423	308200	44.9	0°	-90°	15	1	13	0.1	97.3	2.6	0.117	0.084	98.72	0.14	0.14	0.20	0.14	99.48
SI220034	8338292	308189	48.1	0°	-90°	18	1	18	0.1	95.1	4.9	0.061	0.075	99.03	0.08	0.11	0.18	0.15	99.64
SI220035	8338027	308260	42	0°	-90°	15	1	9	0.1	93.7	6.3	0.072	0.075	98.73	0.07	0.12	0.22	0.16	99.43
SI220036	8337638	308916	56.9	0°	-90°	26	1	18	0.1	96.5	3.5	0.062	0.060	99.08	0.06	0.08	0.11	0.09	99.50
SI220037	8337514	309002	63.8	0°	-90°	29	1	23	0.1	97.9	2.1	0.135	0.080	98.88	0.19	0.09	0.13	0.13	99.61
SI220038	8337218	309270	80.3	0°	-90°	29	1	27	0.1	97.6	2.3	0.083	0.116	99.00	0.09	0.13	0.16	0.08	99.56
SI220039	8337085	309487	80.6	0°	-90°	25	1	23	0.2	98.1	1.7	0.114	0.142	98.98	0.12	0.17	0.22	0.14	99.72
SI220040	8337003	309581	82.1	0°	-90°	24	1	24	0.2	97.8	2.1	0.121	0.123	99.11	0.14	0.14	0.13	0.13	99.74
SI220041	8336837	309779	77.1	0°	-90°	15	1	14	0.1	97.3	2.6	0.095	0.198	98.79	0.12	0.21	0.29	0.12	99.64
SI220042	8336705	309834	91.2	0°	-90°	32	1	32	0.3	97.5	2.2	0.121	0.132	98.95	0.15	0.15	0.16	0.12	99.62
SI220043	8336511	309912	99.9	0°	-90°	39	1	38	0.3	96.7	3.0	0.120	0.165	98.72	0.14	0.21	0.25	0.11	99.58
SI220044	8336362	310033	103	0°	-90°	45	1	43	0.1	97.9	2.0	0.109	0.132	98.99	0.12	0.17	0.19	0.12	99.68
SI220045	8336255	309897	78.6	0°	-90°	25	1	21	0.1	97.6	2.4	0.087	0.093	99.09	0.10	0.12	0.13	0.12	99.63
SI220046	8336384	309832	80.6	0°	-90°	27	1	24	0.1	97.9	2.0	0.080	0.122	99.03	0.09	0.14	0.15	0.12	99.65
SI220047	8336480	309782	73.4	0°	-90°	15	1	12	0.1	96.7	3.3	0.071	0.111	99.02	0.08	0.17	0.25	0.09	99.70
SI220048	8336537	309692	67.1	0°	-90°	21	1	7	0.1	95.0	5.0	0.078	0.080	99.42	0.11	0.12	0.19	0.13	100.03
SI220049	8336148	310186	92	0°	-90°	37	1	30	0.1	98.3	1.7	0.096	0.076	99.26	0.09	0.09	0.08	0.13	99.73
SI220050	8336097	310298	89.6	0°	-90°	29	1	27	0.1	98.4	1.5	0.100	0.101	99.04	0.11	0.11	0.11	0.14	99.59
SI220051	8335844	310372	79.9	0°	-90°	12	1	9	0.5	96.8	2.7	0.070	0.095	99.09	0.09	0.09	0.15	0.13	99.66
SI220052	8335856	310487	96.6	0°	-90°	26	1	25	0.1	97.3	2.7	0.093	0.156	98.84	0.12	0.19	0.23	0.11	99.60
SI220053	8335631	310681	103	0°	-90°	34	1	30	0.1	97.6	2.3	0.107	0.108	98.96	0.13	0.13	0.13	0.12	99.55
SI220054	8335499	310848	96.9	0°	-90°	17	1	15	0.1	99.0	0.9	0.102	0.105	98.98	0.12	0.12	0.08	0.12	99.48
SI220055	8335342	311025	91.7	0°	-90°	6	No mineralisation intercepted.												
SI220056	8335186	311129	105	0°	-90°	18	No mineralisation intercepted.												
SI220057	8335336	311180	86.5	0°	-90°	6	No mineralisation intercepted.												
SI220058	8335488	311282	81.4	0°	-90°	6	No mineralisation intercepted.												
SI220059	8335670	311292	99.4	0°	-90°	24	1	21	0.2	98.3	1.5	0.056	0.068	99.28	0.06	0.08	0.12	0.09	99.71
SI220060	8335844	311127	102	0°	-90°	26	1	24	0.3	98.3	1.5	0.058	0.046	99.26	0.08	0.06	0.08	0.10	99.64
SI220061	8336009	311028	101	0°	-90°	30	1	27	0.2	98.7	1.1	0.060	0.042	99.30	0.09	0.06	0.07	0.09	99.68
SI220062	8336165	310905	103	0°	-90°	28	1	27	0.1	98.4	1.6	0.076	0.047	99.32	0.11	0.07	0.09	0.07	99.72
SI220063	8336345	310815	102	0°	-90°	25	1	24	0.4	97.6	2.0	0.067	0.083	99.05	0.11	0.11	0.16	0.17	99.70
SI220064	8336508	310705	95.4	0°	-90°	30	1	28	0.4	97.3	2.3	0.056	0.062	99.13	0.10	0.08	0.13	0.10	99.63
SI220065	8336656	310579	102	0°	-90°	33	1	31	0.1	98.1	1.9	0.063	0.079	98.97	0.10	0.11	0.17	0.13	99.57
SI220066	8336735	310751	82.6	0°	-90°	21	1	20	0.1	97.5	2.5	0.068	0.096	98.98	0.12	0.13	0.19	0.10	99.59
SI220067	8336645	310831	78.5	0°	-90°	15	1	13	0.1	97.8	2.2	0.075	0.085	99.24	0.12	0.11	0.17	0.09	99.80
SI220068	8337667	309333	63.5	0°	-90°	10	1	9	0.1	96.0	4.0	0.057	0.070	99.22	0.09	0.10	0.17	0.15	99.80
SI220069	8337873	308951	57.8	0°	-90°	15	1	13	0.5	97.7	1.8	0.060	0.056	99.42	0.10	0.09	0.13	0.91	100.71
SI220070	8337875	308705	70.1	0°	-90°	39	1	36	0.3	98.0	1.7	0.079	0.051	99.22	0.11	0.06	0.07	0.14	99.67
SI220071	8337736	308764	55.6	0°	-90°	21	1	19	0.1	97.3	2.7	0.081	0.073	99.21	0.12	0.09	0.14	0.10	99.73

Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI220072	8337694	308690	44.2	0°	-90°	10	1	8	0.2	94.3	5.6	0.070	0.034	99.24	0.10	0.06	0.11	0.08	99.65
SI220073	8337716	308589	47.4	0°	-90°	10	1	8	0.1	97.4	2.6	0.070	0.051	99.05	0.10	0.07	0.11	0.06	99.46
SI220074	8337890	308439	45.8	0°	-90°	9	1	8	0.1	96.7	3.3	0.083	0.068	99.07	0.12	0.10	0.14	0.15	99.64
SI220075	8338521	309283	54.5	0°	-90°	18	1	16	0.4	96.6	3.1	0.072	0.057	99.27	0.12	0.07	0.11	0.16	99.81
SI220076	8338593	309190	54.1	0°	-90°	15	1	14	0.1	97.5	2.4	0.097	0.068	99.29	0.16	0.08	0.11	0.15	99.90
SI220077	8338784	308903	51.3	0°	-90°	9	1	8	0.1	98.6	1.4	0.078	0.045	99.58	0.09	0.07	0.08	-0.01	99.90
SI220078	8338848	308824	54.7	0°	-90°	18	1	15	0.2	99.0	0.8	0.077	0.048	99.49	0.10	0.06	0.06	0.06	99.86
SI220079	8338486	309441	49.3	0°	-90°	12	1	10	0.4	95.8	3.9	0.137	0.095	99.21	0.16	0.11	0.16	0.17	99.93
SI220080	8338350	309474	62.4	0°	-90°	30	1	27	0.1	98.5	1.4	0.081	0.084	99.24	0.12	0.22	0.12	0.07	99.87
SI220081	8338269	309653	43.7	0°	-90°	6	2	4	0.2	92.7	7.1	0.102	0.110	98.93	0.18	0.17	0.26	0.15	99.80
SI220082	8338130	309791	44.8	0°	-90°	15	1	9	0.3	96.2	3.6	0.070	0.066	99.20	0.09	0.08	0.12	0.11	99.70
SI220083	8337991	309892	47.5	0°	-90°	12	1	9	0.2	97.0	2.8	0.132	0.072	99.05	0.16	0.09	0.14	0.18	99.71
SI220084	8337835	310018	46.6	0°	-90°	12	1	11	0.3	95.3	4.3	0.072	0.045	99.11	0.11	0.06	0.11	0.09	99.57
SI220085	8337754	310074	46.4	0°	-90°	12	1	7	0.6	93.9	5.6	0.057	0.043	99.25	0.07	0.06	0.12	0.03	99.62
SI220086	8337838	310249	37.4	0°	-90°	9	No mineralisation intercepted.												
SI220087	8337688	310386	37.7	0°	-90°	15	1	13	1.3	94.2	4.5	0.054	0.030	99.61	0.06	0.04	0.07	0.08	99.95
SI220088	8337657	310877	47.9	0°	-90°	24	1	24	0.3	95.9	3.8	0.058	0.057	99.41	0.09	0.08	0.12	0.14	99.92
SI220089	8337857	310710	46.9	0°	-90°	9	1	7	0.1	96.1	3.8	0.062	0.054	99.44	0.09	0.09	0.13	0.11	99.92
SI220090	8337957	310603	48.1	0°	-90°	12	1	9	0.1	98.3	1.6	0.074	0.050	99.40	0.11	0.06	0.08	0.20	99.94
SI220091	8337451	310960	65.7	0°	-90°	36	1	33	0.1	97.5	2.4	0.067	0.126	98.92	0.11	0.18	0.26	0.09	99.65
SI220092	8337381	311166	53.6	0°	-90°	24	1	23	0.1	97.0	3.0	0.063	0.067	99.19	0.10	0.10	0.14	0.14	99.73
SI220093	8337528	311211	37.4	0°	-90°	6	1	2	0.4	93.8	5.8	0.085	0.226	97.23	0.16	1.56	0.38	0.32	99.78
SI220094	8337921	310968	32.5	0°	-90°	6	No mineralisation intercepted.												
SI220095	8338800	309865	65.1	0°	-90°	39	1	36	0.1	96.9	3.1	0.119	0.093	99.12	0.16	0.12	0.15	0.12	99.73
SI220096	8338754	309357	37.6	0°	-90°	15	1	15	0.3	93.9	5.8	0.345	0.068	98.58	0.41	0.09	0.20	0.38	99.72
SI220097	8338159	309307	96.4	0°	-90°	48	1	47	0.2	96.7	3.1	0.059	0.082	99.27	0.11	0.11	0.13	0.09	99.77
SI220098	8341223	307482	70.2	0°	-90°	35	1	32	0.1	95.9	4.1	0.084	0.138	98.94	0.13	0.20	0.32	0.13	99.84
SI220099	8341307	307393	64.1	0°	-90°	33	1	30	0.1	96.9	3.1	0.075	0.110	99.18	0.10	0.14	0.18	0.13	99.81
SI220100	8341389	307463	54.9	0°	-90°	28	1	23	0.1	97.1	2.8	0.054	0.060	99.13	0.08	0.08	0.13	0.15	99.65
SI220101	8341425	307273	52.2	0°	-90°	24	1	22	0.2	96.4	3.4	0.066	0.084	98.93	0.09	0.13	0.21	0.16	99.62
SI220102	8341578	307074	49.9	0°	-90°	21	1	19	0.1	98.1	1.9	0.065	0.046	99.40	0.09	0.07	0.11	0.17	99.92
SI220103	8341484	307048	48.3	0°	-90°	22	1	21	0.5	96.2	3.4	0.065	0.083	99.25	0.09	0.12	0.21	0.14	99.90
SI220104	8341329	307238	43.5	0°	-90°	14	1	11	0.1	97.6	2.4	0.051	0.035	99.22	0.07	0.06	0.09	0.11	99.61
SI220105	8341109	307242	52.1	0°	-90°	30	1	30	0.3	96.5	3.2	0.065	0.070	99.24	0.09	0.10	0.17	0.13	99.80
SI220106	8341143	307143	54.6	0°	-90°	30	1	29	0.2	97.1	2.7	0.053	0.051	99.42	0.07	0.06	0.10	0.12	99.84
SI220107	8341136	307386	71.1	0°	-90°	45	1	45	0.5	97.2	2.3	0.101	0.053	99.28	0.11	0.07	0.09	0.06	99.68
SI220108	8341322	307039	52.2	0°	-90°	26	1	24	0.3	93.7	6.1	0.055	0.051	99.31	0.07	0.10	0.17	0.13	99.84
SI220109	8341192	306978	58	0°	-90°	33	1	31	0.1	95.8	4.2	0.053	0.047	99.29	0.06	0.09	0.13	0.12	99.76
SI220110	8341010	306927	71.2	0°	-90°	45	1	45	0.3	95.8	3.9	0.051	0.049	99.43	0.06	0.07	0.11	0.10	99.85
SI220111	8340846	307027	59	0°	-90°	33	1	31	0.4	94.9	4.8	0.058	0.087	99.29	0.08	0.12	0.20	0.20	99.98
SI220112	8340717	307163	55.7	0°	-90°	27	1	27	0.2	97.0	2.8	0.059	0.073	99.38	0.08	0.09	0.14	0.14	99.90

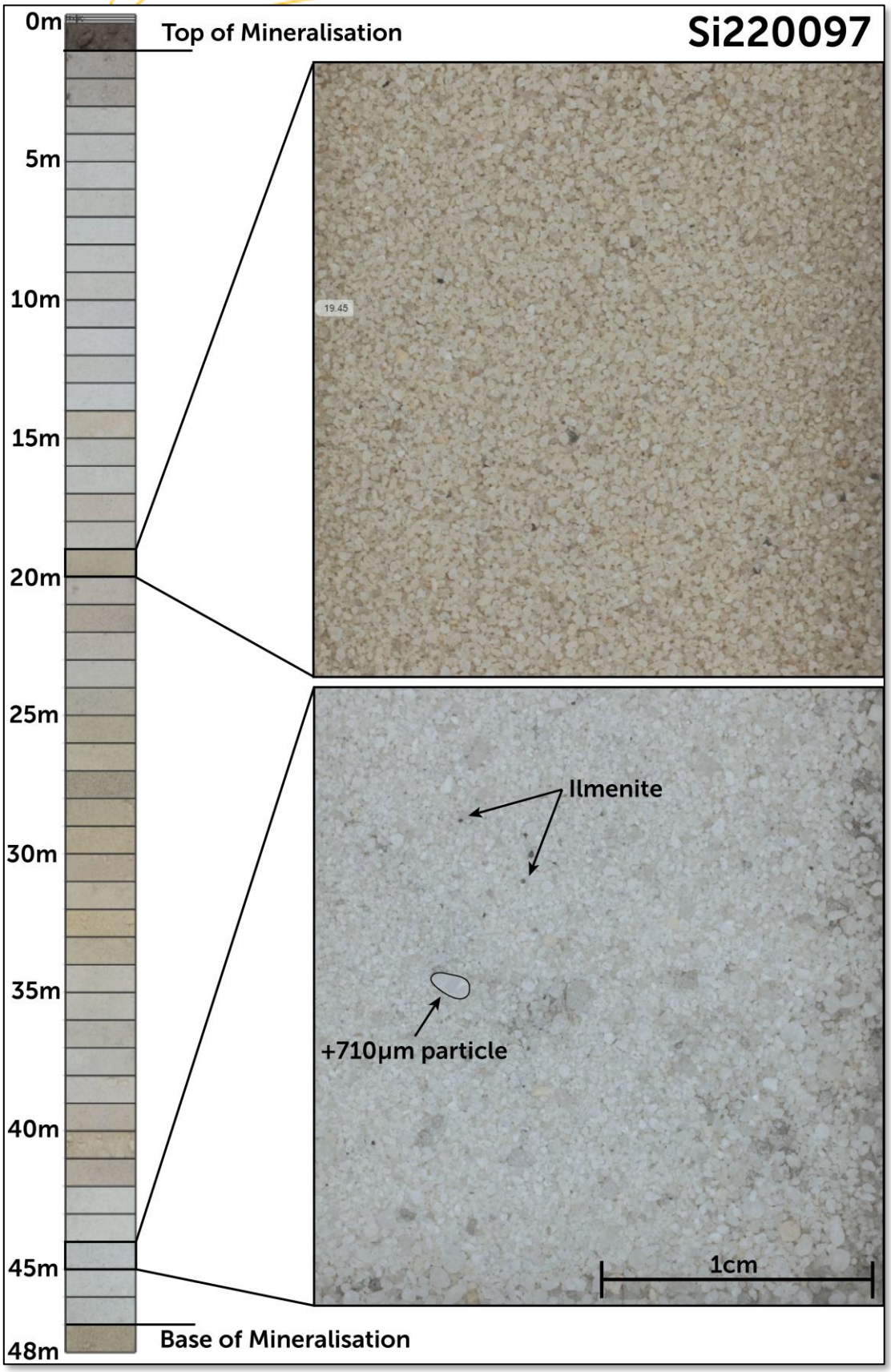
Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI220113	8340212	307727	50.3	0°	-90°	21	2	21	0.1	96.6	3.3	0.056	0.052	99.53	0.09	0.07	0.11	0.16	100.03
SI220114	8340071	307759	49.8	0°	-90°	20	1	20	0.1	96.5	3.5	0.063	0.078	99.12	0.08	0.09	0.14	0.13	99.63
SI220115	8339952	307918	49.5	0°	-90°	21	1	21	0.1	96.8	3.2	0.059	0.088	99.44	0.08	0.10	0.17	0.13	100.00
SI220116	8339799	308045	46.1	0°	-90°	16	1	13	0.2	93.1	6.8	0.061	0.071	99.43	0.09	0.09	0.16	0.11	99.95
SI220117	8339874	307734	51.7	0°	-90°	24	1	21	0.1	97.0	2.9	0.069	0.105	99.23	0.09	0.12	0.19	0.06	99.78
SI220118	8340085	307959	50.6	0°	-90°	22	1	22	0.2	96.8	3.0	0.077	0.048	99.36	0.11	0.07	0.08	0.16	99.86
SI220119	8339958	308131	63	0°	-90°	33	1	33	0.6	97.1	2.3	0.071	0.041	99.35	0.13	0.06	0.08	0.22	99.89
SI220120	8339709	308323	35	0°	-90°	9	1	6	0.6	93.4	6.1	0.079	0.044	99.01	0.15	0.08	0.15	0.13	99.59
SI220121	8339887	308343	54.2	0°	-90°	29	1	27	0.1	97.4	2.6	0.062	0.059	99.56	0.09	0.08	0.11	0.10	100.00
SI220122	8339912	308511	66.8	0°	-90°	30	1	25	0.1	98.0	2.0	0.071	0.054	99.53	0.08	0.07	0.10	0.14	99.98
SI220123	8339664	308677	37.6	0°	-90°	11	1	7	0.1	97.5	2.5	0.080	0.043	99.71	0.11	0.06	0.08	0.12	100.13
SI220124	8339802	308848	47.6	0°	-90°	7	1	4	0.6	94.7	4.7	0.079	0.097	99.02	0.11	0.14	0.22	0.12	99.73
SI220125	8339911	308710	44.5	0°	-90°	9	1	8	0.7	96.0	3.4	0.070	0.074	99.33	0.09	0.10	0.18	0.21	100.01
SI220126	8340032	308571	43.9	0°	-90°	6	No mineralisation intercepted.												
SI220127	8339971	308762	55.1	0°	-90°	18	1	15	0.1	98.0	2.0	0.085	0.113	99.44	0.13	0.13	0.18	0.09	100.06
SI220128	8340104	308637	57.7	0°	-90°	24	1	21	0.3	97.3	2.5	0.166	0.112	99.12	0.21	0.14	0.11	0.26	99.93
SI220129	8340221	308473	56.2	0°	-90°	15	1	12	0.2	97.6	2.2	0.106	0.125	98.72	0.12	0.13	0.15	0.12	99.34
SI220130	8340368	308353	57	0°	-90°	15	1	14	0.1	97.9	2.1	0.088	0.102	99.19	0.13	0.11	0.12	0.18	99.81
SI220131	8340505	308200	55.4	0°	-90°	18	1	16	0.2	97.0	2.8	0.085	0.088	99.02	0.09	0.10	0.12	0.22	99.67
SI220132	8340638	308072	59.2	0°	-90°	24	1	21	0.2	96.8	3.1	0.097	0.094	99.06	0.11	0.12	0.20	0.14	99.75
SI220133	8340710	307902	64.5	0°	-90°	28	1	28	0.1	97.4	2.6	0.084	0.056	99.24	0.10	0.07	0.10	0.14	99.74
SI220134	8340805	307743	61.7	0°	-90°	6	No mineralisation intercepted.												
SI220134A	8340805	307743	61.7	0°	-90°	36	1	35	0.1	95.5	4.4	0.072	0.092	99.25	0.10	0.12	0.18	0.11	99.84
SI220135	8340996	307650	66.4	0°	-90°	39	1	37	0.1	97.4	2.5	0.069	0.075	99.33	0.09	0.09	0.14	0.08	99.81
SI220136	8341180	307598	57.7	0°	-90°	21	1	19	0.1	97.6	2.3	0.089	0.068	99.22	0.12	0.09	0.14	0.13	99.79
SI220137	8341147	307539	68	0°	-90°	33	1	30	0.1	95.9	4.1	0.077	0.122	98.82	0.11	0.16	0.25	0.17	99.62
SI220138	8340987	307400	45.8	0°	-90°	27	1	27	0.1	96.3	3.6	0.057	0.037	99.35	0.08	0.05	0.07	0.17	99.79
SI220139	8340895	307543	39.2	0°	-90°	9	1	9	0.5	94.8	4.7	0.061	0.048	99.30	0.08	0.07	0.14	0.15	99.84
SI220140	8340767	307622	41.4	0°	-90°	12	1	12	0.7	94.1	5.3	0.055	0.043	98.91	0.12	0.23	0.14	0.19	99.66
SI220141	8340667	307791	41.9	0°	-90°	9	1	7	0.1	97.8	2.2	0.051	0.038	99.56	0.10	0.57	0.08	0.16	100.53
SI220142	8340850	307438	54.9	0°	-90°	27	1	27	0.1	97.9	2.1	0.052	0.052	99.27	0.09	0.40	0.10	0.09	100.00
SI220143	8340997	307070	68.8	0°	-90°	42	1	42	0.3	96.9	2.8	0.062	0.060	99.36	0.07	0.07	0.11	0.11	99.78
SI220144	8340939	307143	59.6	0°	-90°	33	1	31	0.1	96.4	3.5	0.056	0.054	99.44	0.06	0.07	0.11	0.10	99.83
SI220145	8340884	307240	49.5	0°	-90°	21	1	21	0.3	96.8	3.0	0.100	0.048	99.39	0.12	0.06	0.10	0.15	99.90
SI220146	8341320	306842	37.7	0°	-90°	12	1	12	0.7	94.6	4.7	0.086	0.034	99.49	0.10	0.05	0.10	0.35	100.14
SI220147	8341281	307725	50.5	0°	-90°	15	1	15	0.2	96.2	3.6	0.082	0.085	99.20	0.10	0.12	0.11	0.23	99.83
SI220148	8340892	307953	44.2	0°	-90°	9	1	7	0.1	96.6	3.4	0.069	0.039	99.74	0.07	0.06	0.08	0.15	100.15
SI220149	8341289	307928	53.6	0°	-90°	20	1	18	0.2	97.7	2.2	0.058	0.037	99.42	0.08	0.05	0.06	0.12	99.77
SI220150	8340776	308387	46.9	0°	-90°	12	1	10	0.2	97.2	2.6	0.065	0.066	99.43	0.07	0.09	0.12	0.14	99.92
SI220151	8340519	308622	60.6	0°	-90°	36	1	34	0.3	97.7	2.0	0.060	0.037	99.64	0.07	0.05	0.05	0.16	100.02
SI220152	8340075	308907	44.5	0°	-90°	15	1	12	0.8	95.9	3.3	0.113	0.077	99.12	0.13	0.10	0.13	0.28	99.82

Collar Information							Mineralised Interval		Grain Size Fractions			<0.71mm >0.106mm Grade		Head Grade					
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Depth m	From m	To m	<0.71mm %	<0.71mm>0.106mm %	>0.106mm %	Al_2O_3 %	Fe_2O_3 %	SiO_2 %	Al_2O_3 %	Fe_2O_3 %	TiO_2 %	LOI %	Total %
SI220153	8340363	308572	35	0°	-90°	3	No mineralisation intercepted.												

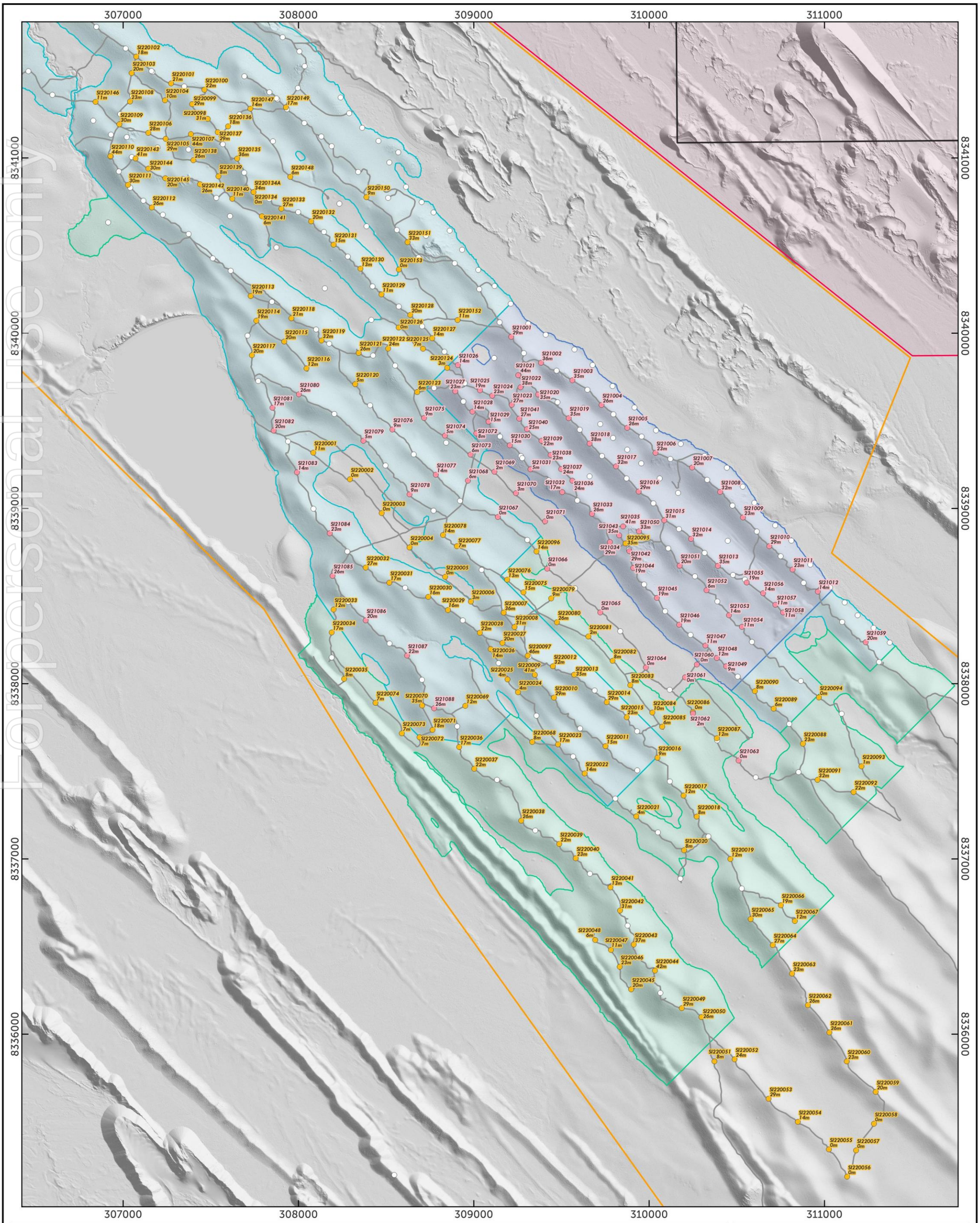
# denotes head grade results were prepared and disclosed in accordance with the JORC Code 2012, and reported in an announcement to the Australian Securities Exchange on 17 April 2024 “Mineral Resource upgrade paves way for Northern Silica Project PFS”

* Where Hole ID contains an * asterisk, the respective drillhole and mineralised interval were included in the bulk testwork program.

Note: Grainsize fractions are reported in µm by ALS Brisbane, however for market comparability, they are reported in mm in this announcement.



Macro photography of significant drillhole Si220097



2024 Drillholes

2023 Drillholes

2021, 2022 Drillholes

Exploration Permit for Minerals
Diatreme Resources

Mining Lease Application
Diatreme Resources

Mining Lease
Cape Flattery Silica Mines

Si2 Mineral Resource Estimate
Inferred Category (April 2024)

Si2 Mineral Resource Estimate
Indicated Category (April 2024)

Si2 Mineral Resource Estimate
Measured Category (April 2024)

Note: In the event not all map features are labelled, refer to the Table of Material Drillholes and Results

250 500 750 1,000 m

Exploration Results

July 2024 - March 2025

Document #: DRX_NSP_CP_8289	Scale: 1:19000
Version: 1.0	CRS: GDA2020 / MGA Zone 55
Author: Frazer Watson	Date Created: 5/3/2025
Approved: Frazer Watson	Date Approved: 5/3/2025

JORC TABLE 1

Section 1 Sampling Techniques and Data

Criteria	Explanation	Commentary
Sampling techniques	• Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. • In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	• For drillholes reported Si21001 to Si21088, Aircore drilling samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. This material was then composited into nominal 3m composites and submitted to ALS Brisbane for sieving into three fractions +710µm, -710µm+106µm and -106µm. The respective fractions were then weighed, followed with the 710µm+106µm fraction pulverised and assayed by method code ME-ICP64. • For drillholes reported Si220001 to Si220153, Aircore drilling samples were collected in 1m intervals, before being composited by scoop into nominal 3m samples (~1kg). This material was then composited into nominal 3m composites and submitted to ALS Brisbane for sieving into three fractions +710µm, -710µm+106µm and -106µm. The respective fractions were then weighed, followed with the 710µm+106µm fraction pulverised and assayed by method code ME-ICP64. In addition a sample representing the full particle size distribution was split, pulverised and then assayed by ME-XRF26. • The Competent Person considers the quality of the sampling method to be fit for the deposit style, and the stage of exploration.
Drilling techniques	• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	• Aircore drilling to refusal, which occurs at geologically determined contact such as clayey sands at the base of mineralisation, or a water table. This is due to the limitations of AC drilling at the water table, and limitations of the compressor on the AC drill rig when penetrating the clay layers. • AC drilling was by a track mounted drill rig with a 3" blade bit, and a rod length of 3m. • The Competent Person considers the quality of the sampling method to be fit for the deposit style, as mineral sands are easily contaminated, or recoveries can be poor and not representative using other drilling methods.
Drill sample recovery	• Method of recording and assessing core and chip sample recoveries and results assessed.	• Sample recovery is monitored at the rig by weighing each 1m interval to observe for the presence or deviation from a consistent sample size. • Sample recovery is maximised within a closed system from the drill bit to the riffle splitter.

Criteria	Explanation	Commentary
	• Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	• After encountering wet clays, sacrificial rods are drilled into clean dry sand, to flush out any contamination through the drilling hoses, prior to drilling the subsequent drill hole. • No relationship between recovery and grade has been observed, as the orebody is relatively homogenous. • Correct interval delineation on AC drilling is achieved with metre intervals marked on the drill mast, and samples are collected when the base of the top drive reaches a metre interval.
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. • The total length and percentage of the relevant intersections logged.	• All drillholes have been logged in their entirety, with qualitative descriptions of grain size, sphericity, roundness, moisture content, lithology, and colour recorded. • Photography is captured on a chip tray basis firstly at the drill rig, and then later on a chiptray compartment by compartment when samples have dried. • Sample photography in a controlled setting using Imago software with a Canon EOS R5 and a Canon 24-50mm lens , a hexadecimal colour value is extracted from the imagery, and the RGB values are derived through python scripts. Colour photography is verified against a Calibrite ColorChecker. • The quality of logging is sufficient for this stage of exploration.
Sub-sampling techniques and sample preparation	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled	• In 2023, AC samples were riffle split after the cyclone, and placed in sample bags representing 1m intervals. • In 2024, AC samples were scooped from the sample bags representing 1m intervals, and composited to a nominal 3m composite. The single scoop is approximately 330g in mass. • Sample preparation was completed at ALS in Brisbane. Full samples are dried at 105°C, then weighed (WEI-22g), then a split is screened (SCR-61) into three size fractions +710µm, -710µm+106µm and -106µm, with a split of the raw sample retained. A nominal 150g split of the raw sample, and a nominal 150g split of the -710µm+106µm fraction are then pulverised using a tungsten carbide ring mill (PUL-33), prior to being assayed. • Importantly, the Competent Person remarks that the -710µm+106µm does not represent “product” grade, as heavy minerals are not removed through the sieving process. • The PUL-33 method has a QC check on a 20g split to ensure >85% passes -75µm • Coarse flushes of an unpulverized sample matching ELIM22 CRM has been introduced to both clean the lab pulveriser between drillholes, and test for any contamination. ELIM22 was prepared by OREAS, specifically for ore grade material in the Cape Bedford / Cape Flattery dune systems. • A coarse flush of the raw ELIM22 sample is included after intersecting a deleterious horizon – and this is used to clean the Tungsten Carbide ring mill / pulveriser at ALS Brisbane. All samples are pulverised sequentially through the same pulveriser. • Crushing is not required as the grain size of the sample material is suitable for pulverizing. • The Competent Person considers the drill sample sizes as appropriate for the grain size of the material, the style of mineralisation and the nature of the drilling program.

Criteria	Explanation	Commentary
		• These methods are determined to be appropriate by the Competent Person to avoid sample carry-over contamination, in addition Cr2O3 is monitored to ensure that pulverisation is performed in a non-ferrous pulverising bowl.
Quality of assay data and laboratory tests	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	• ME-ICP64 is considered a partial digest, it is considered appropriate for silica sand due to the high purity of the -710µm+106µm sample, and the low detection limit for Fe_2O_3 comparative to XRF methods. • As ME-XRF26 is considered a total digest, it is considered appropriate for silica sand when assessing full sample geochemistry. • Loss On Ignition (LOI) is determined by thermogravimetric analysis (TGA) using method code ME-GRA05, where a sample is placed in a furnace at ambient temperature and then heated to 1000°C, and then weighed. • Field duplicates are conducted every 25th sample which is submitted to the lab as blind duplicate. • CRM (ELIM22) is utilised every 33rd sample • Either CRM NCS 60116a or NCS 60117a are used 2 in 100 – for samples drilled in 2024. • ALS Brisbane, and verification of CRM and field duplicate results have indicated that for the method ME-ICP64, Al_2O_3 and Fe_2O_3 are acceptable for the broader range of grades, however TiO_2 recovery is poor on lower purity samples. However recovery is acceptable for higher purity samples. For this reason, Al_2O_3 and Fe_2O_3 results are considered material and appropriate to report, while reporting TiO_2 recovery would be considered misleading. • The quality control procedures adopted by Diatreme establish an acceptable level of accuracy and precision. • The variability observed between the primary sample and the field duplicate assay results are considered appropriate for the style of mineralisation by the Competent Person.
Verification of sampling and assaying	• The verification of significant intersections by either independent or alternative company personnel. • The use of twinned holes. • Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. • Discuss any adjustment to assay data.	• The Competent Person and Diatreme Resources' Exploration Geologist have personally inspected all sample intervals. • 2 twinned holes have been completed, with minimal sampling bias observed. • Collar and geological logging is captured by and stored within the geological logging/database software MX Deposit, in accordance with company procedures. • Photographic data is captured, and stored within Imago, a software package that acts as a repository and analysis tool for geoscientific imagery. • Assay data is recorded, and stored in MX Deposit, a Drillhole Database software. • No adjustment has been made to assay data.
Location of data points	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control.	• All drill hole locations have been surveyed using Spectra Precision SP60, with a Trimble RTX CenterPoint DGPS correction ± 0.05m on the horizontal plane. • The collar data is recorded in the UTM coordinate system: Map Grid of Australia 1994 (MGA94) Zone 55, this is then reprojected to GDA2020 Zone 55 for compatibility with other spatial files. • All drill holes are shallow and vertical, no down-hole surveying is conducted. • Digital elevation models derived from LiDAR (December 2022) were used as the topographic surface to generate RL's for each collar. The DEM was generated via a cloth simulation function, using an approximate 10 ground classified points per square metre. Relative accuracy is considered to be ± 0.1m.

Criteria	Explanation	Commentary
Data spacing and distribution	• Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • Whether sample compositing has been applied.	• First pass drilling spaced nominally at 380m along dune crests, and infill drilling at a nominal 180 - 200m along the trailing arm of an elongate parabolic dune, and in the interdunal valleys, although the Competent Person considers data spacing at these intervals are not a material constraint on the development of geological grade or geological continuity, and as such, the Competent Person considers the data spacing to be more than appropriate for this style of deposit, at this stage of exploration. • Samples have been composited to nominal 3m intervals, following recommendations from a variability assessment completed by Measured Group in 2024, and also on an assessment that the 3m compositing also aligns with likely SMU's for the deposit.
Orientation of data in relation to geological structure	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	• The deposit style is an unlithified aeolian sand deposit, comprised of a series of complex parabolic and elongate parabolic dune systems which are repeatedly deflated and are superimposed upon older dune systems. • The mineralisation process (podsolisation) is gravitationally controlled. The Competent Person has determined that vertical drilling intersects the bedforms at an angle which represents the true width of mineralisation. • No sampling bias is introduced by the orientation of drilling.
Sample security	• The measures taken to ensure sample security	• Sample bags were sealed by cable-tie, and transported in polywoven bags, then securely stored in a locked yard on-site until transported by courier to ALS in Brisbane. • Transport chain of custody forms have been reviewed for each sample dispatch. • Submission reconciliation reports are provided by the laboratory and checked against the sample submission forms.
Audits or reviews	• The results of any audits or reviews of sampling techniques and data.	• Internal reviews by Diatreme staff on both the drillhole database and sampling techniques have been conducted, indicating compliance to internal standards. • No external reviews have been completed at this stage.

Criteria	Explanation	Commentary
Mineral tenement and land tenure status	• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. • The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	• These Exploration Results comprise exploration on the Si2 Deposit, which is the mineral resource within the Northern Silica Project, which is located adjacent to the coastline in Far North Queensland, approximately 53km north of Cooktown. The project is adjacent to the south of the Cape Flattery Silica Mines (CFSM) Mining Lease. CFSM has been in operation since 1967 and is Queensland's largest producer of high purity silica and is reported to have the highest production of high purity silica sand of any mine historically. • The project is located at the northern end of the Cape Flattery/Cape Bedford dune field complex within the Exploration Permits for Minerals (EPM) 17795 & 27212. • Most of the EPM, and the entirety of the Si2 Deposit is located on one land title, Lot 35/SP232620, a freehold lot of 110,000 hectares. • The Project and EPM is in the Mareeba Mining District and falls within the Hope Vale Aboriginal Shire Council area. This lies approximately 35km north of the township of Hope Vale, with a population of approximately 1,500 in the Hope Vale Aboriginal Shire Council. • EPM 17795 is owned by Northern Silica Pty Ltd, a wholly owned subsidiary of the Joint Venture Cape Silica Holdings Pty Ltd between Diatreme Resources 73.2% and Sibelco Silica Pty Ltd 26.8%. • Diatreme was granted a renewal on EPM 17795 "Cape Bedford" until 21 June 2026 on the basis of continued targeting of heavy mineral sands and silica sand. The EPM was granted under protected Native Title Protection Conditions. As of March 2025, the tenure is in good standing. • EPM 17795 is an extensive EPM comprising 147 continuous subblocks (approximately 480km2) covering the majority of the Cape Flattery-Cape Bedford Quaternary dune field complex. • Three EPM's contiguous with EPM 17795 have been taken up by Diatreme, EPM 27212 (granted 27th September 2021), EPM 27265 (granted 30th January 2020, and currently in renewal) and application EPM 27430 (granted 26th October 2021). These tenements cover small areas of the dune field not covered by EPM 17795. EPM 27212 is held by Cape Silica Holdings Pty Ltd, EPM 27430, EPM 27265 are held by Northern Silica Pty Ltd. • An additional EPM 25734 also targeting silica sand was acquired by Diatreme through a takeover of Metallica Minerals in 2024. • Cape Silica Holdings and its subsidiaries have two mining lease applications currently undergoing approvals, ML100235, ML100308, and four accompanying mining lease infrastructure applications, ML 100310, ML 100311, ML 100312, ML 100313. Casuarina Silica Pty Ltd, a subsidiary of Diatreme Resources has a mining lease approval underway (ML100309).
Exploration done by other parties	• Acknowledgment and appraisal of exploration by other parties	• Exploration for silica sand has been undertaken in the Cape Flattery – Cape Bedford area in 11 Authorities to Prospect (ATP's) or Exploration Permits for Minerals (EPMs) since the 1960's. In general, past exploration of the dune field has primarily focused on the prominent active parabolic dunes of clean white silica sand. • Historical exploration activities appear to have missed the Si2 Deposit in it's entirety, until discovery by Diatreme Resources in late 2021. • As there are no assay certificates for this historic data, and the locations of which are dubious, the data is considered qualitative and is not used for Mineral Resource Estimation, or Exploration Targeting.

Criteria	Explanation	Commentary
Geology	• Deposit type, geological setting and style of mineralisation.	• The Northern Silica Project is comprised of unlithified aeolian dune complexes. • The Cape Flattery & Cape Bedford dune fields are aeolian dunes established in the Pleistocene epoch and regularly remobilised during the Pleistocene and Holocene epochs. The dune fields are situated on a coastal plain overlying the Hodgkinson Formation basement with Dalrymple Sandstone forming mesa on basement highs. • Mineralisation is thought to be due to repeated eluviation and illuviation events on immobilised dune systems comprised of an existing quartzose sand source, with reactivated dune systems also exhibiting mineralisation. Intradunal valleys tend to be a surface expression of the B1 horizon, and typically are not considered mineralised. • Deleterious metals are thought to have been eluviated by organic acids, which are transported by gravity through the stratigraphic column and illuviated either by binding to clay rich horizons, or transported away from the deposit through the water table.
Drill hole Information	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: ○ easting and northing of the drill hole collar ○ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ○ dip and azimuth of the hole ○ down hole length and interception depth ○ hole length. • If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	• All material collar information for drillholes has been aggregated in the Table of Material Drillholes and Results attached in this appendix to the announcement.

Criteria	Explanation	Commentary
Data aggregation methods	• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated.	• Data aggregation used in this report is a calculation of the mean average for each reported variable across the respective mineralised profile for that drillhole. • All intercepts have been aggregated in the Table of Material Drillholes and Results attached in this appendix to this report.
Relationship between mineralisation widths and intercept lengths	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	• All drilling was vertical (-90°) intersecting undulating flat-lying aeolian dune sands. • Downhole length correlates with true width of mineralisation.
Diagrams	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported • These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	• Plan view of drill hole collar locations and appropriate are within the announcement, and a higher resolution image is within this appendix.

Balanced reporting	• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results	• All mineralised silica sand results are reported.
		• Where the results in the table are not published, the intervals are considered either
		  ○ Not mineralised (podsolisation process was immature)
		  ○ 0m to 1m interval – topsoil has not been assayed.
		  ○ B1 sands / sandy clays below the mineralised horizon.

Criteria	Explanation	Commentary

Other substantive exploration data	• Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	• Fe_2O_3 percentage is the most significant limiting factor on conversion of ore to high purity silica sand product and determines value after SiO_2 percentage.
		• Fe_2O_3 when found in association with TiO_2, does not act as a contaminant or barrier to refining high- purity silica sand, with metallurgical testing showing gravity separation to accurately remove this impurity.
		• Colour (oranges, yellows, reds) tend to be a significant - but not limiting – indicator on the identification of deleterious or low yielding sands.
		• For the 1t bulk sample, a nominal 850g was composited from each of 1147 intervals drilled in 2023 selected to represent the Measured Category of the Si2 Mineral Resource. The relevant drillholes and intervals are included in this Appendix in the Table of Material Drillholes and Results.
		• Metallurgical testwork was performed at MT Carrara.
		• Geochemical results were performed at ALS Brisbane using ME-XRF26 for head grade & lower purity samples, and ME-PKG85 for higher purity product samples. ME-PKG85 and ME-XRF26 are considered a full digest.
		• Metallurgical testwork was performed at MT Carrara, and consisted of:
		  ○ Receiving a 1t bulk sample,
		  ○ Sample homogenisation, and then sub sampling 5kg of feed material.
		  ○ Sieving and retaining the -1mm+0.045mm product stream
		  ○ Sieving and retaining the -0.710mm+0.106mm product stream sample
		  ○ Undertaking a Heavy Liquid Separation using Bromoform and Acetone to achieve a SG of 2.7 (This is a benchtop scale testwork method to simulate the gravity separation process)
		  ○ The 2.7 SG floats are then attritioned for 5 minutes with 75% solids without any reagents
		  ○ The material is then wet sieved at 0.106mm, with the oversize fraction then passed through two reading IRMS units at 3.0A, 11500 Gauss and 8.0A and 18000 Gauss, respectively. Both with a Pole Gap of 4mm and a Roll Speed of 140rpm.
		  ○ The Non Magnetic fraction is then considered representative of final product for this stage of study.

Criteria	Explanation	Commentary
Further work	• The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). • Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	• The Competent Person recommends the following programs to increase geological confidence on the deposit. ○ Undertake sizing analysis and ICP (or other suitable low Fe_2O_3 detection limit assay) on samples from 2021 & 2022 programs, and maintaining this on future drill programs. ○ In particular, the B1 horizon needs to be checked and tested in the interdune locations by drilling, or geological observations with hand augering to assist better defining geological continuity and support potential upgrade areas. ○ Further study stages may require an improved understanding of environmental and cultural constraints (currently being identified through an EIS) relevant to the development of the deposit. ○ Maintain regular certified bulk density measurements in future drill programs. ○ Complete mineralogical analysis on Fe bearing minerals (such as surface coats, and inclusions) within the silica sands, and with respect to the relevant size fractions. ○ Establishment of a geometallurgical model to underpin the relationship between head grade and amenability to processing. ○ Submission of samples for umpire checks and bulk density assessment, is underway. ○ Testing of lateral extensions of the deposit toward the Southeast ○ Geochemical analysis of the +710µm and -106µm fractions