ASX ANNOUNCEMENT
11th June 2025

6.43 Mt @ 1.07% Cu JORC MINERAL RESOURCE ESTIMATE FOR ICE COPPER-GOLD PROJECT

HIGHLIGHTS:

- **New JORC Code (2012) re-estimation CONFIRMS the original foreign historical resource tonnage and grade for the ICE Copper-Gold Project, Yukon Territory, Canada**
- **Indicated resources of 5.76 Mt @ 1.09% Cu and Inferred resources of 0.67 Mt @0.83% Cu at a 0.3% cutoff**
- **Outcropping mineralisation potentially amenable to open pit extraction**
- **Resource covers 115 drill holes, almost entirely <200m deep, with 92% of resources classified as INDICATED**
- To date, **less than 1% of the Project area has been drill tested** – multiple geochemical and geophysical targets provide potential for discovery of additional mineralisation zones
- **11 priority targets have been identified, with potential for future discovery of additional zones of VHMS mineralisation** near the resource and through the properties[1]
- VHMS deposits often occur as clusters and the available geochemical and geophysical evidence from ICE supports the potential presence of additional deposits

Bastion Minerals Ltd (ASX:**BMO, Bastion** or the **Company**) is pleased to announce a JORC Code Mineral Resource Estimate (**MRE**) for the Company's flagship high grade ICE Copper-Gold Project[2] (**ICE Project** or **Project**) located in the Yukon Territory, Western Canada.

Commenting on the new ICE Project JORC MRE, Bastion Chairman, Mr Gavin Rutherford, said:

"It is a great result to announce a JORC Code MRE for the ICE Copper-Gold Project in Canada. The new JORC MRE not only confirms the copper contained in the original 1998 foreign historical estimate but also demonstrates the potential to add substantial, additional value from the gold, cobalt and minor silver and zinc in the deposit., which were not included in the original estimate.

---

[1] Refer ASX Announcement 2nd December 2024, "11 Exploration Targets Identified – Ice Project, Canada Targeting New Discoveries & Resource Expansion"

[2] Refer ASX Announcement of 30 July 2024. The acquisition of the ICE Copper Project was approved at an Extraordinary General Meeting of shareholders held in mid-October 2024 and completed on 18 November 2024.

With mineralisation beginning at surface, the potential for open-pit extraction is clearly demonstrated.

"One of the many exciting features of the ICE Project is that detailed exploration to date has only been concentrated on the ICE deposit. We therefore have huge potential for additional mineralisation along strike and at depth from the known mineralisation, given drilling to date covers less than 1% of the entire Project area. There are 11 exploration targets already defined within the Project, which as yet have had no follow-up exploration. Excitingly, reprocessing of the original ground-based electromagnetic (EM) survey has highlighted the presence of untested conductors to the NNE and SSW of the ICE deposit.

"This means we see significant exploration upside at the ICE Project, with less than 1% of the project area drilled outside of the resource. The 11 targets already defined by the Company represent potential to discover new mineralised lenses adjacent to known mineralisation or as entirely new deposits. VHMS deposits cluster on a local level and in broader camps of mineralisation, such as in the Kudz ze Kaya district, 80 km east-southeast of ICE."

Table 1. *New JORC (2012) Mineral Resource Estimate for ICE Copper-Gold Project at a 0.3% Cu cut-off*

Class	Cut-off	Mt	Cu %	Au g/t	Ag ppm	Zn %	Co %	Kt Cu
Indicated	Cu 0.3%	5.76	1.09	0.09	2.9	0.11	0.018	62.8
Inferred	Cu 0.3%	0.67	0.83	0.10	2.9	0.09	0.018	5.81
Total	Cu 0.3%	6.43	1.07	0.09	2.9	0.11	0.018	68.6

Project Background

The ICE Project (**Figure 1**) was discovered from follow-up of a highly elevated stream sediment sample in 1996 and the deposit was subsequently drilled during 1996 and 1997. The deposit outcrops, with a zone of oxide mineralisation in the northwestern up-dip part of the deposit. Mineralisation is hosted in a sequence of submarine basalts and brecciated basalts, with intervals of chert and mudstone.

The mineralisation is noted to be hosted with a unit of porphyritic basalt. Mineralisation has been located by drilling and in a ground HLEM survey together with a helimagnetic survey over the property. Two principal conductors were identified in the ground HLEM survey, although it appears there maybe three or more conductors present in the mineralised zone, which trends NNE and have not been fully tested by drilling.

Mineralisation consists of massive sulphide, with disseminated pyrite and interstitial chalcopyrite. The more massive sulphide unit extends as a body down dip to the SE, surrounded by lower grade and more disseminated mineralisation. In addition to this down dip extension of the highest grade mineralisation, there is a NNE extension of mineralisation, which is evident in the block model built from the original assay information.

Low grade mineralisation may extend to the SSE, whereas in the north the high grade mineralisation was not completely closed out. Correlation with the HLEM geophysics data suggests that the original mineralisation continues north of the resource and block model, and is likely to lens-out, with the potential for at least one additional lens to develop further north of the existing mineralisation. To the south there are several highly conductive zones, which are targets for future drilling.

Available Information from Historic Exploration

The ICE Project has a significant amount of historical information available, including:

- Soil sampling across the Project at variable sample density, but majority as grid data.
- A ground HLEM survey, which was conducted over the deposit, but shows what is interpreted to be a continuation of the deposit to the north and to the south, which has not been drilled. There is also interpreted continuation of the conductors coincident with the deposit to the NE and possibly to the east on the edge of the survey.
- A property-wide helicopter EM survey, which identified the deposit and a number of untested HeliEM targets, of which the majority are located along trend from the HLEM survey to the NNE of the deposit.
- A total of 121 diamond drill holes of which 115 were drilled into the deposit. The other holes were drilled off to the southwest of the deposit on what appear to be a combination of geochemical and geophysical targets. Discussion with Aurora Geoscience geophysicist indicates that the drilling on the HLEM targets has not tested them effectively. Diamond holes were almost all less than 200 m depth and drilled from the southeast to northwest, across what is interpreted to be the dip of the deposit, which appears supported by the geology and geophysics.
- 275 density samples from the original hydraulically split core.
- An additional 48 measurements were collected by Aurora Geoscience, using the displacement method. Cores were not coated in wax, as they are generally quite solid and competent.
- An additional 38 measurements were made on pulps from cores that were selected from the re-assaying program. These corresponded to the majority of the samples conducted by Aurora. The majority of results were very similar but 10 of the samples showed significant differences.
- Overall summing the 275 original samples and 48 additional samples, there are 323 samples throughout the deposit.
- Not all samples were originally assayed for gold. Of the 2,594 samples from the drilling, only 449 samples were analysed for gold. All re-assayed core was analysed for gold and a broad suite of elements.

Property Position

In the Yukon, properties are held as alluvial (surficial) or quartz (hard rock) property claims. The ICE Project consists of 260 standard quartz claims covering an area of ~56 km^2. Properties are shown in ***Figure 1***. The properties cover the prospective area of basalts, with an area of felsic volcanics in the southern block of properties, which cover geological units more similar to those hosting the Kudz ze kaya mineralisation.

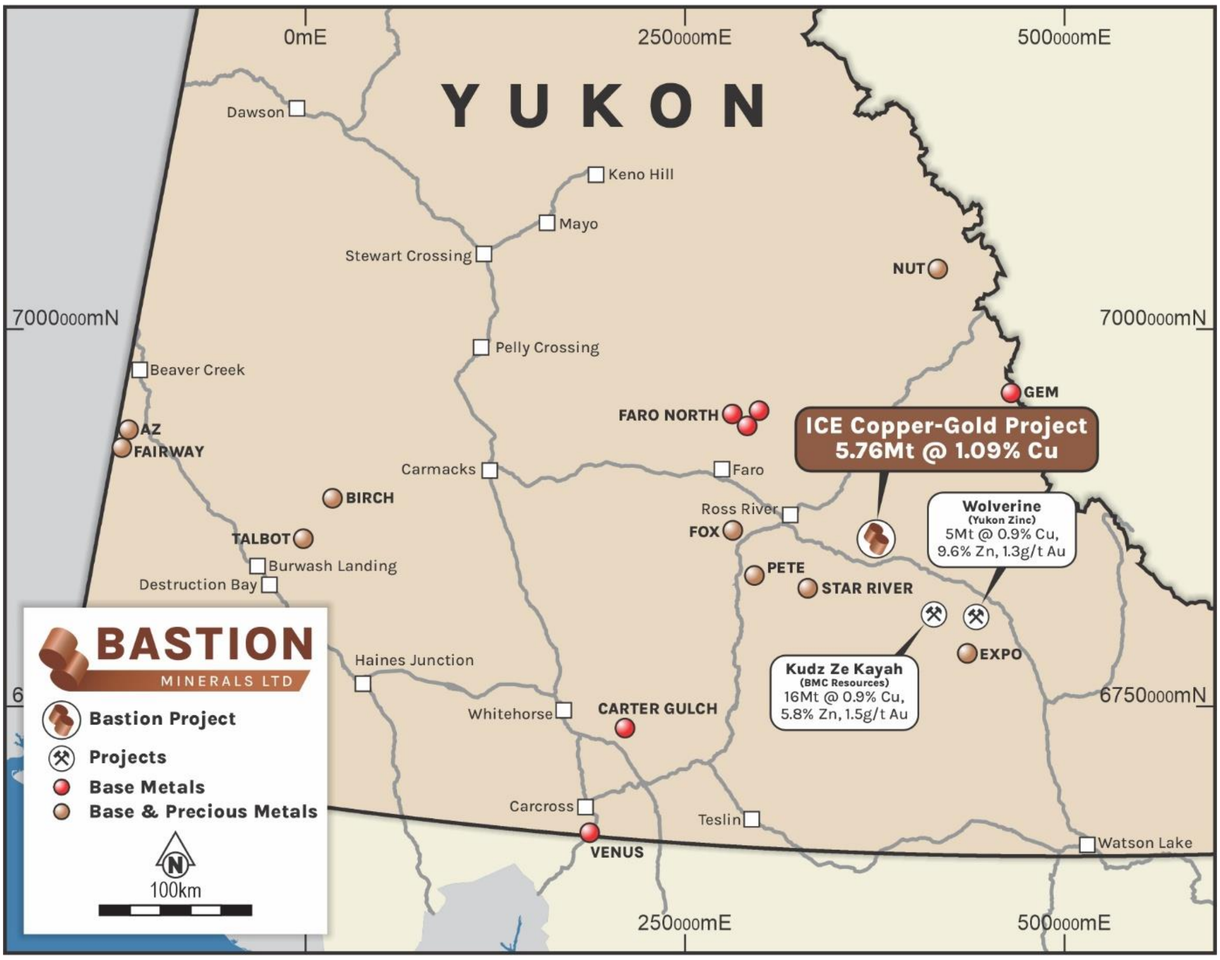

Figure 1: Project location in the south of the Yukon Territory, showing Indicated Resource tonnage

Regional Geology

The ICE Project is located in the Slide Mountain Terrane (**Figure 2**), interpreted as a paleo-oceanic sequence of mafic volcanic rocks adjacent to the Yukon-Tanana Terrane in the Finlayson Lake district, Yukon. These terranes represent arc–back-arc systems that formed adjacent to the Laurentian continental margin of North America in the mid-Paleozoic.

The Slide Mountain Terrane is mafic dominated (**Figure 2**), while the Yukon-Tanana Terrane is more felsic (**Figure 2**). These terranes are stacked onto the western margin of North America and are bounded by the Jules Creek Fault, which parallels the Robert Campbell highway through the area. The Yukon-Tanana Terrane ranges in age from upper Devonian to Lower Permian, whereas the Slide Mountain rocks range from lower Carboniferous to upper Permian. The former consists of a number of fault bounded panels, hosting VHMS mineralisation.

The lower part of the Slide Mountain Terrane consists of metasedimentary and metavolcanic rocks of the Fortin Creek Group, which are present in the southern property block of the ICE project. This unit is composed of cherts, argillites, conglomerates to grits and limestones. This unit is unconformably overlain by Middle Permian mafic metavolcanic rocks and metasedimentary rocks of the Campbell Range Formation (**Figure 2**, from Manor et. al., 2022).

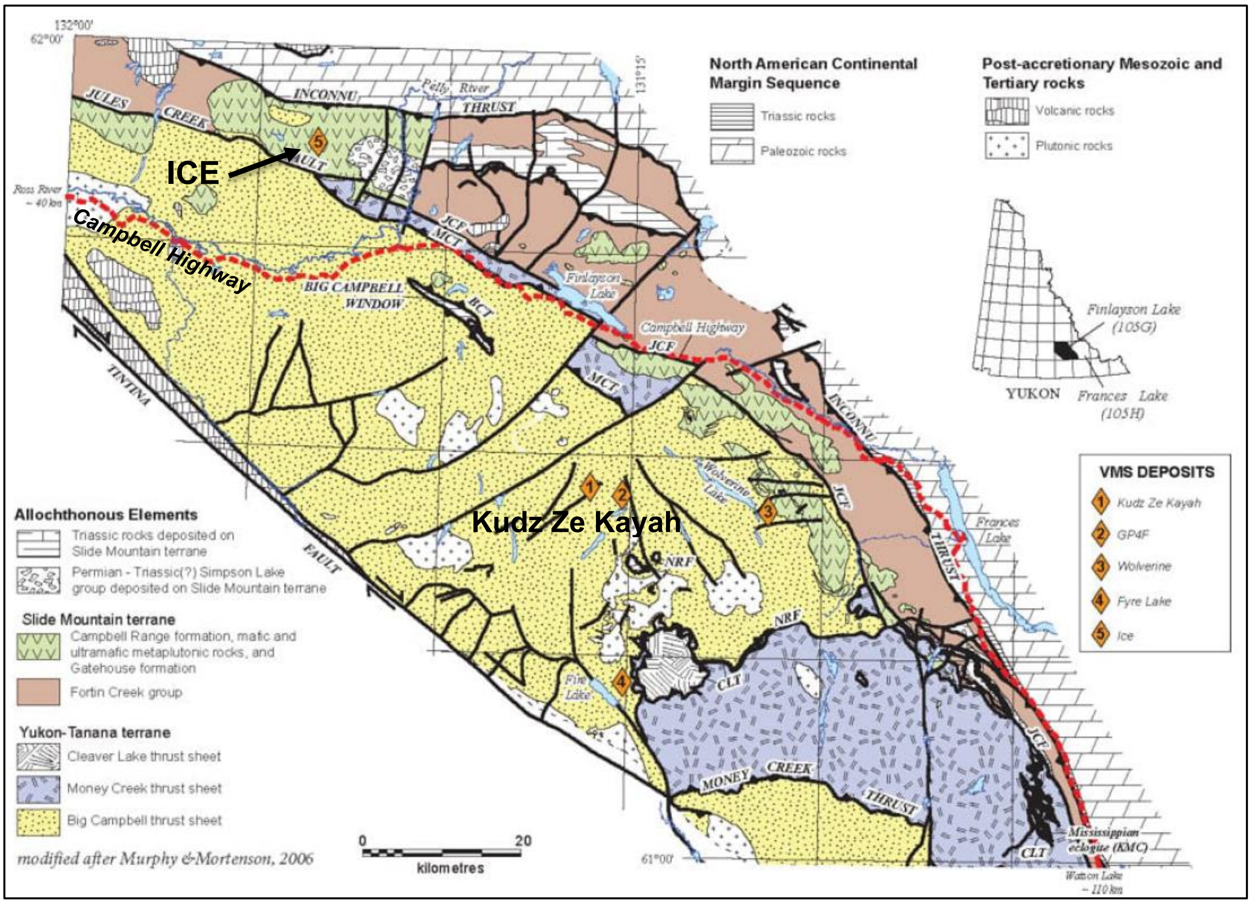

__Figure 2:__ Geological map of the Finnlayson Lake District, with the Slide Mountain Terrane, in tan, in the north and the Yukon-Takana Terrane in yellow and blue grey to the south. Note the locations of the VHMS deposits, shown as diamonds. After BMC Minerals, 2019.

VHMS Mineralisation

The Slide Mountain Terrane contains the Middle Permian ICE mafic VHMS deposit, which is interpreted to form in a back-arc basin to mid-ocean ridge tectonic setting (Plint and Gordon, 1997), Piercey et. al., 2012; McDonald et. al., 2018. Back-arc rocks can contain many large and high-grade volcanogenic massive sulphide (VMS) deposits (Manor et. al., 2022). U/Pb ages for subvolcanic gabbroic rocks considered to be similar to the volcanics range from 273 to 274.3 Ma, which is considered to be the approximate age of the ICE mineralisation.

The Finlayson Lake district is the most stratigraphically intact segment of Yukon-Tanana terrane rocks in the northern Cordillera and has been known to contain VHMS deposits, since before the mid-1990s (Hunt, 1996; Hunt, 1997; Murphy, 1998), when major discoveries were made, along with that of ICE in the adjacent Slide Mountain Terrane.

Exploration in the Yukon-Tanana Terrane has resulted in the discovery of >40Mt of polymetallic ore, including the ~19.1 Mt Kudz Ze Kayah, ~1.5 Mt GP4F, ~10 Mt Kona, and 6.2 Mt Wolverine VMS deposits (Green, 2017; Peter et., al., 2007; van Olden et. al., 2019) These formed as an evolving arc–back-arc system between ca. 366Ma and 345Ma (Devine et., al. 2006; Murphy et. al., 2006; and Piercey et., al., 2008).

Rocks that comprise Yukon-Tanana terrane arc and back-arc assemblages are variably deformed and metamorphosed volcanic, plutonic, and sedimentary rocks that locally retain primary geological and geochemical characteristics; these rocks were deposited or intruded above a pre- to Late Devonian basement (Murphy et. al., 2006).

The Jules Creek transform fault juxtaposes the Yukon-Tanana terrane adjacent to rocks of the Slide Mountain terrane (Murphy et. al., 2006), which were then together thrust above North American platform units along the Inconnu Thrust in the Late Jurassic to Early Cretaceous (Murphy et. al., 2002. Thurs faults in the Finlayson Lake district are interpreted as synthetic faults to the Inconnu Thrust.

The felsic siliciclastic ~1.5Mt GP4F and bimodal-felsic ~18.1Mt Kudz Ze Kayah Zn-Pb-Cu-Ag-Au deposits are hosted in felsic volcaniclastic rocks approximately 4km laterally and ~500-600m stratigraphically apart (**Figure 4**; Manor et. al., 2022; Peter et al, 2007).

Geology and Geological Interpretation - Property Geology and Stratigraphy

The ICE project is hosted in a brecciated porphyritic basalt, within a sequence of basalts, mudstones and cherts (**Figure 3**). Mineralisation in the ICE deposit is predominantly copper, with accessory gold and cobalt and only traces of silver and zinc. The previous foreign resource estimate did not include the value for elements other than copper.

The ICE deposit is hosted in basalts, however, there may be potential for mineralisation to be developed in sedimentary horizons, such as mudstones, in addition to in basalts, providing potential for multiple styles of VHMS mineralisation within the property.

In the relatively massive geological units the definition of dip and strike was predominantly from outcrops of chert and mudstone. These define a fairly consistent dip to the southeast at around 45 degrees, although the northwest outcropping part of the deposit may have a shallower dip.

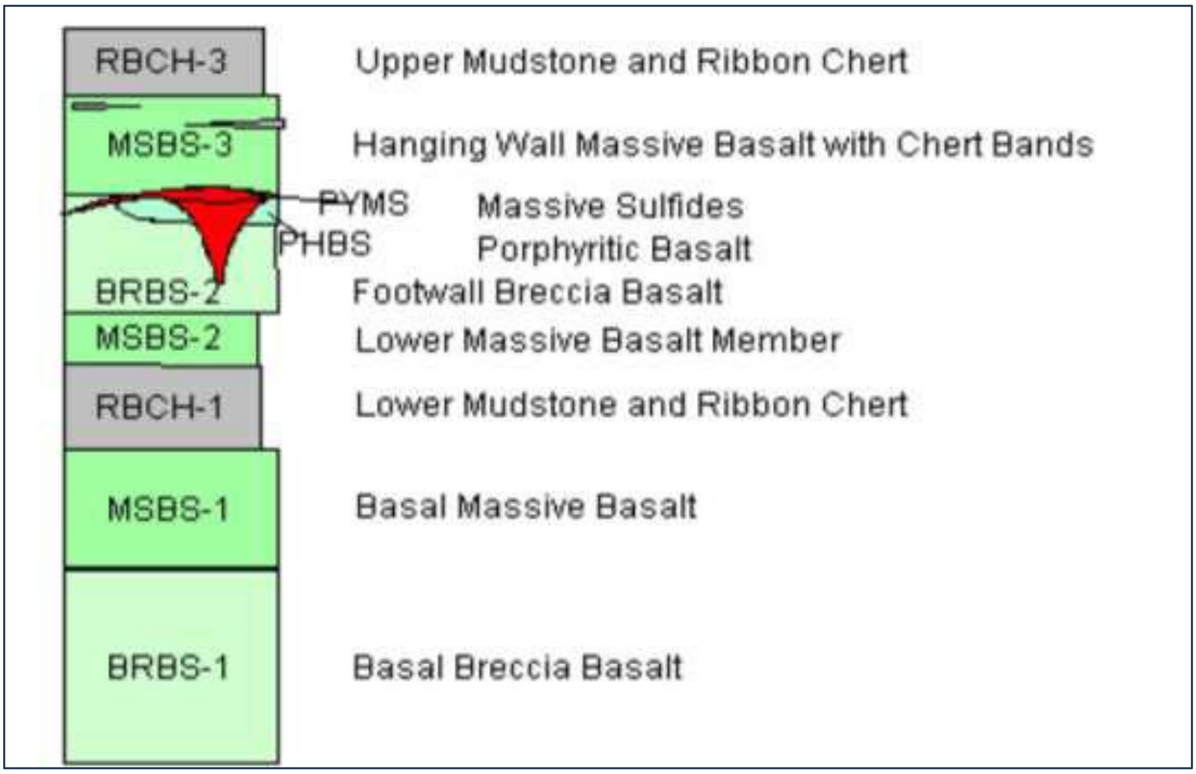

Figure 3: *The deposit stratigraphy as recognised by Expatriate resources in 1996-1997. Note the position of the PYMS massive sulphide unit at the top of the porphyritic basalt unit PHBS*

There were multiple faults mapped, although these are likely to be defined to accommodate differences in location between units and it is unclear what evidence there is at surface for the interpreted faults. Consideration of faults is important, considering the possibility of multiple cycles of volcanic stratigraphy which are very similar.

The geological logging described a large number of geological units. These were simplified to fit the previously defined stratigraphy for the deposit area. Mineralisation is strongly associated with what is described as a porphyritic basalt unit and the massive sulphide mineralisation is present at the top of this unit. Units are labelled from the base of the known sequence upward

Structural Geology

The geological sections present in historical PDF reports showed a number of interpreted faults. The most prominent of these is referred to as the Baseline Fault, trending NNE through the deposit, along the baseline for the local grid.

The historical structural geology interpretation consisted of three faults trending NNE through the deposit and three faults trending NW, essentially at a right angle to the NNE faults. The interpretation was of the NW tending faults being cut by the NNE tending faults.

Evaluation of intervals described as faults in 3D showed the NNE trending “Baseline Fault” (the most north-westerly of the faults interpreted in this orientation), corresponds to a strong number of described fault intersections and has a high probability of existing as defined. This fault appears to have relatively minor offset, which may be down to the southeast sense of movement but also have a minor strike slip offset.

The other two NNE trending faults to the SE were not included in the geological model, as are considered to be of lower confidence, although there could potentially be a fault in this ENE orientation dropping the chert and mudstone unit down to the SE in the NE corner of the deposit.

In the historical data faults were part of the lithological description, rather than as separate descriptions of faulting/structural geology. Therefore, it was necessary to create a separate field for fault intervals in the logging data, in order to represent both structural geology and lithology in the 3D model.

ICE Mineralisation

The geology consists of a number of massive and brecciated basalt layers and overlying mudstones with chert (**Figure 3**). The mineralisation is described as being spatially associated with a porphyritic basalt unit. Although the deposit is classified as a Cyprus style VHMS deposit, due to the occurrence of mudstones in the basalt sequence there could be potential for mineralisation in the mudstone units, which would be more Besshi style mineralisation.

Mineralisation appears to be strongly associated with the porphyritic basalt unit. Mineralisation outcrops in the NW of the deposit, pinching out down dip towards the SE. There is potential for additional lenses of mineralisation to continue to the NNE and the SSW. HLEM and Heli EM suggests a continuation of EM targets in both these directions (**Figure 4** and **Figure 5**).

The soil sample results to the SSE (**Figure 5**) may represent other lenses of mineralisation at deeper levels in the stratigraphy, or down valley transportation of surface mineralisation from the outcropping deposit.

Additional exploration is recommended to the NNE and SSW in particular, to evaluate possible extensions of mineralisation. There may be mineralisation at multiple levels within the stratigraphy. There is the possibility mineralisation could be developed in mudstone units, in addition to the basalt units.

The majority of mineralisation is described as massive sulphide style mineralisation, which appears to correspond to one dominant horizon. In a local area beneath the deeper part of the deposit there is a zone described as stringer mineralisation underlying the massive sulphide and having a much more limited spatial distribution. This is likely to have been a feeder zone for mineralisation in the massive sulphide horizon.

The distribution of geochemistry in the ICE Project suggests there are multiple horizons with elevated geochemistry, although there is a major mineralised trend NNE through the deposit.

Oxidation State

The historical geological logs did not clearly define the oxidation state of the mineralisation at different depths and there was no specific column in the historical geological logging to describe the oxidation state (recent glaciation in Canada means most deposits have limited oxidation).

Consequently, it was necessary to review the geological logs and, based on descriptions and the minerals noted, to assign the oxidation state for intervals of each hole. Material was described as oxidised, transitional or fresh. Mineralisation on the NW side of the deposit, where it outcrops and mineralisation is closest to surface, is the most oxidised. To the southeast of the interpreted Baseline Fault mineralisation is deeper and is all fresh.

Oxidised material is described as completely oxidised, with no sulphide minerals. Transitional consists of combined oxide and sulphide material and includes fracture and patchy oxidation. Fresh material is fully fresh, with sulphides described.

Drilling Techniques - Historic Drilling

Diamond holes were the only type of drilling conducted, with almost all less than 200 m depth and drilled from the southeast to northwest, across what is interpreted to be the dip of the deposit, which appears supported by the geology and geophysics. Holes were drilled on ~50m spaced section lines with an azimuth of ~305°; holes were generally drilled either vertically or dipping ~50° to the northwest (**Figure 6**).

Of the 121 historical diamond drill holes, 115 were drilled in the deposit (**Figure 6**). The other holes were drilled off to the southwest of the deposit on what appear to be a combination of geochemical and geophysical targets. Discussion with Aurora Geoscience geophysicist indicates that the drilling on the HLEM targets has not tested them effectively.

Holes were located on a local grid when drilled and are recorded in historical data with local grid and UTM coordinates. For the resource estimate the historical coordinates were converted to the current Yukon grid system.

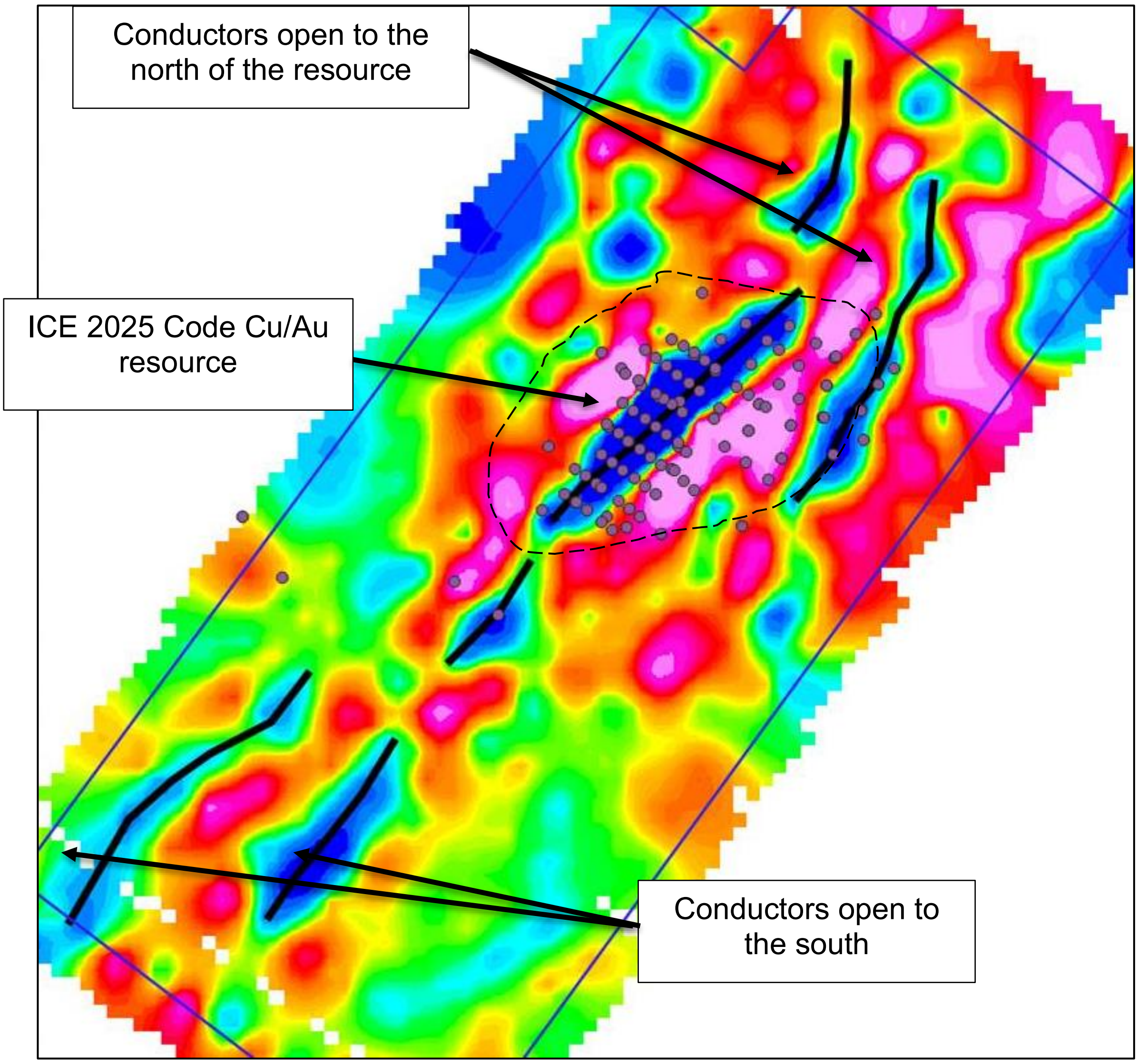

Figure 4: *HLEM ground-based electromagnetic geophysical data and 3520 Hz conductivity data, with the conductive zones interpreted to reflect mineralisation shown as blue in the image, with a black line showing the summary trend of the conductive zone*

Drilling was undertaken in with HQ and NQ diamond core. A site visit by Bastion personnel in September 2024 confirmed that the drill core from the 1996 and 1997 programs is stored on site as stacks of core trays with lids or as core trays in core racks.

Core was found to be generally well organised, with sampling intervals marked by aluminium tags and flagging tape. Core storage was catalogued when on site, for ease of core retrieval. It was noted that only the obviously mineralised intervals were cut and assayed.

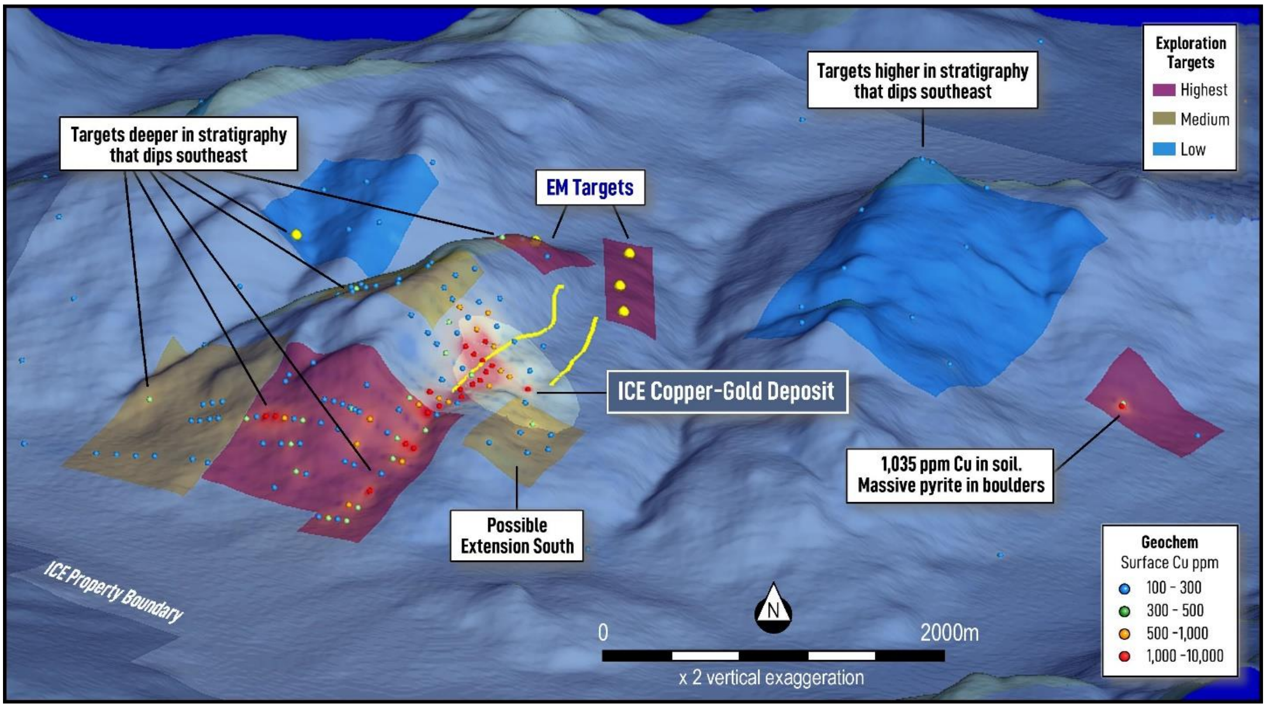

Figure 5: *Soil geochemistry and EM targets through the ICE property. The yellow lines representing the ground HLEM survey and the yellow dots representing conductors detected in the heli EM survey are untested by drilling outside the resource and may represent non-outcropping copper mineralisation. Soil geochemistry to the west of the deposit may represent mineralisation in basalt or sediment layers stratigraphically below the unit hosting the resource. Note the figure has 2 X vertical exaggeration*

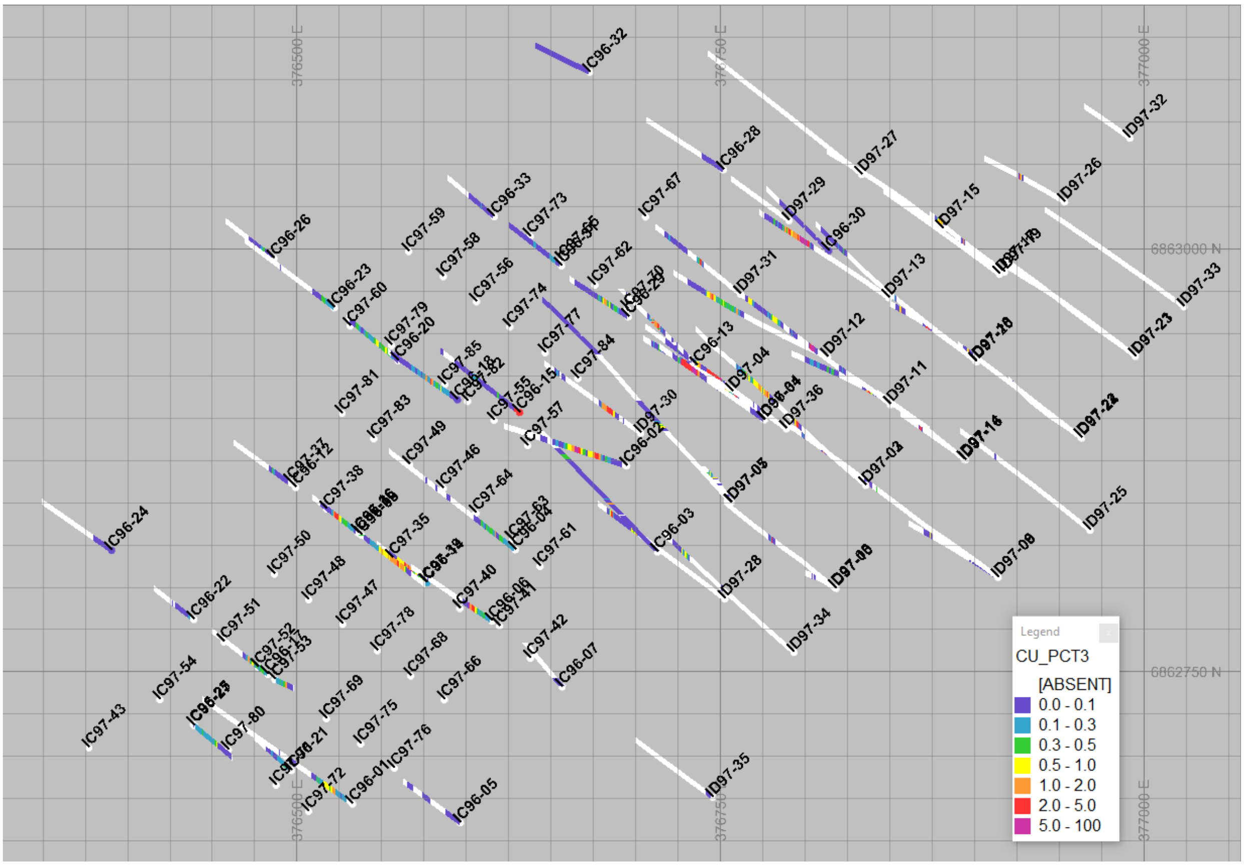

Figure 6: *Drill hole location plan, with copper intervals and grades*

Validation of collar and survey data

Planned drill collar coordinates and collar details were available in different Excel or PDF files in information made available to Bastion. Historical images provided dip and azimuth information that was validated with collar coordinates, azimuth and dip provided on the scanned drilling logs. These contained the survey information at different depths from historical “single shot” survey equipment.

This information was collected and compiled in Excel into a new collar and survey spreadsheet that has been used to develop the 3D model and was compared with historical maps and sections with drill traces. This information appears to be consistent with the cross sections that were available in a pdf file from the original sectional resource estimate. The cross sections were georeferenced in the Leapfrog model to check this. This collar and survey information has been used as the basis for the resource estimate.

During the site visit to view and catalogue the core a selection of holes from the 1996 and 1997 drilling campaign were located on the ground, with the historical drilling coordinates converted from the local grid to UTM coordinates. The drill holes were found to be within approximately 3 m of the converted coordinates (considered to be within GPS error) and in the position consistent with the location of the roads and drill pads that were established at the time.

The collars are interpreted to have originally been surveyed with a Nikon DTM-A20 total station, to provide accurate coordinates. The drill rig is believed to have been relocated by skid and by helicopter during the program. The position of tracks and drill pads from the original work was validated within the area reviewed, during the field visit.

H&S Consultants (HSC) independently projected the collars onto the topographic surface provided, which was used as collar elevations for the MRE. Future activities should include obtaining a high resolution DEM for the project and conducting on-site surveying to confirm the elevations and location of all collars.

One down hole survey was removed from hole ID97-01 at 65.63m because the azimuth (344°) was at variance with adjacent records (310° and 300°). Three other holes had potentially excessive deviation, but these were less obvious and left unchanged.

Sampling and Subsampling Techniques

Cores were collected in trays and were later split by pressure splitter to collect a sample for assay, with the remaining 50% of the core remaining in the tray. The majority of assay samples have a length of 1.52/1.53m, which is equivalent to 5 feet in imperial measurements used at the time of drilling. There are other peaks corresponding to other integer numbers of feet. The core was not subsampled at the time of the original assays.

Subsampling was undertaken as part of the validation assay sampling, when core segments over 1 m intervals (marked by the original flagging tape and sample tags remaining in the core trays) were saw cut, with one half of this core (effectively a quarter of the original core) sent for assay from a selection of intervals and the other quarter remaining in the trays for reference.

Sample Analysis Method and Validation of Assay Data

No original laboratory excel assay report sheets are available for the project. The assays are however available in excel sheets that were previously compiled for each hole and were compiled into a combined project spreadsheet for the project. A significant portion of the soil samples and core assay sample results from what was Chemex Laboratories (now part of ALS) are available in a composite PDF report prepared for the project.

These assay results from the PDF sheets were visually checked against the results provided by the project vendor in Excel format and were found to be consistent, such that they are considered to be dependable for the purposes of resource estimation.

Note that there were not field duplicates or certified reference materials (standard samples) used in the original assay program, so there was no QA/QC of the analyses used to create the original resource model.

In the original 1996-1997 drilling and sampling program samples were analysed for a broad range of elements by ICP (original prep method 205 and method number 294), with over-range assays analysed by an ore-grade method (lower limit 0.01%). The same approach was used with the samples of the re-assay program undertaken in late 2024.

Unfortunately, gold was not analysed systematically through the sampling program and only 805 of the 2,594 samples (which only correspond to intervals of core analysed, but not all core drilled) were analysed for gold, with an apparent preference for analysing higher grade intervals of massive sulphide. Gold was analysed by Fire Assay and Atomic Absorption (prep code 244).

Because there is potential economic value in the gold (and cobalt, with less significant zinc and silver) as a by-product, the recent re-estimate included all potentially economic elements, including gold. In addition to the copper only estimate presented in this announcement these elements were used to calculate a copper equivalent value. The copper equivalent value is not included in this announcement, as insufficient metallurgy has been undertaken to provide information regarding the likely recovery of the other elements into a concentrate. The silver is unlikely to provide additional economic value, with only 55 samples > 10 g/t and a maximum value of 62 g/t. The correlation of gold and other elements shows the strongest correlation with gold, followed by copper.

Check Assaying Program

From the total of 10,584 m of core drilled a total of 2,594 original assays are available, typically with a 1.5 m assay interval. Much of the core above and below the mineralised interval/s was not analysed (presumably to save money). The check assaying program was based on a target of re-assaying 10% (259 samples) of the originally assayed mineral intervals, from throughout the deposit. Ultimately, 235 samples (9.1%) were analysed as check samples, plus standards, duplicates and blank samples.

The target was to collect 259 samples. However, when on site multiple of the target core intervals were found to have been assayed in their entirety, with no core remaining and could not be sampled (these may have been used historically for metallurgical testing – although this is not noted in historical reports). Some additional core intervals were collected in the limited time available on site, but did not make up the shortfall to complete re-sampling of 10% overall.

Intervals were selected to intersect the massive sulphide unit, as well as to have a geographical spread across the deposit and to intersect the lower grade stringer style mineralisation, with holes selected along the SW to NE trend of the deposit.

In addition to the re-assay check samples these were accompanied with QA/QC samples (which were not used in the original 1096 and 1997 sampling programs) to include ~ 10% of the re-assay samples as duplicates, certified standards and blanks.

The core was originally split with a pressure splitter, to create approximately half split core, with half submitted to the laboratory. The resamples core was cut with a core saw, with a quarter submitted for laboratory analysis and the remaining quarter retained for reference.

Given the core was quartered, and mineralisation consists of massive sulphide in places, variability in sample results would expect to be higher than for a more uniformly mineralised deposit, such as a disseminated style. The initial 30 samples were sampled on site, with samples taken between the original intervals marked by flagging tape and sample tickets stapled into the trays.

The subsequent core samples were flown out to the road 20 km from the ICE Project by helicopter and then transported by vehicle to Whitehorse, where it was cut. The first approximately 60 km of the road are gravel and from the town of Ross River, the road is paved all the way to Whitehorse. Given the transportation of the cut core, it is possible some half core moved from one core interval to another, due to vibration during transportation.

Assay results showed there was a relatively high degree of variability for individual sample intervals, although over longer intervals representing the thickness of mineralisation, they showed averages much more consistent with the original results. Therefore, although individual results, when compared between the original half core and re-assay quarter core are variable, the combined results are less so and the average results of all the re-assay samples showed a lower variability still than individual intervals.

The summary statistics of the original assays and the re-assays are provided in **Table 2** below. The results are considered to be reasonable, given the high grade nature of some of the mineralisation and the age of the core. Variation was between +10% for cobalt and -14% for lead (RPD values presented as positives if the re-assays are higher and negative if they are lower.

Overall biases in analyses appear minor, given the performance of the standards and duplicates. However, there may be a slight low bias for copper in the re-assay samples. Cobalt results appear slightly higher overall in the re-assay results.

Analysis of the results showed that the gold results from re-assaying versus the original results have a very high level of correlation (**Table 2** below), with greater variability for copper.

Table 2: *Summary statistics showing the comparison between original and re-assay sample interval assays analysed in the original and re-assay sampling campaigns, For gold, the values are based on only the samples analysed in both programs, where only 113 of the 235 samples re-assayed for gold were originally analysed. Relative Percent Difference (RPD%) shows the difference between the original and re-assay of the same samples, showing some elements presented slightly higher results during the re-analyses and others slightly lower*

	Cu%	Co%	Au g/t	Ag ppm	Zn%	Pb%
ORIGINAL	1.30	0.02	0.13	2.42	0.13	0.00
REASSAY	1.18	0.02	0.13	2.55	0.14	0.00
RPD%	**-9**	**10**	**-6**	**5**	**6**	**-14**

QA/QC reassaying program

Two certified standards were used with the samples to check the results. The standard analyses are considered acceptable, although RPD% values are often above 5%. Consistent with the comparison of the results above copper results were below the standard, although the averages for zinc and lead averaged below the standard values, gold was above the standard values and cobalt close to the standard values.

Field duplicate samples showed a significant level of variability, as observed between the original re-assay samples. Copper in particular shows a relatively high level of variability between the primary and duplicate pairs, with copper noted to be the worst performing element across the original-reassay comparisons and the duplicates included with the re-assays.

Overall the original assays are considered to have been adequately validated by the check assays. Analysis of the duplicate samples in an additional laboratory could be considered as a further check on repeatability of the results.

Eight blank samples were analysed. No average value was provided for the blank sample used by Aurora Geoscience for the batches sent to the laboratory. Most elements analysed were present in concentrations of < 1 to 10 ppm. The RPD variability averaged 30%, considering the low concentrations of elements. Results appear reasonable, with no significant spikes in the elements of interest.

Table 3: *Summary of standard performance in the re-assay batches, with standard values and acceptable ranges, average values across the number of standards and Relative Percentage Difference values, representing variability*

Standard	Analyses	Cu%	Co%	Au g/t	Ag ppm	Zn%	Pb%
CDN-ME-2001		1.06+/-0.04%	0.02+/-0.001%	1.317+/-0.139 g/t	574 +/-24 ppm	1.5 +/-0.05%	0.78 +/-0.031%
Average	5	1.05	0.02	1.42	577.40	1.50	0.76
RPD%	5	4.30	4.56	10.19	6.58	3.01	7.52
CDN-ME-2101		1.32+/-0.06%		0.765 g/t +/- 0.087	48+/-4ppm	1.488 +/-0.057%	0.827 +/-0.038%
Average	4	1.26	130.63	0.80	n/a	1.43	0.81
RPD%	4	13.08	5.36	8.92	n/a	12.91	7.81
Comment		Below	Neutral	Above	Neutral	Below	Below

Specific Gravity Data and Validation

A total of 276 samples were originally collected and analysed for specific gravity as part of the original assaying program. These samples were mostly from massive sulphide samples and did not geographically cover the entire deposit. SG values ranged from 2.41 (two samples of 2.41 and 2.42 g/cc) to a maximum of 4.81 g/cc. The average SG of the 276 samples was 3.30 g/cc. The details of how the samples were measured is not documented.

As part of the re-assay program, 48 samples were measured for SG by Aurora Geoscience in their shed facility in Whitehorse. Measurements were made with samples in water and air. Material was not covered in wax, as core is compact and does not contain vugs or open fractures.

As a check on the measurements made by Aurora, 38 of the 48 core SG intervals were re-analysed using the pulps (**Figure 7**). Of these measurements 10 were significantly different, in some with the Aurora results higher, and in others with the ALS laboratory results higher. However, the average density across the 38 samples was 3.18 g/cc, very similar to that of the 48 sample set.

Samples show a similar distribution of density ranges, when plotted in increments of 0.2 g/cc. The average value for SG was 3.20 g/cc across the 48 samples. See **Figure 8** for a comparison between the datasets.

In the original samples there was a clear bias towards the geological units associated with mineralisation, with most samples from the following units.

- PYMS – The massive sulphide unit
- PHBS – The porphyritic basalt mineralisation host
- BRBS-2 – The brecciated basalt unit that underlies the mineralisation
- MSBS-3 – The massive basalt that overlies the mineralised package

Plotting the SG samples by depth for the combined holes shows a pattern where the shallower material generally has a higher SG value. This is consistent with the distribution of the massive sulphide unit, which is typically present at the top of the porphyritic basalt geological unit and can be underlain by more stringer type mineralisation.

Overall the specific gravity data from the core is considered reasonable, with the most significant possible restriction the geographical distribution of the samples. The re-sampling endeavoured to provide samples in areas where there was previously no information, however, most of the "unmineralized" core above and below the ICE mineralised lens was not cut and there are no samples from this "background" lithology material.

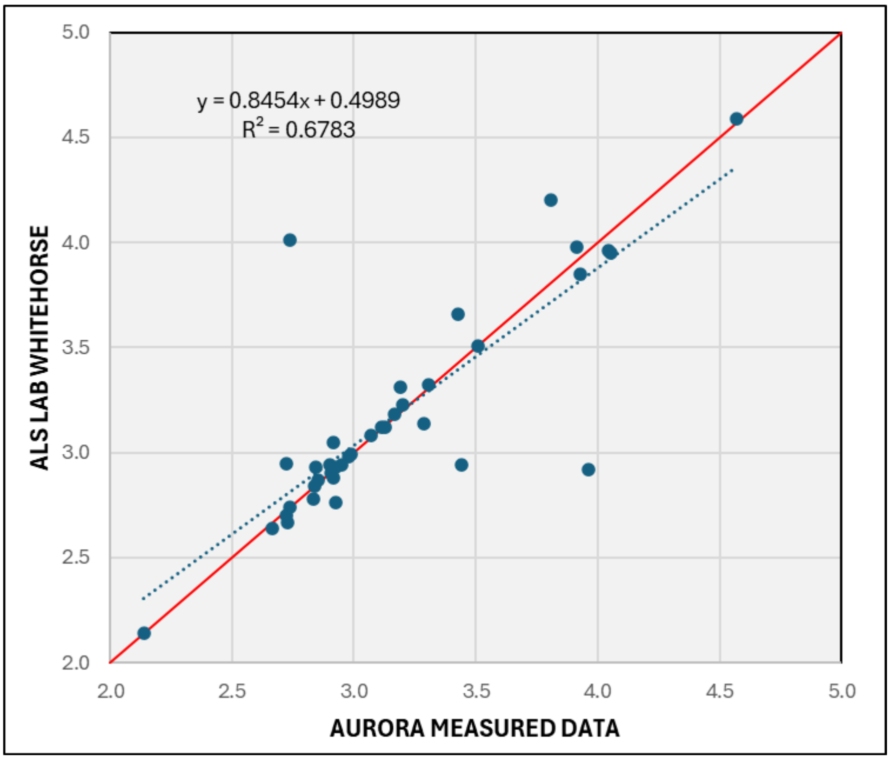

Figure 7: SG data for 38 samples analysed by Aurora and ALS laboratories

Modelling of Mineralisation

The following section details how different aspects of the mineralisation were accounted for in the resource model.

Mineralisation Extent

The initial interpretation of mineralisation by BMO was used as a guide, along with the drill hole logging, to develop an outline of mineralisation for estimation. HSC formed the opinion that the main mineralised lens was essentially confined to the PYMS and upper PHBS geological units, with sporadic mineralisation in the BRBS-2 unit interpreted as a separate feeder zone to the main mineralisation.

The main mineralised lens was modified to include immediately adjacent mineralisation above a nominal 0.1% copper equivalent grade threshold and generally excluding material below this threshold. Sometimes lower grade material was included to maintain reasonable local continuity and unit thickness.

The base of the feeder zone was defined as the base of the BRBS unit or the base of assays.

A similar process was used to define the surfaces for the base of oxidation and top of fresh rock. HSC based these surfaces on drill hole logging and surface topography. Weathering codes are limited to “F” for fresh rock, “T” for transition and “S” for oxide, and many intervals at the top of holes had no logging.

There was not a column in the historical logging defining oxidation state. These codes were derived from observations on individual minerals in the logging of each hole, which were coded with an abbreviation of the mineral name. However, the oxide material is not necessarily depleted in copper and there are no sulphur assays to confirm the logging codes. Iron assays were not particularly useful to resolve this uncertainty.

Given the “relatively minor offset” interpreted on what is referred to the baseline fault, trending NNE through the deposit, HSC decided to ignore this structure, which was not obvious during the interpretation of mineralisation. This fault coincides with the change in dip at the northern end of the deposit but cuts across the flat dipping area in the south.

The majority of assay samples have a length of 1.52/1.53m, which is equivalent to 5 feet in imperial measurements used at the time of drilling.

Low default values were assigned to unassayed intervals prior to compositing, on the assumption that any visually obvious mineralisation would have been assayed. Default values for Cu, Ag, Pb, Zn and Co were half the lower assay detection limit.

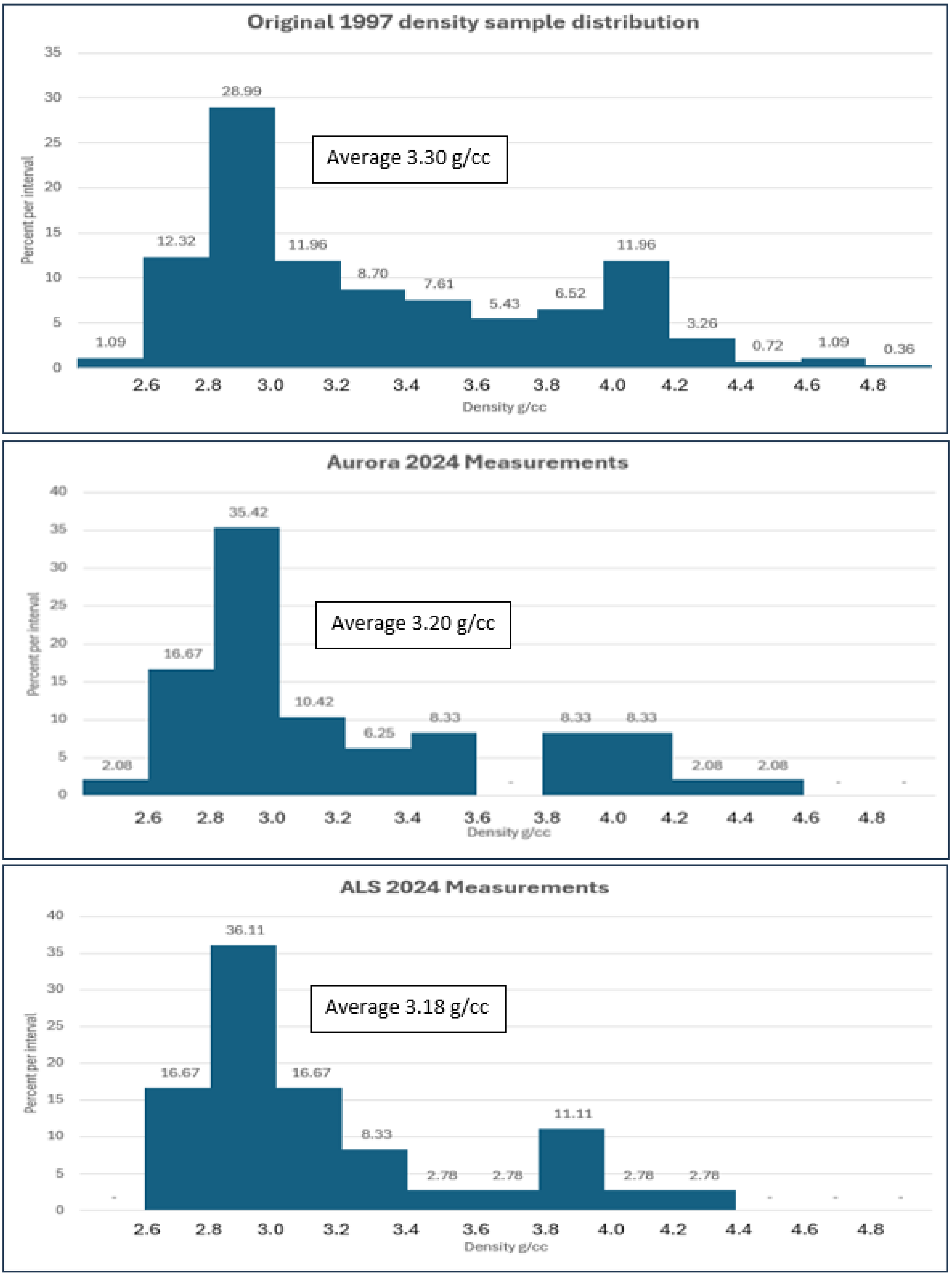

Figure 8: *SG data for the project, showing the original data above, 48 samples measured by Aurora in December 2024 (middle) and below 38 samples measured by ALS labs*

Treatment of Gold Assays

The low number of assays for gold required special consideration, so correlation analysis was performed to find the element that correlated best with gold. **Table 4** shows the results of this analysis, which determined that silver has the best correlation with gold for samples with all assays.

Table 4: *Summary of correlation between elements*

	Cu	Pb	Zn	Au	Ag	Co	Fe
Cu	1.000						
Pb	0.384	1.000					
Zn	0.219	0.094	1.000				
Au	**0.629**	0.377	0.327	1.000			
Ag	**0.669**	**0.575**	0.276	**0.805**	1.000		
Co	**0.712**	0.356	0.319	**0.665**	**0.644**	1.000	
Fe	0.329	0.132	0.247	0.408	0.313	**0.608**	1.000

A regression was performed between silver and gold, which provided a simple formula to convert silver to gold values for unassayed samples. Samples without silver or gold assays were assigned a gold value of half the lower detection limit.

Samples were flagged with the mineralisation wireframes (massive sulphide and feeder zone) and those above or below were flagged as hanging wall or footwall. Samples were not flagged by the oxidation surfaces because there was no obvious evidence to indicate that these had an impact on grades.

Given the sample length analysis, it was considered logical to use a nominal composite interval of 1.50m for data analysis and estimation, with composites less than 0.74m removed. Samples were composited within the different mineralisation zones, as shown in **Table 5**.

Table 5: *Summary of composite statistics for copper in the Hanging Wall (HW), Massive Sulphide (MS), Stringer Feeder zone (Feeder) and Footwall (FW).*

ZONE	Desc.	Samples	Min	Max	Mean	SD	CV
0	HW	807	0.00025	0.04	0.001	0.003	2.78
1	MS	1,578	0.00025	11.17	0.683	1.305	1.91
2	Feeder	1,643	0.00025	4.06	0.075	0.259	3.47
3	FW	2,674	0.00025	0.40	0.002	0.014	6.63

A histogram of copper grades within the massive sulphide zone is presented in **Figure 9**, which shows an approximately log-normal grade distribution with a low grade peak representing low default grades.

Variography

Variograms were generated for the metals of interest within the massive sulphide zone. The flatter upper north-western part of this zone was selected for this analysis because it has a reasonably consistent orientation and a higher drill hole density than the steeper dipping south-eastern section. Drill hole spacing in this upper area is typically 25m on section lines spaced 50m apart.

The variogram maps for copper in upper zone 1 are presented in **Figure 10**, and show the expected NE-SW strike of mineralisation and a shallow dip to the SE.

Figure 11 displays the directional variogram models for copper in upper zone 1, showing that the along strike direction has better continuity than the down dip direction, while the down hole direction has the shortest ranges.

Application of Density Data in the Model

Becker 1998 reported that: “Chemex Labs Ltd. in North Vancouver determined the specific gravity (SG) of pulps from 273 drill core samples which included most rock units and mineralization types comprising resource or waste cells.” “The measured average SG for three other rock types was reduced for the purpose of the resource calculation to allow for open space that may have been present in oxidized core but which was eliminated during grinding to produce the assay pulp.”

This indicates that specific gravity was measured using a pycnometer method and correctly states that this method does not account for any porosity in the samples. Dry bulk density is the attribute required for resource estimation because it does account for sample porosity.

Table 6 shows a breakdown of the recent data provided by the associated codes, which do not necessarily correspond to 1998 lithology/oxidation categories.

HSC has substantial experience in estimating density from assays for base metal deposits, so this technique was applied to the ICE deposit data:

1. Cu, Zn and Pb assays were converted to weight percentage of chalcopyrite, sphalerite and galena respectively,
2. Fe attributable to calculated chalcopyrite and sphalerite was subtracted from the total Fe assay,
3. 5% Fe was subtracted from the remaining Fe to account for Fe in non-sulphide gangue minerals,
4. Final remaining Fe was converted to pyrite content,
5. Proportion of gangue calculated by subtracting total sulphide mineral proportion from 100%,

6. Density calculated as the weighted average of the mineral volumes and densities, where gangue had an assumed SG of 2.80.

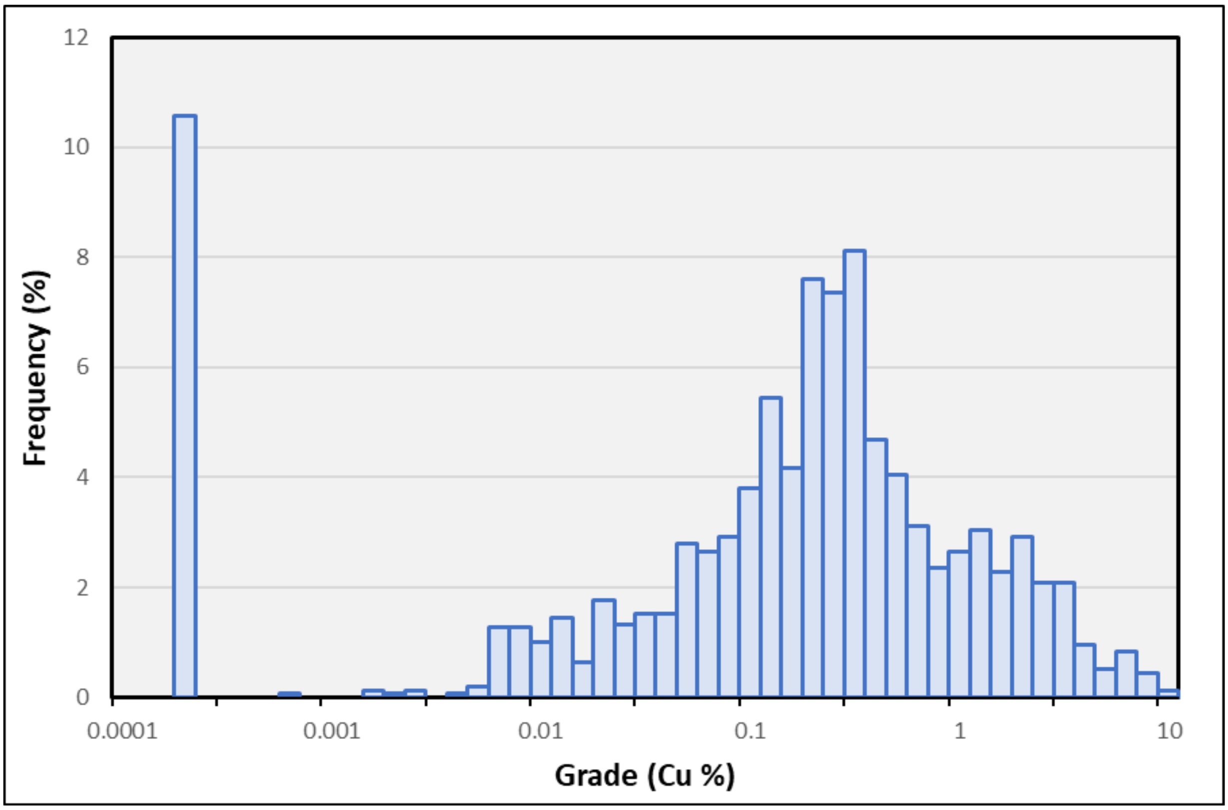

Figure 9: *Histogram for copper in the Massive Sulphide (Zone 1)*

The main issue with this process for the ICE data set was the substantial number of Fe assays reporting as over the upper detection limits of 15 and 30%. This was dealt with by assuming a crude regression where Fe grade equals 10x the Cu grade, but not below the original Fe assay. Total sulphide mineral content was limited to 100%, with pyrite reduced if necessary. This procedure could be refined further, perhaps by limiting Fe to 100% minus all other assayed elements.

This process was applied to samples with SG measurements and Fe grades below the upper detection limits, which are plotted in **Figure 12** showing good correlation and unbiasedness. This validates the assumptions of subtracting 5% Fe for non-sulphide gangue and a gangue SG of 2.80.

Density was then calculated for all drill hole intervals using this process, and a preferred density value was selected, with actual measurements used where available and calculated values otherwise. Samples were then flagged and composited in the same way as the grade data, followed by variography.

The average of the final preferred values is significantly lower than measured values (-13.3%), suggesting a selection bias in the samples chosen for measurement. The average copper grade for samples with measured density values is 2.5 times greater than all samples (2.42% vs 0.68% Cu), confirming a selection bias.

In the future additional density measurements should be taken to validate existing data and obtain more meaningful values for oxide and transition material.

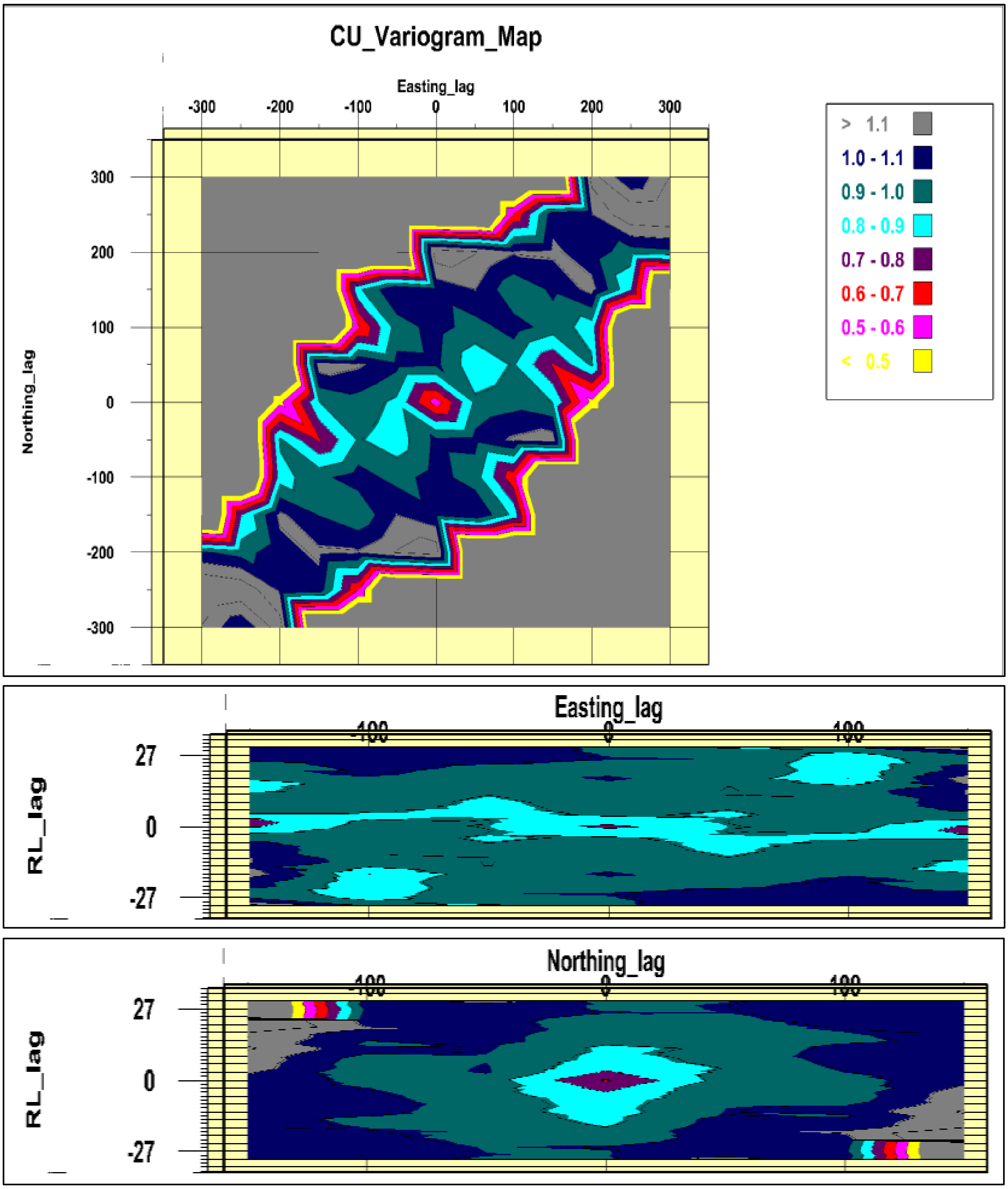

Figure 10: *Variogram Maps for Copper – Upper Zone 1*

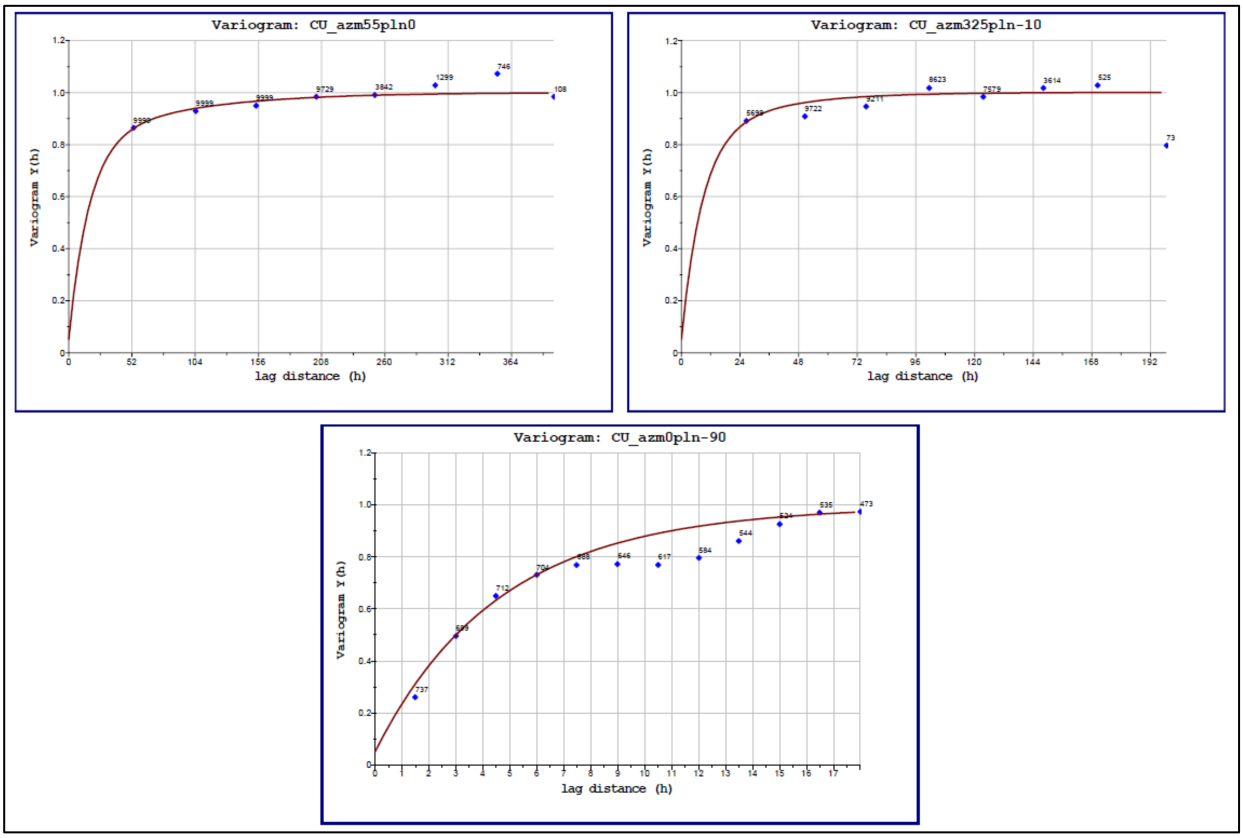

Figure 11: *Variogram Models for Copper – Upper Zone 1, (top left = along strike, top right = down dip, bottom = down hole)*

Table 6*: Summary of specific gravity data.*

Unit	Oxidation	Samples	Min. SG	Max. SG	Avg. SG	Avg. Cu %
PYMS	Fresh	116	2.42	4.81	3.26	1.44
	Trans	14	2.82	4.10	3.64	2.98
	Oxide	2	4.04	4.37	4.21	3.43
PHBS	Fresh	14	2.66	4.76	3.15	1.50
	Trans	16	2.74	4.12	3.45	2.78
	Oxide	12	2.82	4.47	3.62	2.95
BRBS-2	Fresh	53	2.75	4.30	3.25	1.00
	Trans	24	2.64	4.29	3.37	1.40
	Oxide	5	2.78	4.06	3.57	8.07
MSBS-3	Fresh	19	2.41	4.16	3.04	1.20
	Oxide	1	3.03	3.03	3.03	0.09
Grand Total		**276**	**2.41**	**4.81**	**3.30**	**1.69**

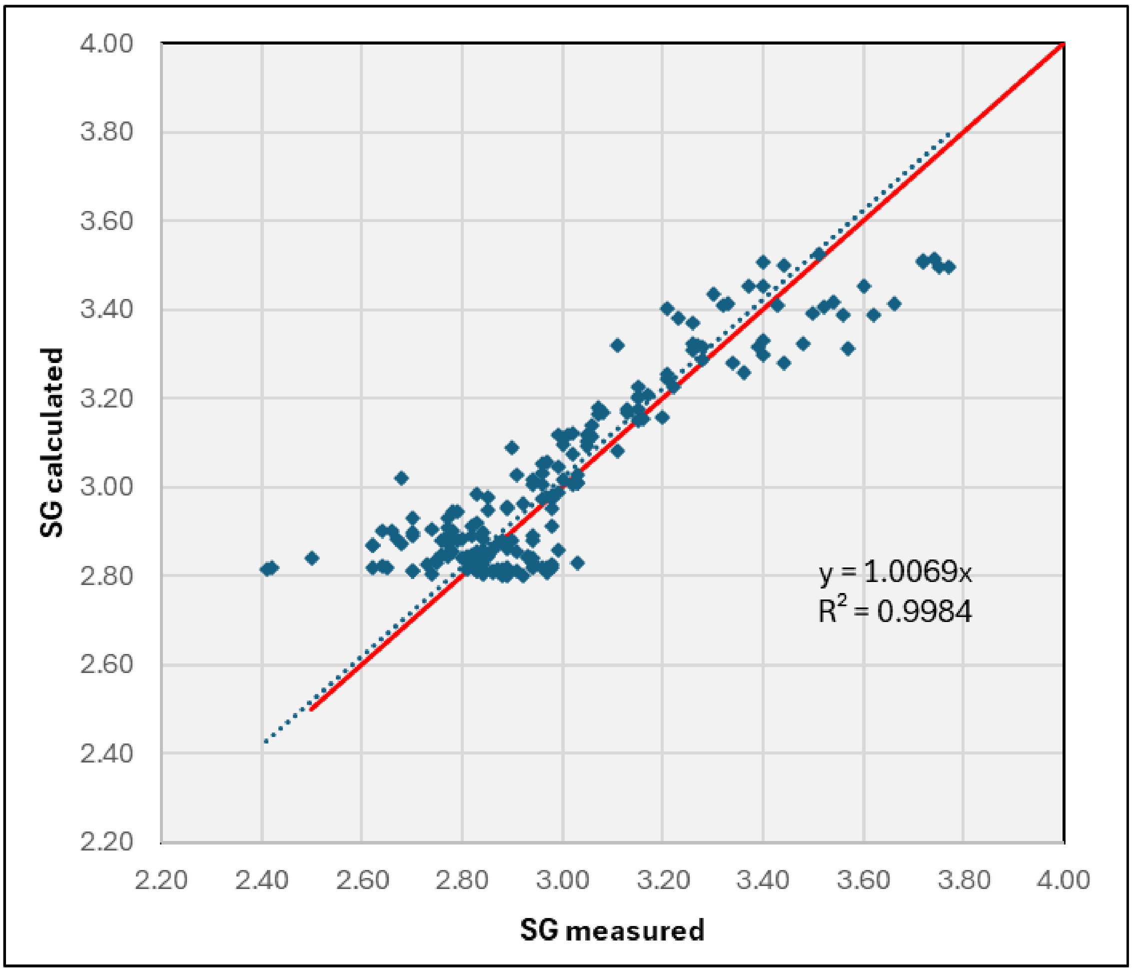

Figure 12: *Comparison of measured and calculated SG*

Sample Recovery

Core recovery averages 82.6%. There are 172 of 2,590 (6.6%) of intervals with recovery >100% and 45 intervals (1.7%) with recovery <20%. Samples with recoveries as low as 2% have copper assays and there is one sample (N111423) with 15% recovery and a copper grade of 2.03%. Apart from 2 samples, core recovery is only recorded for intervals with assays, with most core above and below the mineralised interval not cut and assayed.

HSC has developed a method of analysing sample recovery data that involves a conditional expectation plot. The data is divided into grade bins with equal numbers of samples and then the average recovery is calculated for each bin. The equal sample weight in each bin is important and avoids problems associated with low sample numbers.

Averaging recovery by grade bins avoids issues with high numbers of 100% recovery values. The resulting graph can then be assessed to see if the resulting line has a significant gradient. If the trend line is horizontal, then there is no bias in grade due to poor sample recovery, while a significant gradient could indicate a bias and would require further investigation, particularly if higher grades are associated with lower recoveries. In this case, there is no obvious bias.

Estimation Methodology

Ordinary kriging (**OK**) was chosen as the appropriate estimation method for metal grades at the ICE deposit, because grade distributions are not particularly skewed, show reasonable continuity as defined by variography and do not contain extreme erratic values.

The model was generated in NAD83 Zone 9 coordinates, and the dimensions of the block model are presented in **Table 7.** The blocks are orthogonal to the grid, although the drill hole section lines and mineralisation are oblique.

Table 7: *Summary of ICE block model dimensions*

Parameter	X	Y	Z
Origin	376,350	6,862,600	1,000
Maximum	377,050	6,863,150	1,400
Block Size	12.5	12.5	2.5
Number of blocks	56.0	44.0	160.0
Length	700	550	400

The block size represents ½ to ¼ of the drill hole spacing, which is a little smaller than preferred but was deemed necessary to adequately accommodate the variable orientation of mineralisation. Sub-blocks at half the parent block size in each direction were used at zone boundaries, although estimates were generated at the scale of parent blocks.

Dynamic estimation was implemented, based on the orientation of the mid-plane of zone 1, in order to deal with the variable orientation of mineralisation.

The estimation search parameters are provided in **Table 8**; an extra pass at double the Pass 3 radii was used for iron because no low default values were applied to unassayed intervals.

Table 8: *Summary of ICE estimation search strategy*

Pass	Radii			Samples		Octants
	X	Y	Z	Min	Max	Min
1	50	50	5	12	32	4
2	100	100	10	12	32	4
3	200	200	20	8	32	4

No grade cutting was applied because grade distributions are not particularly skewed, show reasonable continuity as defined by variography and do not contain extreme erratic values. Estimates were generated for Cu, Au, Ag, Pb, Zn, Co and Fe, and the final copper equivalent metal grade estimates were density weighted.

Density was estimated directly from the preferred composite data using the same scheme as the metal grades. To account for oxidation, HSC applied nominal factors of 2.5/2.8 for oxide and 2.7/2.8 for transitional material to the estimated density values.

A check estimate was also generated using the nearest neighbour (NN) method, which is similar to the polygonal method used in 1998. A composite length of 2.5m was utilised for this model, which corresponds to the nominal block height

Model Validation

The new model was validated in a number of ways – visual and statistical comparison of block model and drill hole grades, assessment against the previous estimate, comparison with the nearest neighbour check model and analysis of grade-tonnage data.

Visual comparisons of block and drill hole grades, like **Figure 13**, show reasonable agreement in all areas examined and no obviously inexplicable areas of grade or excessive smearing in the model. The dynamic interpolation honours the locally interpreted mineralisation orientation well.

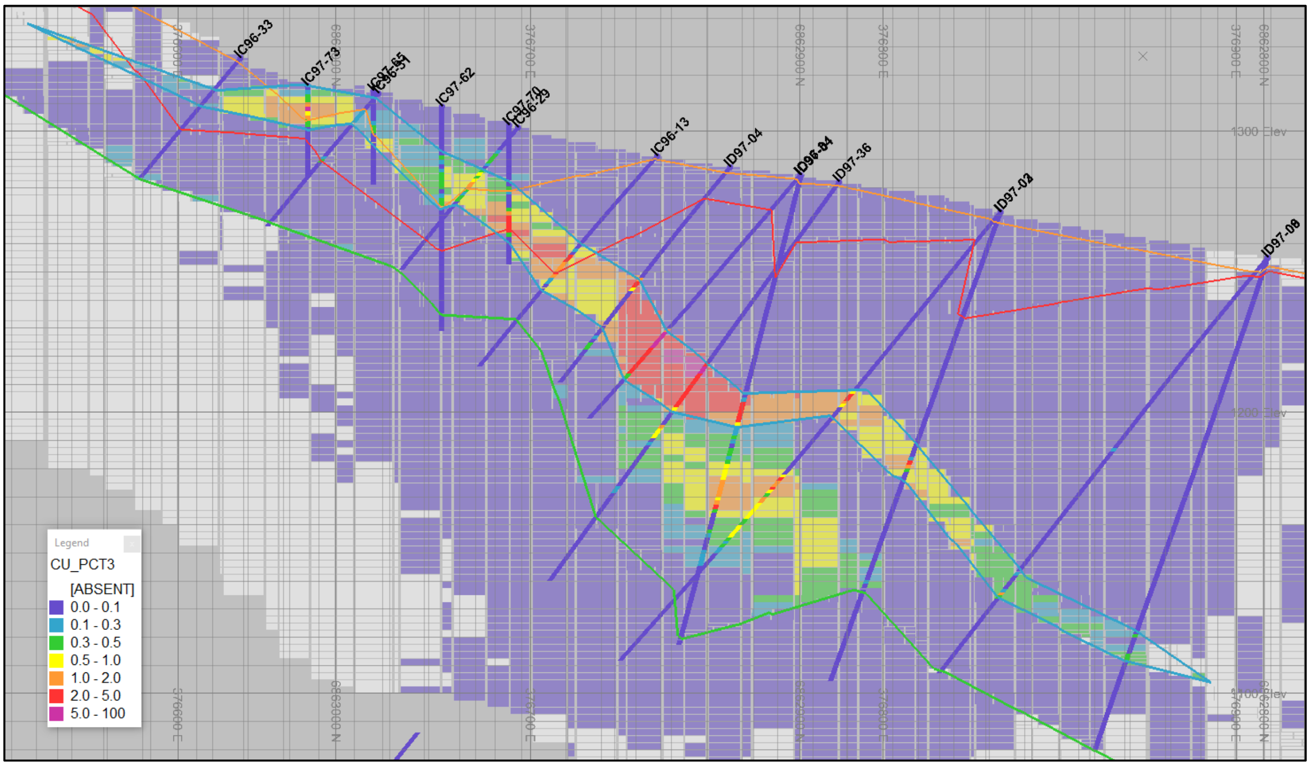

Figure 13: *Cross-section showing Drill Holes and Model Blocks coloured by Copper. (Lines: blue = MS, green = Base of Feeder, orange = base of Oxidation, red = top of Fresh Rock)*

A comparison of drill hole composite and block model grades for Zone 1 shows some significant differences, particularly for Cu, Ag and Au, as shown in **Table 10**. This can be explained as the effect of data clustering, although in this case the situation is the opposite to normal. Here drilling is concentrated in areas of lower grade (shallow), with fewer samples available in higher grade areas (deeper). The model grades are volume weighted and are therefore more representative of the zone than the drill hole composite grades. The density weighting of estimates has also increased block metal grades by around 5-12%.

Cut-off grade

The 1998 estimate used a cut-off grade of 0.3% Cu for secondary copper mineralisation and 0.5% for sulphides. Becker 1998 stated that: “It is assumed that all mining would be by open pit methods, that most secondary copper mineralization could be recovered by heap leaching, coupled with solvent extraction electrowinning and that sulphide mineralization would be milled and concentrated by selective flotation.”

The cut-off grade of 0.3% Cu has been applied for the resource estimate and is considered likely to be economic for the mining method and scale of operation envisioned for ICE, based on comparison with similar deposits elsewhere. This parameter will be evaluated further in the future, provided that sufficient resources are found that contribute to a mineable tonnage of mineralisation.

A comparison of the 1998 global resource and the 2025 final OK model at an 0.3% Cu cut-off grade in **Table 9** shows similar copper metal content, with higher tonnage and lower grade in the latter.

This is not an unexpected result for a comparison between a polygonal and OK estimate, because the former is essentially undiluted and unsmoothed.

When the 1998 and 2025 NN models are compared, the NN model is almost identical globally to the 1998 resource, apart from Co grade which may be a rounding issue.

The grade-tonnage curves for the 2025 OK model, presented **in Figure 14**, show a smooth transition between cut-off grades and no obvious kinks or bumps suggestive of over-constraining of the grade estimates or a conditional bias.

Table 10 contains the grade-tonnage data for the 2025 OK model, which shows that the model includes 4.22 Mt at an average grade of 1.42% Cu above a 0.50% Cu cut-off grade and 6.43 Mt at an average grade of 1.07 % Cu at a 0.3% cut-off grade. All grades, including SG, increase steadily as cut-off grade rises. **Table 10** also shows there is a significant proportion of the resource with grade >1.5% Cu above an 0.55% Cu cut-off grade.

Comparison of cross sections between the NN and OK models show sudden changes in grade and lack of grade continuity in the NN model, compared to the smoother, more continuous grade distribution in the OK model. HSC contends that the OK model is a more reasonable spatial distribution of grades, including appropriate smoothing and dilution that produces mineable grades. The NN model would require substantial dilution to produce mineable grades and represents an extreme end member without any smoothing or dilution, i.e., it is unrealistic. It is encouraging to note that the high grade core of mineralisation is present in both models, albeit to varying degrees.

The similarity between the 1998 estimate and 2025 NN model, and the differences between the 2025 NN and OK models give confidence that the OK model is a more reasonable representation of the mineable resource than the 1998 estimate.

***Table 9:** Comparison of 1998 polygonal and 2025 OK Models (2025 @ 0.3% Cu cut-off grade, 1998 @ 0.3/0.5% Cu). The polygonal model does not take into account dilution, which is accounted for in the OK model*

Model	Mt	Cu %	Ag ppm	Zn %	Co %	Kt Cu
1998	4.56	1.48	3.53	0.14	0.020	67.5
2025 OK	6.43	1.07	2.92	0.11	0.018	68.6
% Diff	41.0%	-28.0%	-17.3%	-21.1%	-8.7%	1.6%

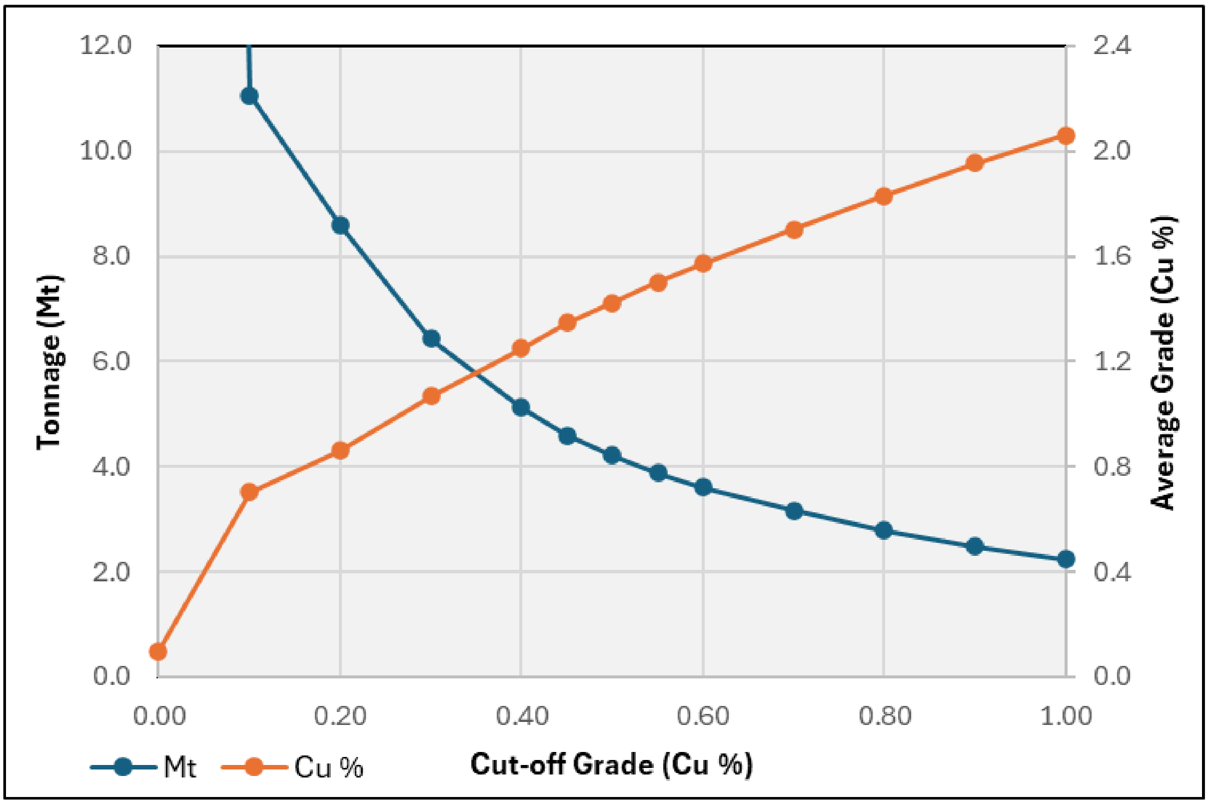

Figure 14: *Grade tonnage for the 2025 OK model*

Table 10: *Grade-Tonnage data from the new OK model*

CUTOFF	Mt	Cu %	Au g/t	Ag ppm	Zn %	Co %	SG t/m3	Kt Cu
0.00	83.0	0.10	0.01	0.4	0.01	0.002	2.80	80.6
0.10	11.1	0.70	0.06	2.0	0.09	0.013	2.90	77.6
0.20	8.61	0.86	0.07	2.4	0.10	0.015	2.92	73.9
0.30	**6.43**	**1.07**	**0.09**	**2.9**	**0.11**	**0.018**	**2.97**	**68.6**
0.40	5.12	1.25	0.11	3.5	0.12	0.021	3.02	64.0
0.45	4.59	1.35	0.12	3.7	0.13	0.022	3.04	61.8
0.50	**4.22**	**1.42**	**0.12**	**4.0**	**0.13**	**0.023**	**3.05**	**60.0**
0.55	3.88	1.50	0.13	4.2	0.14	0.024	3.06	58.2
0.60	3.60	1.57	0.14	4.5	0.14	0.025	3.08	56.7
0.70	3.16	1.70	0.15	4.9	0.15	0.027	3.11	53.8
0.80	2.79	1.83	0.16	5.3	0.15	0.028	3.13	51.0
0.90	2.47	1.96	0.17	5.7	0.16	0.030	3.16	48.3
1.00	2.24	2.06	0.18	6.0	0.16	0.032	3.18	46.1

Resource Classification

The 1998 global resource was classified as Indicated in an audit by Thompson 1998, although it was apparently not classified by Becker (1998), who did the original estimate.

The estimation search pass for copper is presented in upper **Figure 15** and shows that the majority of blocks were estimated in Passes 1 and 2, with minor additional tonnes in Pass 3. HSC then smoothed the search pass results to minimise the "spotted dog" effect and combined passes 1 and 2 into Class 2, and Pass 3 data into Class 3, as shown in lower **Figure 15**. The distribution of copper mineralisation in the resource is shown in **Figure 16**.

Resource classification was based on estimation search pass, subsequent to smoothing. The majority of resources are classified as Indicated, in line with the 1998 estimates, with around 10% of tonnage as Inferred, occurring around the edges of the resource or in areas with wider spaced drilling, as might be expected.

This scheme is considered to take appropriate account of all relevant factors, including the relative confidence in tonnage and grade estimates, confidence in the continuity of geology and copper values, and the quality, quantity and distribution of the data. The drill spacing is approximately 50 m spaced lines, with approximately 25 m spaced holes through much of the deposit, with drilling becoming sparser around the edges of the deposit. The classification appropriately reflects the Competent Persons' view of the deposit.

Mining and Metallurgical Methods and Parameters'

The deposit is considered to be primarily amendable to open pit mining, with the potential for underground exploitation of deeper mineralisation. Consideration of current economics would be required to assess the basis of extraction with recent commodity prices.

The OK estimation method implicitly incorporates internal mining dilution at the scale of the model block size. No specific assumptions were made about external mining dilution or mining losses in the Mineral Resource Estimate.

The maximum slope for the historical 1998 conceptual pit design was 50 degrees on the eastern side and 45 degrees on the other three sides. The maximum stripping ratio for the historical pit outline was considered to be 10:1 for the massive sulphide mineralisation. No significant metallurgical test work has been completed on the ICE deposit. Metallurgy is a priority to evaluate extractability and to assess the likely value of accessory mineralisation of gold, cobalt, zinc and silver to generate a copper equivalent resource.

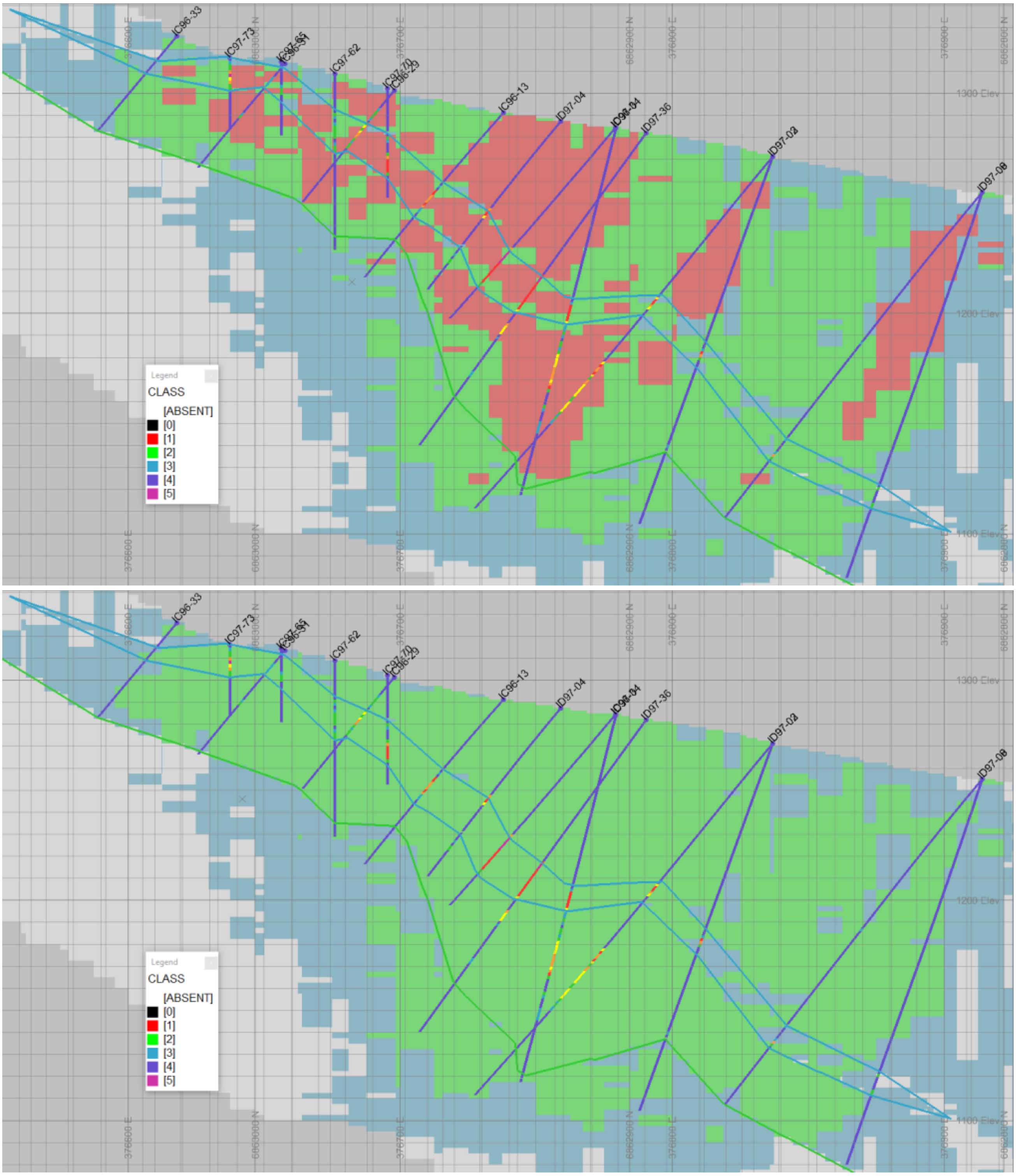

Figure 15: *Cross section showing the estimation pass (upper part of figure) and the combined class (lowest part of the figure)*

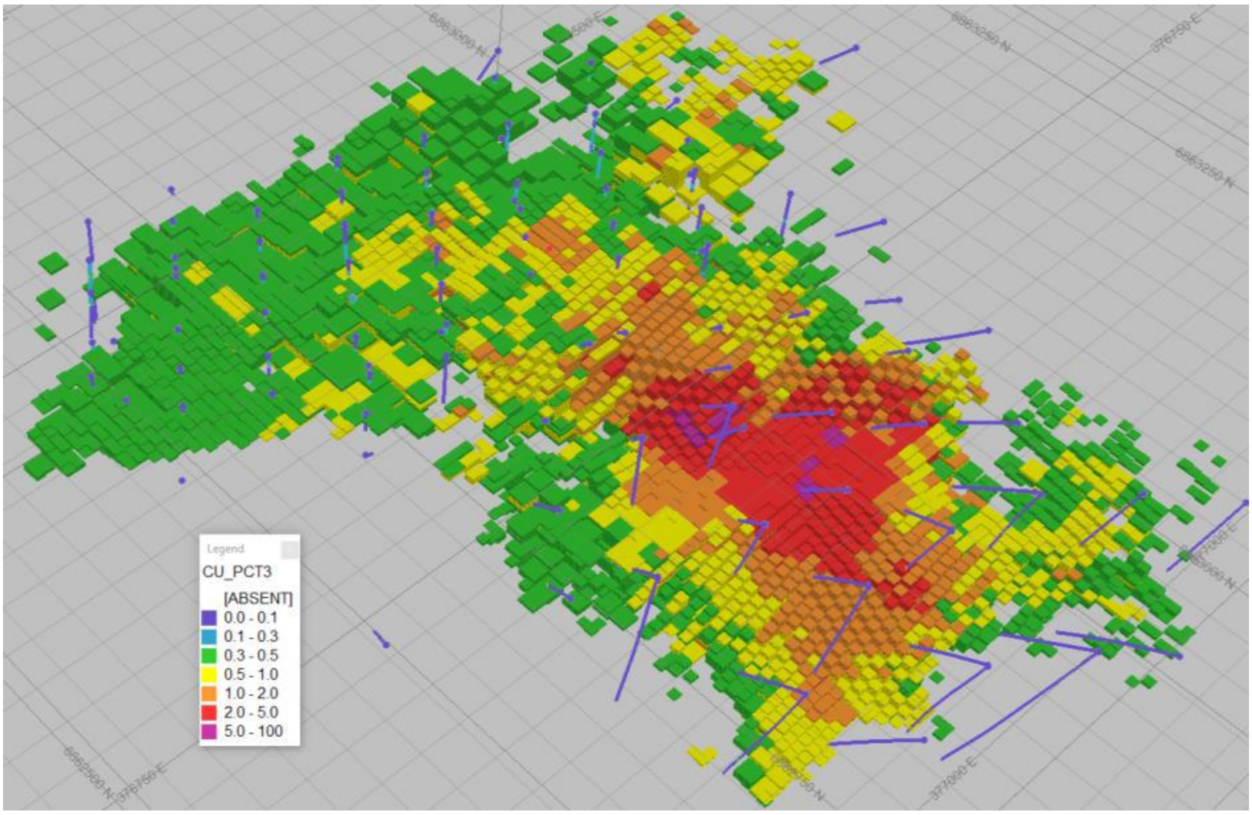

__Figure 16:__ Oblique view of the ICE resource with Cu > 0.3%, looking to the NW

__Table 11:__ Cu mineralisation and other elements at a 0.3% Cu cut-off

Class	Cut-off	Mt	Cu %	Au g/t	Ag ppm	Zn %	Co %	Kt Cu
Indicated	Cu 0.3%	5.76	1.09	0.09	2.9	0.11	0.018	62.8
Inferred	Cu 0.3%	0.67	0.83	0.10	2.9	0.09	0.018	5.81
Total	Cu 0.3%	6.43	1.07	0.09	2.9	0.11	0.018	68.6

Further work is required to determine to what extent potential by-product metals are recoverable and could contribute value to the ICE Project.

This announcement was approved for release by the Chairman of Bastion Minerals.

For more information contact:

Gavin Rutherford
gavin.rutherford@bastionminerals.com

APPENDIX 1
Statements and Disclaimers

Competent Person Statement

The information in this report that relates to Mineral Resources is based on and fairly represents information and supporting documentation compiled by Mr Arnold van der Heyden who is a Director of H & S Consultants Pty Ltd. Mr van der Heyden is a member and Chartered Professional (Geology) of the Australian Institute of Mining and Metallurgy and has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration, and to the activity being undertaken, to qualify as a Competent Person as defined in the 2012 edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' (JORC code). Mr van der Heyden consents to the inclusion in this report of the matters based on the information in the form and context in which it appears.

The information in this announcement that relates to Exploration Results that underpin the Mineral Resources has been compiled by Mr Murray Brooker (AIG #3503; RPGEO # 10,086), of Hydrominex Geoscience Pty Limited. The information in the market announcement provided under rules 5.12.2 to 5.12.7 is an accurate representation of the available data and studies for the material mining project and the information referred to in rule 5.22(b) and (c).
need
Mr Brooker, who is an independent geological consultant to Bastion Minerals, is a Member of the Australian Institute of Geoscientists, (AIG), and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity he is undertaking to qualify as the "Competent Person" as defined in the 2012 Edition of the *Australasian Code for Reporting Exploration Results, Mineral Resources and Ore Reserves*. Mr Brooker consents to the inclusion in the announcement of the matters based on this information in the form and context in which it appears. The announcement is based on and fairly represents information and supporting documentation prepared by the competent person.

Forward-Looking Statements

Certain statements contained in this Announcement, including information as to the future financial or operating performance of Bastion Minerals and its projects may also include statements which are 'forward-looking statements' that may include, amongst other things, statements regarding targets, estimates and assumptions in respect of mineral reserves and mineral resources and anticipated grades and recovery rates, production and prices, recovery costs and results, capital expenditures and are or may be based on assumptions and estimates related to future technical, economic, market, political, social and other conditions. These 'forward-looking statements' are necessarily based upon a number of estimates and assumptions that, while considered reasonable by Bastion Minerals, are inherently subject to significant technical, business, economic, competitive, political and social uncertainties and contingencies and involve known and unknown risks and uncertainties that could cause actual events or results to differ materially from estimated or anticipated events or results reflected in such forward-looking statements.

Bastion Minerals disclaims any intent or obligation to update publicly or release any revisions to any forward-looking statements, whether as a result of new information, future events, circumstances or results or otherwise after the date of this Announcement or to reflect the occurrence of unanticipated events, other than required by the *Corporations Act 2001* (Cth) and the Listing Rules of the Australian Securities Exchange (**ASX**). The words ‘believe’, ‘expect’, ‘anticipate’, ‘indicate’, ‘contemplate’, ‘target’, ‘plan’, ‘intends’, ‘continue’, ‘budget’, ‘estimate’, ‘may’, ‘will’, ‘schedule’ and similar expressions identify forward-looking statements.

All ‘forward-looking statements’ made in this Announcement are qualified by the foregoing cautionary statements. Investors are cautioned that ‘forward-looking statements’ are not guarantee of future performance and accordingly investors are cautioned not to put undue reliance on ‘forward-looking statements’ due to the inherent uncertainty therein.

For further information please visit the Bastion Minerals website at www.bastionminerals.com

APPENDIX 2 References

Bastion, 6 November, 2024. Exceptional Shallow High-Grade Initial Resampling Results 10.98m @ 7.15% Copper for JORC Code Resource Definition - ICE Copper Project.

Bastion, 17 September, 2024. ICE Copper Project Update 10,500 m Historical Drill Core Confirmed On Site, Resampling And Assaying Underway To Define JORC Code Resource.

Bastion, 12 September, 2024. ICE Copper Project Update: Bastion Meets Yukon Government Agencies & Begins First Nations Engagement To Establish Access For Exploration Plans.

Bastion, 12 August, 2024. High-Grade Copper Open Pit Potential With Untested Potential Along Strike And Nearby - ICE Copper Project (Yukon).

Bastion, 30 July, 2024. BMO To Acquire High-Grade Canadian Copper Portfolio – Thick Drill Intersections To 20.56m @ 5.20% Copper. Historical Resource 5mt @ 1.5% Copper – Major Expansion Potential.

Becker, T.C. 1998a. Assessment report describing geological mapping, soil geochemistry and diamond drilling on the ICE property for Expatriate resources, February, 1998.

Becker T.C. 1998b. Report describing mineral resource calculations at ICE property in the Watson Lake Mining District, Yukon Territory, for Expatriate Resources Ltd. May, 1998.

Devine, F.; Carr, S. D.; Murphy, D. C.; Davis, W. J.; Smith, S.; and Villeneuve, M. “Geochronological and geochemical constraints on the origin of the Klatsa metamorphic complex: Implications for Early Mississippian high-pressure metamorphism within Yukon-Tanana terrane,” in Paleozoic Evolution and Metallogeny of Pericratonic Terranes at the Ancient Pacific Margin of North America, Canadian and Alaskan Cordillera, M. Colpron and J. L. Nelson, Eds., vol. 45, pp. 107–130, Geological Association of Canada, Special Paper, 2006.

Green, A. “Fyre Lake Project,” NI 43-101 Technical Report R431.2017, prepared for BMC Minerals, Ltd, Yukon Territory, Canada, 2018, June 2019, http://www.sedar.com/.

Hunt, J. A. “Massive sulphide deposits in the Yukon-Tanana and adjacent terranes,” in Yukon Exploration and Geology 1996, pp. 35–45, Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, 1997.

Hunt, J. "The setting of volcanogenic massive sulphide deposits in the finlayson lake district," in Yukon Exploration and Geology 1997, Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, 1998.

McDonald, M.; Piercey, S.; Layne, G.; Pigage, L. and Piercey, G. "Mineral assemblages, textures and in situ sulphur isotope geochemistry of sulphide mineralization from the Cyprus-type ice volcanogenic massive sulphide (VMS) deposit, Yukon, Canada," Minerals, vol. 8, no. 11, p. 501, 2018

Manor, M.J.; Piercey, S.K.; Murphy, D.C.; and Wall, C.J. Age and Chemostratigraphy of the Finlayson Lake District, Yukon: Implications for Volcanogenic Massive Sulfide (VMS) Mineralization and Tectonics along the Western Laurentian Continental Margin. GeoScienceWorld Lithosphere Volume 2022, Article ID 4584611, 45 pages https://doi.org/10.2113/2022/4584611

Murphy, D. C.; Mortensen, J. K.; Piercey, S. J.; Orchard, M. J. and Gehrels, G. E. "Mid-Paleozoic to early Mesozoic tectonostratigraphic evolution of Yukon-Tanana and Slide Mountain terranes and affiliated overlap assemblages, Finlayson Lake massive sulphide district, southeastern Yukon," in Paleozoic Evolution and Metallogeny of Pericratonic Terranes at the Ancient Pacific Margin of North America, Canadian and Alaskan Cordillera, M. Colpron and J. L. Nelson, Eds., vol. 45, pp. 75–106, Geological Association of Canada, Special Paper, 2006.

Murphy, D. C.; Colpron, M.; Roots, C. F.; Gordey, S. P.; and Abbott, J. G. "Finlayson Lake targeted geoscience initiative (southeastern Yukon), part 1: bedrock geology," in Yukon Exploration and Geology 2001, D. S. Emond, L. H. Weston, and L. L. Lewis, Eds., pp. 189–207, Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, 2002.

Murphy, D. C. "Stratigraphic framework for syngenetic mineral occurrences, Yukon-Tanana Terrane south of Finlayson Lake: a progress report," in Yukon Exploration and Geology 1997, Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, 1998.

Peter, J. M. ; Layton-Matthews, D. ; Piercey, S. J.; Bradshaw, G. D.; Paradis, S. and Bolton, A. "Volcanic-hosted massive sulphide deposits of the Finlayson Lake District, Yukon," in Mineral Deposits of Canada: A Synthesis of Major Deposit-Types, District Metallogeny, the Evolution of Geological Provinces, and Exploration Methods, W. D. Goodfellow, Ed., pp. 471–508, Geological Association of Canada, Mineral Deposits Division, Special Publication No. 5, 2007.

Piercey, S. J.; Murphy, D. C.; and Creaser, R. A. "Lithosphere asthenosphere mixing in a transform-dominated late Paleozoic backarc basin: Implications for northern Cordilleran crustal growth and assembly," in Geosphere, vol. 8, no. 3, pp. 716–739, 2012.

Piercey, S. J.; Peter, J. M.; Mortensen, J. K.; Paradis, S.; Murphy, D. C.; and Tucker, T. L. "Petrology and U-Pb geochronology of footwall porphyritic rhyolites from the Wolverine volcanogenic massive sulfide deposit, Yukon, Canada: implications for the genesis of massive sulfide deposits in continental margin environments," Economic Geology, vol. 103, no. 1, pp. 5–33, 2008.

Plint H. E. and Gordon, T. M. "The Slide Mountain Terrane and the structural evolution of the Finlayson Lake Fault Zone, southeastern Yukon," Canadian Journal of Earth Sciences, vol. 34, no. 2, pp. 105–126, 1997.

Koski, R.A. and Mosier, D.L. Deposit Type and Associated Commodities. Volcanogenic Massive Sulfide Occurrence Model. Scientific Investigations Report 2010–5070–C. U.S. Geological Survey. 2012.

Tempelman-Kluit D.J., Gordey, S.P. and Read, B.C. 1976. Stratigraphic and structural studies in the Pelly Mountains Yukon Territory; Geological Survey of Canada Paper 76-1A, p 97-106.

Thompson, I. S. 1998. Audit of Mineral Resources of ICE Deposit, Yukon, for Expatriate Resources Ltd. By Derry, Michener, Booth & Wahl Consultants Ltd. November 19. 1998.

Tucker , T. and Moore J. May 9th, 2002. A Summary Report for the Finlayson North Project in the Watson Lake Mining District Yukon Territory, Canada. Expatriate Resources Ltd Internal Report.

van Olden, K.; Green, A.; and Davidson, G. "Kudz Ze Kayah Property," NI 43-101 Feasibility Study Technical Report R173.2019, prepared for BMC Minerals, Ltd, Yukon, Canada, 2019, June 2019, http://www.sedar.com/.

APPENDIX 3 Drill collars

Table 12: *ICE Project historical drill collars in the historical project NAD27 datum.*

Collar_ID	EastingUTM9_Nad27	NorthingUTM9_Nad27	Nad27_Elevation	Azimuth	Dip	EOH
IC96-01	376627	6862488	1256	305	-50	182
IC96-02	376788	6862687	1290	288	-50	116
IC96-03	376807	6862636	1278	316	-50	152
IC96-04	376723	6862638	1283	308	-50	148
IC96-05	376690	6862476	1246	306	-50	66
IC96-06	376709	6862596	1276	304	-50	93
IC96-07	376750	6862557	1262	320	-50	53
IC96-08	376632	6862646	1286	0	-90	74
IC96-09	376632	6862646	1286	128	-50	74
IC96-10	375995	6862395	1240	165	-51	84
IC96-11	376311	6862388	1238	300	-51	78
IC96-12	376593	6862675	1298	306	-50	70
IC96-13	376830	6862747	1301	315	-48	99
IC96-14	376671	6862618	1275	308	-50	57
IC96-15	376725	6862719	1291	308	-50	90
IC96-16	376630	6862648	1286	308	-50	54
IC96-17	376577	6862564	1272	308	-50	65
IC96-18	376689	6862726	1296	305	-50	77
IC96-19	376391	6862328	1222	308	-50	59
IC96-20	376654	6862750	1313	310	-50	64
IC96-21	376590	6862507	1259	312	-50	46
IC96-22	376533	6862597	1285	308	-50	45
IC96-23	376616	6862781	1330	307	-50	105
IC96-24	376484	6862637	1316	305	-50	78
IC96-25	376533	6862534	1265	0	-90	52
IC96-26	376580	6862810	1351	308	-50	56
IC96-27	376533	6862534	1265	130	-50	46
IC96-28	376846	6862862	1322	303	-50	85
IC96-29	376789	6862775	1309	303	-50	66
IC96-30	376908	6862814	1298	315	-49	82
IC96-31	376750	6862806	1323	308	-49	62
IC96-32	376767	6862920	1362	296	-50	55
IC96-33	376710	6862835	1337	310	-50	56
IC96-34	376870	6862715	1288	305	-50	115
IC97-35	376650	6862633	1281	0	-90	46
IC97-36	376630	6862648	1286	0	-90	42
IC97-37	376590	6862678	1300	0	-90	40
IC97-38	376611	6862662	1291	0	-90	35
IC97-39	376670	6862619	1275	0	-90	32
IC97-40	376690	6862603	1278	0	-90	35
IC97-41	376713	6862593	1275	0	-90	36
IC97-42	376732	6862574	1267	0	-90	15
IC97-43	376471	6862521	1265	0	-90	38
IC97-44	375921	6862509	1267	270	-50	165
IC97-45	375921	6862509	1267	305	-50	111
IC97-46	376680	6862674	1289	0	-90	47
IC97-47	376621	6862594	1275	0	-90	34
IC97-48	376601	6862608	1279	0	-90	32
IC97-49	376660	6862688	1287	0	-90	29

Collar_ID	EastingUTM9_Nad27	NorthingUTM9_Nad27	Nad27_Elevation	Azimuth	Dip	EOH
IC97-50	376580	6862623	1284	0	-90	34
IC97-51	376551	6862583	1279	0	-90	30
IC97-52	376571	6862568	1274	0	-90	34
IC97-53	376581	6862561	1271	115	-70	37
IC97-54	376513	6862549	1269	0	-90	34
IC97-55	376710	6862714	1289	0	-90	36
IC97-56	376700	6862784	1319	0	-90	77
IC97-57	376730	6862699	1292	0	-90	42
IC97-58	376680	6862799	1324	0	-90	40
IC97-59	376660	6862814	1333	0	-90	39
IC97-60	376625	6862770	1325	0	-90	54
IC97-61	376737	6862628	1281	0	-90	41
IC97-62	376770	6862794	1318	0	-90	80
IC97-63	376721	6862644	1282	0	-90	29
IC97-64	376700	6862659	1281	0	-90	37
IC97-65	376750	6862809	1323	0	-90	33
IC97-66	376681	6862549	1263	0	-90	17
IC97-67	376800	6862834	1325	0	-90	45
IC97-68	376661	6862563	1264	0	-90	18
IC97-69	376611	6862538	1266	0	-90	31
IC97-70	376789	6862780	1310	0	-90	49
IC97-71	376582	6862499	1258	0	-90	26
IC97-72	376601	6862483	1254	0	-90	27
IC97-73	376732	6862823	1329	0	-90	33
IC97-74	376720	6862769	1312	0	-90	50
IC97-75	376631	6862523	1261	0	-90	31
IC97-76	376651	6862509	1258	0	-90	31
IC97-77	376740	6862754	1305	0	-90	45
IC97-78	376641	6862578	1269	0	-90	31
IC97-79	376650	6862758	1316	0	-90	50
IC97-80	376553	6862519	1254	0	-90	27
IC97-81	376620	6862718	1309	0	-90	46
IC97-82	376695	6862725	1295	0	-90	46
IC97-83	376639	6862703	1300	0	-90	47
IC97-84	376760	6862739	1297	0	-90	40
IC97-85	376681	6862735	1298	0	-90	43
ID97-01	376870	6862714	1288	312	-75	173
ID97-02	376930	6862676	1267	310	-50	210
ID97-03	376930	6862676	1267	310	-70	178
ID97-04	376851	6862731	1295	303	-50	98
ID97-05	376850	6862666	1278	318	-50	264
ID97-06	377008	6862621	1255	314	-50	189
ID97-07	376850	6862666	1278	318	-80	175
ID97-08	376912	6862615	1257	307	-50	132
ID97-09	377008	6862621	1255	305	-72	187
ID97-10	376912	6862615	1258	300	-80	150
ID97-11	376944	6862724	1273	309	-51	190
ID97-12	376907	6862752	1286	303	-49	168
ID97-13	376943	6862787	1283	305	-50	149

Collar_ID	EastingUTM9_Nad27	NorthingUTM9_Nad27	Nad27_Elevation	Azimuth	Dip	EOH
ID97-14	376988	6862691	1264	309	-51	192
ID97-15	376975	6862828	1284	305	-49	128
ID97-16	376988	6862691	1264	310	-75	194
ID97-17	377009	6862801	1275	307	-50	132
ID97-18	376995	6862749	1267	307	-44	178
ID97-19	377012	6862802	1274	304	-69	178
ID97-20	376995	6862749	1267	308	-66	157
ID97-21	377089	6862752	1263	309	-52	155
ID97-22	377057	6862704	1260	307	-50	146
ID97-23	377089	6862752	1263	311	-70	272
ID97-24	377057	6862704	1260	306	-70	159
ID97-25	377062	6862649	1254	309	-58	186
ID97-26	377047	6862843	1271	301	-70	165
ID97-27	376927	6862859	1302	308	-51	110
ID97-28	376846	6862609	1267	306	-50	146
ID97-29	376884	6862832	1303	306	-48	63
ID97-30	376797	6862707	1295	305	-47	103
ID97-31	376856	6862789	1301	309	-50	101
ID97-32	377086	6862881	1274	306	-72	111
ID97-33	377118	6862781	1264	305	-49	159
ID97-34	376887	6862577	1254	310	-50	169
ID97-35	376839	6862492	1244	306	-50	89
ID97-36	376883	6862709	1284	306	-54	175

APPENDIX 4 historical drilling results

Table 13: *ICE drilling intersections >0.3% Cu, which are 823 of the total 2595 assays in the drilling database.*

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC96-01	19.9	21.34	1.44	1.05	0.009		0.6
IC96-01	21.34	23.5	2.16	1.11	0.009		0
IC96-01	23.5	24.75	1.25	0.98	0.010		0.2
IC96-01	24.75	26.67	1.92	0.32	0.002		0
IC96-01	26.67	28.18	1.51	0.54	0.001		0
IC96-01	28.18	29.9	1.72	0.5	0.006		0.2
IC96-01	29.9	31.4	1.5	0.56	0.002	0.02	0
IC96-01	31.4	33	1.6	0.63	0.009	0.005	0.2
IC96-01	38.05	39.62	1.57	0.32	0.004		0.2
IC96-01	40.5	42.06	1.56	0.39	0.004		0
IC96-02	19	20.73	1.73	0.38	0.010	0.005	0
IC96-02	24.99	26.76	1.77	1.02	0.022	0.02	1.4
IC96-02	26.76	28.75	1.99	4.1	0.030	0.03	1.4
IC96-02	28.75	30.17	1.42	4.72	0.005		0
IC96-02	30.17	31.7	1.53	1.13	0.010		0
IC96-02	31.7	32.92	1.22	1.93	0.008		0
IC96-02	32.92	34.44	1.52	0.93	0.014		0.2
IC96-02	34.44	37.4	2.96	0.56	0.027	0.015	0.6
IC96-02	39.01	40.54	1.53	0.39	0.009		0
IC96-02	40.54	42.06	1.52	0.46	0.012	0.005	0
IC96-02	42.06	43.59	1.53	0.99	0.012		0
IC96-02	43.59	45.55	1.96	2.97	0.033	0.02	0
IC96-02	45.55	46.63	1.08	5.03	0.016	0.015	0
IC96-02	46.63	48.16	1.53	7.13	0.048		0
IC96-02	48.16	49.35	1.19	8.29	0.035	0.01	0
IC96-02	49.35	50.57	1.22	1.49	0.023	0.095	1.8
IC96-02	50.57	53.08	2.51	1.2	0.015	0.09	2
IC96-02	53.08	54.55	1.47	0.59	0.016	0.01	0
IC96-02	54.55	56.62	2.07	0.86	0.014		0
IC96-02	56.62	58.24	1.62	0.45	0.011		0
IC96-03	60.35	61.57	1.22	1.32	0.014	0.04	2.2
IC96-03	61.57	62.71	1.14	1.18	0.011	0.05	1.6
IC96-03	117.71	118.81	1.1	0.3	0.010		1
IC96-03	118.81	120.4	1.59	0.35	0.011		0.2
IC96-03	120.4	121.92	1.52	0.33	0.013	0.01	0.2
IC96-03	121.92	122.85	0.93	0.45	0.012	0.015	0.2
IC96-04	15.48	17.07	1.59	0.34	0.004		0
IC96-04	17.07	17.98	0.91	0.32	0.003	0.005	0
IC96-04	18.9	20.27	1.37	0.39	0.003		0
IC96-04	22.56	23.62	1.06	1.02	0.051		0
IC96-04	26.52	28.04	1.52	0.46	0.009		0
IC96-04	28.04	29.11	1.07	0.46	0.009		0
IC96-04	29.11	30.18	1.07	0.39	0.014		0
IC96-04	30.18	31.09	0.91	0.48	0.043		0
IC96-04	32.46	33.15	0.69	0.33	0.014	0.015	0
IC96-04	33.15	34.75	1.6	0.31	0.017		0
IC96-04	38.56	40.23	1.67	0.47	0.035		0
IC96-06	8.21	9.34	1.13	0.39	0.005		0.2
IC97-58	33.83	35.36	1.53	0.01	0.003		0
IC97-58	35.36	36.88	1.52	0.02	0.003		0
IC97-58	36.88	38.4	1.52	0.03	0.004		0
IC97-59	3.3	4.27	0.97	0.52	0.003		3.8
IC97-59	4.27	5.79	1.52	0.31	0.003		1.4
IC97-59	5.79	7.31	1.52	0.20	0.004		0.6
IC97-59	7.31	8.8	1.49	0.27	0.004		0.4
IC97-59	8.8	10.06	1.26	0.18	0.003		0.2
IC97-59	13.11	14.63	1.52	0.33	0.004		0
IC97-59	15.76	16.7	0.94	0.78	0.014		0
IC97-60	3.05	4.27	1.22	0.22	0.004		0
IC97-60	6.5	7.31	0.81	0.24	0.005		0
IC97-60	7.31	8.83	1.52	0.55	0.005		0
IC97-60	8.83	10.36	1.53	0.41	0.004		0.8
IC97-60	10.36	11.88	1.52	0.43	0.003		0.8
IC97-60	11.88	13.41	1.53	0.32	0.004		2.2
IC97-60	13.41	14.44	1.03	0.36	0.005		3.6
IC97-60	14.44	15.39	0.95	0.17	0.004		0
IC97-60	16.46	17.98	1.52	0.13	0.003		0.2
IC97-60	17.98	19.51	1.53	0.25	0.004		0
IC97-60	19.51	21.03	1.52	0.21	0.004		0.2
IC97-60	21.03	22.56	1.53	0.26	0.004		0
IC97-60	22.56	23.77	1.21	0.41	0.004		1.2
IC97-60	23.77	25.3	1.53	0.29	0.006		1.8
IC97-60	25.3	26.43	1.13	0.50	0.011		3.4
IC97-60	26.43	27.13	0.7	0.27	0.004		2.6
IC97-60	27.13	28.65	1.52	0.13	0.004		1.4
IC97-60	28.65	30.18	1.53	0.29	0.005		3.4
IC97-60	30.18	31.7	1.52	0.42	0.005		7.8
IC97-60	31.7	33.3	1.6	0.32	0.005		5.6
IC97-62	40.84	42.37	1.53	0.01	0.003		0
IC97-62	42.37	43.89	1.52	0.01	0.005		0
IC97-65	13.75	15.3	1.55	0.22	0.005		0
IC97-65	15.3	16.8	1.5	0.05	0.004		0
IC97-65	16.8	18.29	1.49	0.03	0.006		0
IC97-66	4.3	5.6	1.3	0.34	0.003		0
IC97-67	16.15	17.68	1.53	0.01	0.003		0
IC97-67	17.68	19.51	1.83	0.01	0.003		0
IC97-67	20.22	21.34	1.12	0.14	0.005		0
IC97-67	24.08	25.6	1.52	0.02	0.003		0
IC97-68	5.5	7.01	1.51	0.14	0.003		0
IC97-68	7.01	8.38	1.37	0.13	0.002		0
IC97-68	8.38	10.36	1.98	0.24	0.004		0
IC97-68	10.36	13.11	2.75	0.02	0.005		0
IC97-69	3.66	5.4	1.74	0.26	0.001		0
IC97-69	5.4	6.4	1	0.25	0.001		0
IC97-69	10.97	12.5	1.53	0.40	0.001		0.6
IC97-72	16.46	17.53	1.07	0.28	0.002		0

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC96-06	9.34	10.36	1.02	0.3	0.006		0.2	IC97-72	17.53	19.35	1.82	0.17	0.000		0
IC96-06	11.25	12.69	1.44	0.39	0.005		0.2	IC97-73	2.1	3.66	1.56	0.24	0.011		0
IC96-06	16.46	17.48	1.02	0.38	0.003		0.2	IC97-73	8.53	10.06	1.53	0.77	0.008		1
IC96-06	17.48	18.5	1.02	0.69	0.002		0.2	IC97-73	10.06	11.73	1.67	1.30	0.008		0
IC96-06	18.5	19.51	1.01	0.97	0.003		0	IC97-73	11.73	13.41	1.68	0.44	0.004		0
IC96-06	19.51	20.5	0.99	2.92	0.003		0	IC97-73	13.41	14.78	1.37	0.24	0.003		0
IC96-06	20.5	21.34	0.84	2.98	0.002		0	IC97-73	14.78	16.31	1.53	0.01	0.003		0
IC96-06	21.34	22	0.66	1.07	0.002		0	IC97-73	16.31	17.68	1.37	0.03	0.003		0
IC96-06	22	22.6	0.6	2.47	0.003		0.2	IC97-73	17.68	19.2	1.52	0.04	0.003		0
IC96-06	22.6	23.77	1.17	1.37	0.004		0.2	IC97-73	19.2	20.73	1.53	0.01	0.002		0
IC96-06	23.77	24.6	0.83	1.14	0.004		0	IC97-74	1.22	2.74	1.52	0.24	0.002		1.4
IC96-06	24.6	25.45	0.85	1.78	0.004		0	IC97-74	2.74	4.27	1.53	0.24	0.001		0.6
IC96-06	25.45	26.4	0.95	5.15	0.021		0	IC97-74	4.27	5.8	1.53	0.28	0.001		0.2
IC96-06	26.4	27.13	0.73	0.4	0.007		0	IC97-74	5.8	7.32	1.52	0.19	0.001		0
IC96-08	13.41	14.94	1.53	0.42	0.006		0	IC97-74	40.84	42.37	1.53	0.02	0.003		0
IC96-08	14.94	16.92	1.98	0.39	0.036	0.02	0	IC97-75	6	7.92	1.92	0.45	0.003		0.2
IC96-08	16.92	18	1.08	1.7	0.045	0.02	0	IC97-75	7.92	9.45	1.53	0.47	0.002		0.2
IC96-08	18	19.02	1.02	2.06	0.078	0.02	0	IC97-75	9.45	11.35	1.9	0.51	0.002		0.2
IC96-08	19.02	20.3	1.28	4.99	0.073	0.02	1	IC97-75	11.35	13.26	1.91	0.39	0.002		0.2
IC96-08	20.3	21.8	1.5	2.35	0.021	0.01	0	IC97-75	13.26	14.78	1.52	0.29	0.002		0
IC96-08	21.8	22.9	1.1	1.99	0.039	0.03	0	IC97-75	14.78	16.31	1.53	0.24	0.002		0
IC96-08	22.9	24.08	1.18	1.63	0.064	0.025	0	IC97-75	16.31	18.29	1.98	0.25	0.002		0
IC96-08	24.08	25.6	1.52	2.36	0.006	0.01	0	IC97-75	18.29	19.81	1.52	0.25	0.003		0
IC96-08	25.6	26.5	0.9	2.75	0.006		0	IC97-75	19.81	21.34	1.53	0.41	0.003		0
IC96-08	26.5	27.8	1.3	0.6	0.010		0	IC97-75	21.34	22.71	1.37	0.24	0.004		0
IC96-09	20.73	24.69	3.96	0.89	0.003		0	IC97-76	10.67	12.19	1.52	0.14	0.003		0
IC96-09	24.69	25.95	1.26	1.82	0.005		0	IC97-76	12.19	13.11	0.92	0.01	0.004		0
IC96-09	25.95	27.83	1.88	0.58	0.004	0.015	0	IC97-76	13.11	14.48	1.37	0.01	0.005		0
IC96-09	27.83	28.65	0.82	0.7	0.004		0	IC97-76	14.48	15.85	1.37	0.32	0.006		0
IC96-09	28.65	29.87	1.22	0.5	0.004		0	IC97-76	15.85	17.53	1.68	0.24	0.008		0
IC96-09	29.87	30.95	1.08	0.99	0.032	0.1	1	IC97-76	17.53	18.44	0.91	0.26	0.008		0
IC96-09	30.95	32.35	1.4	1.72	0.069	0.025	1	IC97-77	1.22	2.74	1.52	0.01	0.003		0
IC96-09	32.35	33.22	0.87	0.83	0.008		0	IC97-77	2.74	4.27	1.53	0.02	0.003		0
IC96-09	33.22	34.75	1.53	1.22	0.007		0	IC97-77	4.27	5.79	1.52	0.06	0.004		0
IC96-09	34.75	36.27	1.52	1.41	0.007		0.2	IC97-77	5.79	7.32	1.53	0.48	0.010		0
IC96-09	36.27	37.79	1.52	1.52	0.008	0.015	0.4	IC97-77	7.32	8.84	1.52	1.06	0.003		0
IC96-09	37.79	39.55	1.76	1.18	0.009	0.01	0.2	IC97-77	8.84	11.89	3.05	0.00	0.000		0
IC96-09	39.55	40.84	1.29	1.64	0.102	0.07	1	IC97-77	11.89	13.41	1.52	0.05	0.001		59
IC96-09	40.84	42	1.16	1.69	0.054	0.03	0	IC97-77	13.41	14.94	1.53	0.05	0.000		53
IC96-09	42	43.5	1.5	2.18	0.065	0.04	1	IC97-77	14.94	16.46	1.52	0.00	0.000		0
IC96-09	43.5	45.42	1.92	0.71	0.004		0	IC97-77	16.46	18	1.54	0.01	0.000		60.2
IC96-09	45.42	46.94	1.52	1.05	0.009	0.025	0	IC97-77	18	19.51	1.51	0.66	0.002		0.2
IC96-09	46.94	48	1.06	1.01	0.007	0.025	1.2	IC97-77	19.51	21.34	1.83	1.16	0.004		0
IC96-09	48	49.23	1.23	1.64	0.007	0.03	1.2	IC97-77	21.34	23.01	1.67	0.54	0.005		0
IC96-09	49.23	50.9	1.67	0.91	0.007	0.025	0.4	IC97-77	23.01	24.38	1.37	0.26	0.010		0
IC96-09	50.9	53.04	2.14	0.39	0.006		0.2	IC97-77	24.38	25.91	1.53	0.19	0.009		0
IC96-12	26.06	27.43	1.37	0.35	0.011		0	IC97-79	14.78	16.31	1.53	0.11	0.003		0
IC96-13	46.72	47.4	0.68	0.43	0.007		0	IC97-79	37.19	38.91	1.72	0.19	0.006		0.2
IC96-13	47.4	48.58	1.18	3.61	0.005		0	IC97-79	38.91	40.23	1.32	0.10	0.007		0

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC96-13	48.58	49.99	1.41	2.9	0.005	0.03	0	IC97-79	40.23	41.76	1.53	0.29	0.007		0
IC96-13	49.99	51.28	1.29	1.37	0.003	0.07	5	IC97-79	41.76	42.98	1.22	0.39	0.009		0
IC96-13	51.28	53.04	1.76	1.27	0.015	0.27	9	IC97-79	42.98	44.5	1.52	0.18	0.009		0
IC96-13	53.04	54.56	1.52	1.64	0.043	0.38	8	IC97-79	44.5	45.72	1.22	0.46	0.007		0
IC96-13	54.56	55.83	1.27	4.35	0.081	0.425	12	IC97-79	45.72	47.22	1.5	0.21	0.007		0.2
IC96-13	55.83	57.03	1.2	1.83	0.005	0.04	1	IC97-79	47.22	48.65	1.43	0.24	0.006		3.2
IC96-14	2.9	4.57	1.67	0.56	0.008	0.03	2.4	IC97-80	15.85	17.25	1.4	0.01	0.004		0
IC96-14	5.33	6.71	1.38	0.94	0.012	0.015	1.2	IC97-80	19.2	20.88	1.68	0.01	0.004		0
IC96-14	8.2	8.83	0.63	0.4	0.009	0.005	0.4	IC97-81	3.2	4.57	1.37	0.07	0.004		0.2
IC96-14	8.83	9.75	0.92	0.41	0.006		0.2	IC97-81	4.57	6.4	1.83	0.06	0.004		0
IC96-14	10.97	12.19	1.22	0.91	0.004		0	IC97-81	7.77	9.14	1.37	0.09	0.003		0.4
IC96-14	12.19	14.17	1.98	0.57	0.002		0	IC97-81	9.14	10.36	1.22	0.00	0.000		0
IC96-14	14.17	16.15	1.98	0.42	0.003	0.035	0.2	IC97-81	10.36	11.89	1.53	1.40	0.015		1.8
IC96-14	16.15	17.37	1.22	2.04	0.004		0	IC97-81	11.89	13.41	1.52	0.36	0.006		0.2
IC96-14	17.37	18.9	1.53	2.23	0.004		0	IC97-81	13.41	14.94	1.53	0.33	0.011		0.2
IC96-14	18.9	20.12	1.22	1.69	0.004		0.2	IC97-81	14.94	16.6	1.66	0.46	0.018		0.8
IC96-14	20.12	21.05	0.93	1.15	0.009	0.055	0.2	IC97-81	16.6	17.98	1.38	1.56	0.043		2
IC96-14	21.05	21.34	0.29	3.72	0.052	0.33	23.4	IC97-81	17.98	19.43	1.45	1.77	0.044		2.8
IC96-14	21.34	23.16	1.82	1.93	0.014	0.04	5	IC97-81	19.43	20.75	1.32	0.25	0.029		0.6
IC96-14	23.16	24.5	1.34	1.07	0.019	0.025	0.2	IC97-81	20.75	22	1.25	0.10	0.004		0.2
IC96-14	24.5	24.99	0.49	1.37	0.029	0.01	0	IC97-81	22	23.2	1.2	0.12	0.003		0
IC96-14	24.99	26.3	1.31	3.43	0.039	0.045	0.2	IC97-81	23.2	24.4	1.2	0.17	0.003		0
IC96-14	26.3	28.96	2.66	0.73	0.044	0.02	0.8	IC97-81	24.4	25.6	1.2	0.17	0.003		0
IC96-14	28.96	29.65	0.69	1.08	0.004		0.2	IC97-81	25.6	26.8	1.2	0.26	0.003		1.4
IC96-14	29.65	31.09	1.44	0.53	0.005		0	IC97-81	26.8	28.85	2.05	0.35	0.010		0.6
IC96-14	31.09	32.61	1.52	0.79	0.004		0.2	IC97-81	28.85	30.5	1.65	0.09	0.005		0
IC96-14	32.61	34.44	1.83	0.82	0.004		0	IC97-81	30.5	32.3	1.8	0.02	0.005		0
IC96-15	0	7.32	7.32	2.03	0.004		0.4	IC97-82	5.64	6.7	1.06	0.17	0.001		6.4
IC96-15	24.4	26.9	2.5	0.42	0.009		0.2	IC97-82	25.04	26.3	1.26	0.65	0.085		0
IC96-15	48.46	49.99	1.53	0.3	0.016	0.01	0.8	IC97-83	17.98	19.35	1.37	0.07	0.005		0
IC96-16	12.5	13.72	1.22	0.36	0.004		0	IC97-84	10.28	11.89	1.61	0.10	0.007		0
IC96-16	13.72	15.85	2.13	0.37	0.003		0	IC97-84	11.89	14.17	2.28	0.54	0.005		0
IC96-16	15.85	18.15	2.3	0.43	0.003		0	IC97-84	14.17	15.65	1.48	2.57	0.004		0
IC96-16	20.42	22.1	1.68	0.66	0.034	0.13	1.4	IC97-84	15.85	17.68	1.83	0.48	0.055		2.6
IC96-16	22.1	23.77	1.67	0.81	0.020	0.05	0.2	IC97-84	17.68	18.9	1.22	1.92	0.062		7.4
IC96-16	23.77	26.21	2.44	2.12	0.015	0.03	0.4	IC97-84	18.9	20.12	1.22	2.67	0.063		9.2
IC96-16	26.21	27.58	1.37	2.4	0.011	0.02	0.4	IC97-84	20.12	21.95	1.83	2.33	0.053		9.8
IC96-16	27.58	28.96	1.38	1.95	0.009		0	IC97-84	21.95	23.48	1.53	2.84	0.040		9.4
IC96-17	5.79	8.23	2.44	0.42	0.005		0	IC97-85	14.48	15.7	1.22	0.31	0.006		0
IC96-17	8.23	9.75	1.52	0.35	0.005		0	IC97-85	15.7	17.05	1.35	0.36	0.008		0
IC96-17	12	14.48	2.48	0.35	0.005		0	IC97-85	18.9	20.42	1.52	0.15	0.003		0
IC96-17	17.07	18.59	1.52	0.53	0.005		0	IC97-85	21.95	23.47	1.52	0.67	0.007		0
IC96-17	18.59	20.12	1.53	0.34	0.005		0	IC97-85	23.47	25.4	1.93	0.74	0.009		0
IC96-17	22	23.32	1.32	1.61	0.016		0.2	IC97-85	26.52	28.04	1.52	0.18	0.006		0
IC96-18	17.98	19.51	1.53	0.65	0.006	0.04	2.8	ID97-01	80.16	81.69	1.53	0.01	0.005		0
IC96-18	21.22	22.56	1.34	0.4	0.004	0.06	0.8	ID97-01	83.12	84.28	1.16	4.54	0.102	0.63	16
IC96-18	22.56	24.22	1.66	0.36	0.004	0.03	0.6	ID97-01	84.28	85.8	1.52	2.16	0.092	0.575	13
IC96-18	27.03	28.65	1.62	1.18	0.006	0.09	1.6	ID97-01	88.09	89.61	1.52	2.23	0.107	0.69	30
IC96-18	28.65	29.7	1.05	1.05	0.006	8E-05	1.4	ID97-01	89.61	91.09	1.48	2.11	0.082	0.67	23

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC96-18	29.7	30.24	0.54	2.03	0.018	2E-04	4.4	ID97-01	91.09	92.66	1.57	0.02	0.004		0
IC96-18	34.75	36.27	1.52	1	0.019	0.015	1	ID97-01	95.4	96.77	1.37	0.30	0.012		1
IC96-20	10.36	13.41	3.05	0.39	0.010		0	ID97-01	141.43	143.02	1.59	0.31	0.009	0.025	1
IC96-20	13.41	15.8	2.39	0.62	0.007		0	ID97-01	143.02	144.17	1.15	0.02	0.005		0
IC96-20	15.8	17.37	1.57	0.37	0.006		0	ID97-01	144.17	145.69	1.52	0.03	0.004		0
IC96-20	17.37	19.96	2.59	0.47	0.006	0.02	0	ID97-01	145.69	147.07	1.38	0.02	0.004		0
IC96-20	19.96	21.96	2	0.46	0.006		0	ID97-02	81.05	82.5	1.45	0.01	0.004		0
IC96-20	24.08	27.13	3.05	0.58	0.004	0.03	1.6	ID97-02	83.14	83.8	0.66	0.04	0.001		0
IC96-20	27.13	30.18	3.05	0.36	0.010	0.01	0.6	ID97-02	83.8	84.73	0.93	2.91	0.048	0.395	8
IC96-20	37.5	39.32	1.82	0.34	0.005		0.2	ID97-02	88.41	89.74	1.33	0.92	0.007		1
IC96-20	48.2	49.99	1.79	0.45	0.022	0.025	1	ID97-02	119.89	121.34	1.45	0.04	0.003		0
IC96-20	49.99	51.1	1.11	0.32	0.010	0.02	0.6	ID97-02	121.34	122.83	1.49	0.83	0.021	0.025	1
IC96-21	7.92	9.75	1.83	0.43	0.003		0	ID97-02	129.67	130.75	1.08	0.20	0.014	0.04	0
IC96-23	10.97	12.95	1.98	0.37	0.004	0.025	1.4	ID97-03	94.06	95.7	1.64	2.84	0.050	0.35	8
IC96-23	12.95	14.94	1.99	0.33	0.005	0.01	0.4	ID97-03	95.7	97.14	1.44	1.68	0.092	0.505	7
IC96-25	7.62	9.75	2.13	0.33	0.009		0	ID97-04	55.71	57	1.29	0.05	0.003		0
IC96-25	9.75	11.58	1.83	0.34	0.007		0.2	ID97-04	57	57.9	0.9	0.12	0.005		0.8
IC96-25	11.58	15.24	3.66	0.35	0.006		0	ID97-04	57.9	58.85	0.95	0.04	0.003		0
IC96-25	15.24	16.78	1.54	0.38	0.010		0	ID97-04	74.68	76.18	1.5	0.05	0.004		0.8
IC96-25	18.9	21.03	4.25	0.8	0.009		0	ID97-04	76.18	77.42	1.24	0.03	0.004		0.2
IC96-26	11.28	13.4	2.12	0.32	0.006	0.04	1.8	ID97-05	99.24	100.28	1.04	0.58	0.015	0.07	2.6
IC96-27	9.75	11.58	1.83	0.38	0.004		0	ID97-05	114	115.52	1.52	0.01	0.006		0.6
IC96-27	24.84	26.82	1.98	0.38	0.007		0	ID97-05	122.53	124	1.47	0.01	0.031		0.2
IC96-27	26.82	27.85	1.03	0.79	0.047		0	ID97-05	124	125.3	1.3	0.01	0.015		1
IC96-29	13.11	15.85	2.74	0.4	0.007		0	ID97-05	216.87	218.39	1.52	0.01	0.001		0
IC96-29	19.2	20.73	1.53	0.3	0.004		0	ID97-05	220.68	221.59	0.91	0.00	0.001		0
IC96-29	20.73	21.95	1.22	0.95	0.006		0	ID97-05	221.59	222.96	1.37	0.01	0.001		0
IC96-29	23.16	24.38	1.22	0.3	0.004		0	ID97-05	223.72	224.94	1.22	0.00	0.001		0
IC96-29	24.38	25.7	1.32	1.04	0.007	0.1	1.6	ID97-05	224.94	226.31	1.37	0.01	0.001		0
IC96-29	25.7	26.97	1.27	1.99	0.044	0.57	8.4	ID97-05	226.31	227.38	1.07	0.01	0.001		0
IC96-29	26.97	28.15	1.18	0.89	0.004	0.01	0	ID97-05	227.38	228.3	0.92	0.01	0.001		0.4
IC96-29	28.15	29.41	1.26	0.46	0.007		0	ID97-05	228.3	229.21	0.91	0.01	0.001		0.2
IC96-29	32.31	33.83	1.52	0.42	0.006		0	ID97-05	232.26	233.78	1.52	0.01	0.001		0.2
IC96-30	53.77	54	0.23	1.69	0.050	0.6	11.8	ID97-07	104.59	105.46	0.87	0.11	0.003		0.6
IC96-32	30.1	30.5	0.4	0.45	0.009	0.365	3.8	ID97-09	60.96	63.71	2.75	0.01	0.001		0
IC96-34	72.1	73.5	1.4	1.23	0.083	0.24	1.5	ID97-11	93.88	94.49	0.61	2.77	0.041	0.05	1
IC96-34	73.5	74.7	1.2	4.97	0.084	0.19	4.2	ID97-11	94.49	95.25	0.76	0.09	0.004		0
IC96-34	74.7	76.1	1.4	12.4	0.140	0.48	62	ID97-11	95.25	96.01	0.76	0.08	0.004		0
IC96-34	76.1	77.42	1.32	8.71	0.133	0.65	52.4	ID97-11	109.2	110.53	1.33	0.02	0.002		0
IC96-34	77.42	78.94	1.52	5.06	0.074	0.52	31	ID97-11	110.53	111.86	1.33	0.02	0.003		0
IC96-34	78.94	80.47	1.53	9.17	0.019	0.4	49.6	ID97-11	111.86	113.39	1.53	0.03	0.003		0.2
IC96-34	80.47	81.99	1.52	3.45	0.036	0.54	21	ID97-11	113.39	114.02	0.63	2.93	0.018	0.06	8.8
IC96-34	81.99	83.52	1.53	3.84	0.069	1	38	ID97-11	114.02	115.62	1.6	0.01	0.003		0
IC96-34	83.52	85.04	1.52	3.52	0.056	0.67	27.1	ID97-11	115.62	117.13	1.51	0.15	0.004		0.4
IC96-34	85.04	86.56	1.52	3.67	0.030	0.66	21	ID97-11	117.13	118.85	1.72	0.01	0.003		0
IC96-34	86.56	88.09	1.53	4.47	0.027	0.65	20.1	ID97-11	125.91	127.63	1.72	0.04	0.005		0
IC96-34	88.09	89.61	1.52	3.03	0.025	0.67	19.4	ID97-11	127.63	128.96	1.33	0.01	0.003		0
IC96-34	89.61	91.14	1.53	3.88	0.028	0.71	23.1	ID97-11	128.96	130.45	1.49	0.01	0.003		0
IC96-34	91.14	92.66	1.52	6.06	0.060	0.88	35.6	ID97-11	130.45	132.08	1.63	0.29	0.020		3.6

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC96-34	94.18	95.71	1.53	0.381	0.007		1.6	ID97-11	133.41	134.9	1.49	0.86	0.019	0.095	4
IC97-35	7.92	8.38	0.46	0.65	0.002		0.4	ID97-11	142.07	143.2	1.13	0.03	0.017		0.8
IC97-35	12.5	13.41	0.91	0.5	0.004		1.2	ID97-11	147.07	148.29	1.22	0.02	0.032		1
IC97-35	13.41	14.63	1.22	0.7	0.003		2.2	ID97-11	148.29	149.55	1.26	0.03	0.015		0.4
IC97-35	14.63	15.96	1.33	0.86	0.028		0	ID97-11	149.55	150.88	1.33	0.07	0.016		0.4
IC97-35	15.96	16.46	0.5	1.15	0.027		0.2	ID97-11	150.88	152.4	1.52	0.05	0.019		1
IC97-35	16.46	17.37	0.91	0.72	0.028	0.025	1	ID97-11	152.4	153.92	1.52	0.05	0.018		0.2
IC97-35	17.37	18.9	1.53	0.69	0.078	0.03	1	ID97-11	153.92	155.45	1.53	0.08	0.018		2.2
IC97-35	18.9	20.07	1.17	0.51	0.017	0.02	0	ID97-11	155.45	156.97	1.52	0.00	0.038		0.2
IC97-35	20.07	21.03	0.96	1.07	0.008	0.015	1	ID97-11	156.97	158.31	1.34	0.01	0.051		0.6
IC97-35	21.03	22.56	1.53	1.34	0.012		0	ID97-11	158.31	159.68	1.37	0.01	0.039		0.2
IC97-35	22.56	23.7	1.14	1.86	0.015	0.005	0	ID97-11	159.68	161.21	1.53	0.01	0.027		0
IC97-35	23.7	24.57	0.87	3.17	0.090	0.05	0	ID97-11	161.21	162.2	0.99	0.02	0.030		0
IC97-35	24.57	26	1.43	1.83	0.008	0.005	0	ID97-11	162.2	163.07	0.87	0.20	0.017	0.01	0.18
IC97-35	26	26.7	0.7	1.13	0.005	0.01	0	ID97-11	163.07	164.59	1.52	0.91	0.013	0.01	0.83
IC97-35	26.7	27.58	0.88	1.46	0.003		0.4	ID97-11	164.59	166.12	1.53	0.61	0.010	0.01	0.58
IC97-35	27.58	29.4	1.82	0.57	0.004		0.2	ID97-11	166.12	167.18	1.06	0.26	0.006	0.01	0.25
IC97-36	6.25	6.77	0.52	0.44	0.005		0	ID97-12	45.1	45.36	0.26	0.47	0.010		3.4
IC97-36	7.62	9.04	1.42	0.47	0.008		0	ID97-12	87.3	88.69	1.39	0.01	0.003		0
IC97-36	9.04	10.76	1.72	0.42	0.008		0	ID97-12	88.69	89.3	0.61	0.01	0.003		0.2
IC97-36	10.76	11.58	0.82	0.51	0.008		0	ID97-12	89.3	90.15	0.85	0.01	0.004		0.2
IC97-36	15.85	17.07	1.22	0.45	0.017		0	ID97-12	94.64	95.71	1.07	0.21	0.029	0.08	3
IC97-36	18.17	19.51	1.34	0.63	0.029	0.015	0.2	ID97-12	96.93	98.15	1.22	0.30	0.035	0.1	3
IC97-36	19.51	21.04	1.53	2.38	0.032	0.02	0	ID97-12	98.15	99.3	1.15	0.49	0.045	0.265	6.8
IC97-36	21.04	22.55	1.51	3.01	0.014	0.03	0.8	ID97-12	99.3	100.43	1.13	0.46	0.038	0.14	3.6
IC97-36	22.55	23.34	0.74	2.7	0.011		0	ID97-12	100.43	101.7	1.27	0.24	0.010	0.075	1.8
IC97-36	23.34	23.84	0.5	3.2	0.038	0.05	0.6	ID97-12	101.7	103.33	1.63	0.40	0.013	0.15	3.2
IC97-36	23.84	24.84	1	1.75	0.004		0	ID97-12	103.33	104.85	1.52	0.27	0.011	0.12	1
IC97-36	24.84	25.32	0.48	2.23	0.031	0.02	0.6	ID97-12	104.85	106.38	1.53	0.35	0.013	0.045	1
IC97-36	25.32	26.52	1.2	2.51	0.007		0	ID97-12	106.38	107.9	1.52	0.41	0.012	0.02	0.8
IC97-37	6.4	7.62	1.22	0.31	0.003		0	ID97-12	112.47	114	1.53	0.23	0.016	0.075	1
IC97-37	8.84	10.36	1.52	0.36	0.002		0	ID97-12	115.52	117.04	1.52	0.24	0.013	0.055	0.6
IC97-37	10.36	11.3	0.94	0.45	0.003		0.4	ID97-12	117.04	118.57	1.53	0.50	0.012	0.03	1.4
IC97-37	11.3	12.19	0.89	0.4	0.002		0.8	ID97-12	118.57	120.09	1.52	1.61	0.013	0.065	2.4
IC97-37	13.41	14.74	1.33	0.43	0.003		0	ID97-12	121.62	122.85	1.23	1.21	0.035	0.075	4.8
IC97-37	14.74	15.5	0.76	0.46	0.009		0	ID97-12	122.85	124.1	1.25	1.60	0.039	0.07	4.8
IC97-37	15.5	16.46	0.96	0.32	0.013		0	ID97-12	124.1	125.5	1.4	0.66	0.034	0.05	5.2
IC97-37	16.46	17.98	1.52	0.38	0.025		0	ID97-12	125.5	126.19	0.69	0.11	0.010	0.05	0.6
IC97-37	17.98	19.51	1.53	0.42	0.026		0	ID97-12	126.19	127.23	1.04	0.63	0.019	0.03	1.4
IC97-37	19.51	20.27	0.76	0.37	0.027		0	ID97-12	127.23	128.6	1.37	0.22	0.051	0.06	1.2
IC97-37	20.27	22.56	2.29	0.48	0.023		0	ID97-12	128.6	129.93	1.33	0.04	0.027		0.2
IC97-37	24.69	25.6	0.91	0.78	0.004		0	ID97-12	131.03	132.2	1.17	0.06	0.034		0.2
IC97-37	25.6	28.65	3.05	0.54	0.019		0	ID97-12	132.2	133.5	1.3	0.04	0.013		0.2
IC97-38	10.36	11.46	1.1	0.64	0.075	0.035	0	ID97-12	140.62	141.43	0.81	0.01	0.006		0
IC97-38	11.46	14.63	3.17	0.95	0.072	0.04	0	ID97-12	141.43	142.95	1.52	0.00	0.002		0
IC97-38	14.63	15.83	1.2	0.54	0.058	0.02	0	ID97-12	142.95	144.48	1.53	0.00	0.002		0
IC97-38	15.83	17.23	1.4	2.22	0.041	0.02	0	ID97-12	144.48	145.82	1.34	0.01	0.003		0
IC97-38	17.23	18.18	0.95	2.14	0.027	0.015	0	ID97-12	145.82	146.72	0.9	0.00	0.002		0
IC97-38	18.18	18.88	0.7	1.38	0.013	0.01	0	ID97-12	146.72	147.52	0.8	0.01	0.003		0

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC97-38	18.88	19.94	1.06	1.3	0.014	0.03	0	ID97-12	147.52	148.44	0.92	0.01	0.002		0
IC97-38	19.94	21.03	1.09	1.05	0.031	0.03	0	ID97-12	148.44	149.35	0.91	0.01	0.003		0
IC97-38	22.56	24.23	1.67	0.34	0.057	0.02	0	ID97-13	85.92	87.34	1.42	0.01	0.003		0
IC97-38	24.23	25.9	1.67	0.52	0.035	0.025	0	ID97-13	87.34	88.62	1.28	0.01	0.004		0
IC97-38	25.9	27.13	1.23	1.65	0.014		0.4	ID97-13	88.62	89	0.38	0.21	0.019		0.6
IC97-39	3.81	5.33	1.52	0.3	0.001		2.6	ID97-13	93.72	95.15	1.43	5.44	0.154	0.56	42.2
IC97-39	5.33	6.886	1.556	0.41	0.001		1.2	ID97-13	95.15	96.29	1.14	8.43	0.131	0.58	29.4
IC97-39	6.886	7.72	0.834	0.35	0.003		0.6	ID97-13	96.29	97.23	0.94	10.20	0.168	0.39	14
IC97-39	7.72	9.75	2.03	1.89	0.008		2.2	ID97-13	97.23	98.76	1.53	7.96	0.104	0.645	21.2
IC97-39	9.75	11.11	1.36	2.32	0.008		1.6	ID97-13	98.76	99.97	1.21	7.58	0.101	0.83	25
IC97-39	11.11	11.89	0.78	1.49	0.003		0.8	ID97-13	99.97	101	1.03	7.48	0.066	0.765	20
IC97-39	11.89	13.41	1.52	1.42	0.004		0	ID97-13	101	101.8	0.8	1.85	0.022	0.27	2.2
IC97-39	13.41	14.63	1.22	0.88	0.013		0	ID97-13	101.8	103.08	1.28	1.40	0.014	0.07	1.4
IC97-39	14.63	17.07	2.44	0.42	0.020		0	ID97-13	103.08	104.12	1.04	3.15	0.035	0.04	3.4
IC97-39	18.55	21.67	3.12	0.75	0.022		0	ID97-13	105.16	106.68	1.52	1.20	0.034		1.4
IC97-40	10.36	11.28	0.92	0.39	0.004		0	ID97-13	117.04	118.57	1.53	1.60	0.033		5.8
IC97-40	13.41	14.17	0.76	0.35	0.003		0	ID97-13	120.93	122.55	1.62	0.03	0.004		0
IC97-40	14.17	15.85	1.68	0.49	0.003		0	ID97-13	122.55	123.8	1.25	0.03	0.006		0
IC97-40	15.85	17.07	1.22	3.4	0.004		0	ID97-13	123.8	124.66	0.86	0.04	0.054		0.2
IC97-40	17.07	18.59	1.52	1.55	0.004		0	ID97-13	124.66	126.19	1.53	0.03	0.036		0.2
IC97-40	18.59	19.81	1.22	1.8	0.003		0	ID97-13	126.19	127	0.81	0.11	0.025		0.2
IC97-40	19.81	20.8	0.99	2.09	0.005		0	ID97-13	127	127.71	0.71	0.01	0.004		0
IC97-40	20.8	21.56	0.76	3.64	0.005		0	ID97-13	127.71	129.24	1.53	0.03	0.023		0.2
IC97-40	21.56	22.56	1	2.05	0.005		0	ID97-13	129.24	130.76	1.52	0.35	0.015		0.2
IC97-41	6.71	8.38	1.67	0.3	0.006		0	ID97-13	139.75	141.04	1.29	0.01	0.002		0
IC97-41	12.34	13.41	1.07	0.54	0.005		0	ID97-14	104.25	105.47	1.22	0.01	0.004	0	0.2
IC97-41	13.41	14.38	0.97	0.38	0.005		0	ID97-14	105.47	107.14	1.67	0.01	0.004	0	0.4
IC97-41	14.38	14.94	0.56	0.99	0.002		0	ID97-14	107.14	108.12	0.98	0.24	0.007	0.3	13
IC97-41	14.94	16.07	1.13	6.54	0.008		0	ID97-14	108.12	108.93	0.81	0.59	0.027	0.48	22
IC97-46	19.26	21.34	2.08	4.25	0.029	0.435	3.8	ID97-16	136.23	137.87	1.64	0.03	0.003		0
IC97-46	21.34	22.56	1.22	2.45	0.052	0.305	4	ID97-16	137.87	139.3	1.43	0.01	0.003		0
IC97-46	22.56	23.47	0.91	4.51	0.072	0.22	5.4	ID97-18	84.84	86.16	1.32	0.01	0.003		0.2
IC97-46	23.47	24.38	0.91	4.74	0.072	0.17	5.2	ID97-18	86.16	86.31	0.15	2.71	0.051		2
IC97-46	24.38	25.76	1.38	2.57	0.053	0.09	2.6	ID97-18	86.31	87.33	1.02	0.22	0.003		0.4
IC97-46	25.76	26.12	0.36	5.04	0.034	0.125	4	ID97-18	140.49	141.88	1.39	0.01	0.003		0
IC97-46	26.12	27.53	1.41	0.86	0.010	0.015	0.6	ID97-18	141.88	143.26	1.38	0.02	0.003		0
IC97-46	27.53	28.42	0.89	0.58	0.003		0	ID97-18	143.26	144.73	1.47	0.01	0.003		0
IC97-46	28.42	30.43	2.01	0.72	0.004		0.2	ID97-18	144.73	146.3	1.5	0.41	0.016		6
IC97-46	30.43	32	1.57	9.94	0.051	0.17	4.4	ID97-18	146.3	147.83	1.54	0.03	0.007		1
IC97-46	32	33.53	1.53	9.17	0.066	0.235	4	ID97-18	147.83	149	1.05	0.04	0.017		2.2
IC97-46	33.53	34.75	1.22	10.9	0.031	0.235	3	ID97-18	149	150.48	1.48	0.01	0.003		0
IC97-46	34.75	35.66	0.91	6.25	0.066	0.19	2.8	ID97-18	150.48	152.04	1.56	0.14	0.009		0.6
IC97-46	35.66	36.88	1.22	0.48	0.005	0.01	0	ID97-18	152.04	153.53	1.49	0.09	0.018		0.8
IC97-46	36.88	38.4	1.52	1.29	0.003	0.015	0.8	ID97-18	153.53	154.85	1.32	0.04	0.014		0.2
IC97-46	38.4	39.93	1.53	1.49	0.004	0.01	0.2	ID97-18	154.85	156.05	1.2	0.01	0.024		0.4
IC97-46	39.93	41.3	1.37	0.97	0.007		0	ID97-18	156.05	157.42	1.37	0.01	0.012		0.2
IC97-46	41.3	42.37	1.07	1.17	0.008		0.4	ID97-18	157.42	158.85	1.43	0.01	0.012		0.2
IC97-46	42.37	43.59	1.22	0.56	0.007	0.01	0	ID97-18	158.85	160.02	1.17	0.00	0.009		0.4
IC97-46	43.59	44.35	0.76	2.12	0.010	0.02	0.8	ID97-18	160.02	161.54	1.52	0.01	0.011		0.6

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC97-46	44.35	45.87	1.52	0.347	0.011		0	ID97-18	161.54	163.07	1.53	0.01	0.011		0.6
IC97-46	45.87	46.94	1.07	0.318	0.009		0	ID97-18	163.07	164.59	1.52	0.00	0.011		0.2
IC97-47	7.62	9.14	1.52	0.359	0.005		0	ID97-18	166.12	167.64	1.52	0.00	0.014		0.6
IC97-47	10.66	11.32	0.66	1.18	0.003		0	ID97-18	168.24	169.76	1.52	0.01	0.003		0.2
IC97-47	11.32	12.75	1.43	2.51	0.003		0	ID97-18	169.76	170.84	1.08	0.01	0.003		0.4
IC97-47	12.75	13.81	1.06	2.89	0.003		0	ID97-18	170.84	172.21	1.37	0.01	0.003		0.6
IC97-47	13.81	15.09	1.28	1.95	0.003		0	ID97-19	60.6	60.96	0.36	0.64	0.004		0.4
IC97-47	15.09	17.07	1.98	1.93	0.003		0	ID97-19	64.73	65.75	1.02	0.01	0.001		0
IC97-47	17.07	17.68	0.61	2.77	0.004		0	ID97-19	89.61	91.13	1.52	0.01	0.002		0
IC97-47	17.68	18.9	1.22	1.74	0.003		0	ID97-19	91.13	92.66	1.53	0.01	0.003		0
IC97-47	18.9	20.42	1.52	1.43	0.006		0	ID97-19	92.66	93.9	1.24	0.01	0.003		0
IC97-47	20.42	21.64	1.22	0.46	0.007		0	ID97-19	93.9	95.45	1.55	1.76	0.073	0.35	4.6
IC97-47	21.64	23.16	1.52	0.51	0.008		0	ID97-19	95.45	96.25	0.8	4.22	0.051	0.71	20.4
IC97-47	23.16	24.69	1.53	0.55	0.008		0	ID97-19	96.25	97.65	1.4	0.04	0.002		0
IC97-48	10.97	12.34	1.37	0.43	0.003		0	ID97-19	149.96	151.49	1.53	1.07	0.012	0.03	5
IC97-48	12.34	14.02	1.68	1.01	0.003		0	ID97-19	151.49	153.01	1.52	0.87	0.012	0.03	3.8
IC97-48	14.02	15.07	1.05	0.83	0.003		0	ID97-19	153.01	154.53	1.52	1.29	0.016	0.065	7.8
IC97-48	15.07	16.96	1.89	1.25	0.004		0	ID97-19	154.53	156.06	1.53	1.16	0.020	0.05	7.4
IC97-48	16.96	18.59	1.63	0.83	0.005		0	ID97-19	156.06	157.58	1.52	0.49	0.012	0.035	3
IC97-48	18.59	20	1.41	0.37	0.006		0	ID97-19	157.58	158.95	1.37	0.54	0.012	0.04	3.2
IC97-49	12.6	13.18	0.58	0.46	0.036		0.4	ID97-20	91.9	93.28	1.38	3.41	0.007	0.725	18.2
IC97-49	13.18	14.33	1.15	2.19	0.021		0.8	ID97-20	93.28	94.32	1.04	0.51	0.005	0.305	1.4
IC97-49	14.33	15.54	1.21	2.77	0.021		1	ID97-20	94.32	95.86	1.54	0.05	0.002		0
IC97-49	15.54	17.07	1.53	2.56	0.009		0.6	ID97-20	95.86	97.54	1.68	0.04	0.002		0
IC97-49	17.07	17.85	0.78	1.28	0.006		0.4	ID97-20	97.54	99.21	1.67	0.03	0.002		0
IC97-49	17.85	18.75	0.9	1.96	0.011		0.2	ID97-20	129.84	131.37	1.53	0.01	0.003		0
IC97-49	18.75	20.27	1.52	0.75	0.016		0	ID97-20	131.37	132.82	1.45	0.01	0.003		0
IC97-49	22.86	24.38	1.52	0.32	0.010		0	ID97-20	135.84	136.86	1.02	0.54	0.026	0.02	0.8
IC97-49	24.38	25.3	0.92	0.49	0.007		0	ID97-20	136.86	138.07	1.21	1.19	0.046	0.055	2.2
IC97-49	25.3	26.21	0.91	0.67	0.010		0	ID97-20	138.07	139.19	1.12	0.95	0.014	0.035	1.2
IC97-49	26.21	27.73	1.52	0.34	0.007		0.6	ID97-20	139.19	139.9	0.71	0.15	0.006		0.6
IC97-49	27.73	29.26	1.53	0.42	0.013		1.2	ID97-20	139.9	141.13	1.23	0.08	0.006		0.4
IC97-50	13.37	14.93	1.56	0.45	0.004		0	ID97-22	130.87	132.02	1.15	0.06	0.005	0	0
IC97-50	14.93	15.85	0.92	0.99	0.004		0	ID97-22	132.02	133.5	1.48	1.12	0.076	0.38	3.6
IC97-50	15.85	16.72	0.87	0.34	0.007		0	ID97-22	133.5	134.77	1.27	0.97	0.055	0.42	4.8
IC97-51	3.35	5.18	1.83	0.35	0.004		0	ID97-26	86.67	88.33	1.66	0.01	0.003		0
IC97-51	5.18	6.25	1.07	0.35	0.005		0	ID97-26	88.33	88.58	0.25	0.04	0.002	0.09	0
IC97-51	7.16	8.67	1.51	0.56	0.012		0	ID97-26	90.19	91.7	1.51	3.91	0.101	0.68	10
IC97-51	8.67	9.82	1.15	0.35	0.004		0	ID97-26	91.7	92.96	1.26	0.02	0.003		0
IC97-51	9.82	11.3	1.48	0.53	0.005		0	ID97-26	92.96	94.18	1.22	0.02	0.003		0
IC97-51	11.3	12.65	1.35	0.45	0.004		0	ID97-26	94.18	95.55	1.37	0.01	0.003		0
IC97-51	12.65	13.11	0.46	0.39	0.008		0	ID97-28	93.42	94.66	1.24	0.38	0.003		0.8
IC97-51	14.02	14.94	0.92	0.3	0.009		0	ID97-28	100.6	101.46	0.86	0.17	0.003		0.2
IC97-51	15.85	17.07	1.22	0.4	0.010		0	ID97-28	102.76	104.01	1.25	0.76	0.004	0.015	1.6
IC97-51	17.07	18.07	1	0.31	0.007		0	ID97-28	104.01	104.85	0.84	2.10	0.006	0.04	5.6
IC97-52	3.66	5.18	1.52	0.39	0.003		0	ID97-28	115.82	117.3	1.48	0.01	0.023		0.6
IC97-52	5.18	6.71	1.53	0.41	0.004		0	ID97-28	117.3	118.87	1.57	0.00	0.021		0
IC97-52	6.71	7.77	1.06	0.37	0.004		0	ID97-28	118.87	120.09	1.22	0.05	0.012		0
IC97-52	7.77	9.3	1.53	0.6	0.007		0	ID97-28	120.09	120.7	0.61	0.01	0.017		0.2

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC97-52	9.3	10.52	1.22	0.333	0.003		0	ID97-28	120.7	122	1.3	0.00	0.014		0
IC97-52	10.52	12.04	1.52	0.3	0.003		0	ID97-28	122	123.14	1.14	0.02	0.018		0.2
IC97-52	12.04	13.41	1.37	0.45	0.005		0	ID97-28	123.14	124.36	1.22	0.01	0.017		0.2
IC97-52	13.41	14.94	1.53	0.34	0.004		0	ID97-28	124.36	125.27	0.91	0.02	0.040		0.4
IC97-52	14.94	16.15	1.21	0.58	0.003		0	ID97-28	125.27	126.24	0.97	0.04	0.023		0.4
IC97-52	16.15	17.68	1.53	0.61	0.005		0	ID97-28	126.24	127.4	1.16	0.05	0.034		1.6
IC97-52	17.68	18.29	0.61	0.68	0.005		0	ID97-28	127.4	128.47	1.07	0.26	0.006	0.11	1.4
IC97-52	18.29	19.81	1.52	0.75	0.005		0	ID97-28	128.47	129.24	0.77	0.99	0.046	0.04	2.8
IC97-52	19.81	21.2	1.39	1.27	0.009		0.8	ID97-28	129.24	130.26	1.02	2.16	0.078	0.08	7.6
IC97-52	21.2	22.65	1.45	0.97	0.004		0	ID97-28	130.26	131.15	0.89	2.27	0.088	0.065	7
IC97-52	22.65	23.7	1.05	0.84	0.005		0	ID97-28	131.15	132.28	1.13	0.56	0.025	0.025	1.4
IC97-53	2.44	3.66	1.22	0.41	0.002		1	ID97-30	28.65	29.3	0.65	0.07	0.013		0
IC97-53	5.64	7.62	1.98	0.39	0.006		0	ID97-30	29.9	30.66	0.76	4.81	0.052	0.26	13
IC97-53	10.5	12.05	1.55	0.49	0.005		0	ID97-30	33.22	34.75	1.53	3.25	0.102	0.405	7
IC97-53	15.39	17.2	1.81	0.3	0.003		0	ID97-30	37.8	38.94	1.14	1.58	0.058	0.325	5
IC97-53	17.2	19.2	2	0.35	0.004		0	ID97-30	38.94	39.65	0.71	3.16	0.081	0.475	8
IC97-53	19.2	21.03	1.83	1.74	0.005		0.2	ID97-30	39.65	41.72	2.07	1.56	0.021	0.08	1.2
IC97-53	21.03	23	1.97	1.43	0.005		0	ID97-30	41.72	42.92	1.2	0.19	0.014	0.05	0.6
IC97-55	3.65	4.57	0.92	0.44	0.008		0	ID97-31	66.14	67.36	1.22	0.01	0.003		0
IC97-55	4.57	7.03	2.46	1.83	0.007		0	ID97-31	67.36	68.88	1.52	0.01	0.003		0
IC97-55	7.03	8.07	1.04	2.36	0.006		0	ID97-31	68.88	70.41	1.53	0.02	0.003		0
IC97-55	8.07	8.83	0.76	3.49	0.010		0	ID97-31	70.41	71.93	1.52	0.03	0.003		0
IC97-55	8.83	10.05	1.22	0.53	0.014		0	ID97-31	71.93	73.46	1.53	0.04	0.003		0.2
IC97-55	10.05	11.27	1.22	0.73	0.020		0	ID97-31	73.46	74.98	1.52	0.01	0.003		0
IC97-55	11.27	12.03	0.76	0.8	0.018		0	ID97-31	74.98	76.5	1.52	0.01	0.003		0
IC97-55	12.03	13.71	1.68	0.53	0.009		0	ID97-31	76.5	78.03	1.53	0.01	0.003		0
IC97-55	13.71	14.78	1.07	0.59	0.007		0	ID97-31	78.03	79.25	1.22	0.01	0.003		0
IC97-55	14.78	16.3	1.52	0.44	0.008		0	ID97-31	79.25	80.16	0.91	0.01	0.003		0
IC97-55	16.3	17.25	0.95	0.5	0.035		0	ID97-31	80.16	81.28	1.12	0.01	0.003		0
IC97-55	20.42	21.37	0.95	1.95	0.017		0	ID97-31	85.07	86.05	0.98	0.12	0.003		0.8
IC97-55	21.37	22.24	0.87	0.46	0.030		0	ID97-31	86.05	87.17	1.12	0.01	0.003		0.6
IC97-55	22.24	23.46	1.22	0.59	0.020		1.6	ID97-31	87.17	88.85	1.68	0.02	0.004		4.4
IC97-55	23.46	23.98	0.52	0.47	0.007		0.4	ID97-31	88.85	90.37	1.52	0.01	0.003		0
IC97-56	5.79	7.76	1.97	0.31	0.004		0.6	ID97-34	133.33	134.76	1.43	0.18	0.007		0.6
IC97-56	17.98	19.51	1.53	0.37	0.002		1.4	ID97-34	142.18	143.26	1.08	0.04	0.010		0
IC97-56	21.03	22.45	1.42	0.48	0.004		0	ID97-34	144.58	145.39	0.81	0.07	0.009		0.4
IC97-56	22.45	24.08	1.63	0.32	0.004		0	ID97-34	145.39	146.61	1.22	0.01	0.010		0
IC97-56	24.08	25.6	1.52	0.36	0.003		0	ID97-34	146.61	147.68	1.07	0.01	0.009		0
IC97-56	25.6	27.13	1.53	0.34	0.003		0	ID97-34	147.68	149.05	1.37	0.08	0.011		0
IC97-56	27.13	28.65	1.52	0.31	0.003		0	ID97-34	149.05	149.96	0.91	0.02	0.010		0
IC97-56	28.65	30.15	1.5	0.38	0.003		0	ID97-34	149.96	150.78	0.82	0.12	0.009		0.2
IC97-56	34.9	36.5	1.6	0.68	0.016		0.4	ID97-34	153.3	154.23	0.93	0.01	0.003		0
IC97-56	36.5	38.45	1.95	2.81	0.013		0.2	ID97-35	2.44	3.66	1.22	0.01	0.003		0
IC97-56	38.45	40.39	1.94	0.92	0.010		0	ID97-35	3.66	4.88	1.22	0.01	0.003		0
IC97-56	49.99	51.51	1.52	0.67	0.014		0	ID97-36	76.66	78.33	1.67	0.01	0.003		0
IC97-56	51.51	53.04	1.53	0.56	0.009		0	ID97-36	78.33	79.55	1.22	0.01	0.004		0
IC97-56	53.04	54.56	1.52	0.53	0.007		0	ID97-36	79.55	80.4	0.85	0.33	0.007		0.4
IC97-56	54.56	56.08	1.52	0.42	0.008		0	ID97-36	80.4	81.22	0.82	7.24	0.165	0.42	11.4
IC97-56	56.08	57.4	1.32	0.63	0.008		0	ID97-36	81.22	82.32	1.1	8.32	0.131	0.94	26.8

DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t	DDH	From	To	Interval	Cu%	Co%	Au g/t	Ag g/t
IC97-56	57.4	58.67	1.27	0.5	0.009		0	ID97-36	82.32	83.4	1.08	9.92	0.069	0.715	27
IC97-56	58.67	60.2	1.53	1.03	0.011		0	ID97-36	83.4	84.43	1.03	4.43	0.061	0.795	22.4
IC97-56	61.57	62.8	1.23	1.08	0.008		0	ID97-36	85.95	87.48	1.53	3.93	0.082	0.735	15.4
IC97-56	62.8	64.31	1.51	1.76	0.010		0	ID97-36	87.48	89	1.52	2.68	0.035	0.755	13.2
IC97-56	64.31	65.23	0.92	0.92	0.010		0	ID97-36	89	90.53	1.53	4.05	0.047	0.65	10
IC97-56	65.23	66.75	1.52	0.85	0.011		0	ID97-36	90.53	91.59	1.06	3.54	0.061	0.43	7.2
IC97-56	66.75	68.3	1.55	1.43	0.011		0	ID97-36	91.59	93.12	1.53	4.23	0.057	0.675	13.2
IC97-56	68.3	69.8	1.5	1.27	0.011		0	ID97-36	93.12	94.64	1.52	3.44	0.032	0.57	8.6
IC97-56	69.8	71.3	1.5	0.31	0.008		0	ID97-36	94.64	96.16	1.52	3.01	0.041	0.7	6.6
IC97-56	71.3	72.85	1.55	0.41	0.007		0	ID97-36	96.16	97.84	1.68	4.12	0.059	0.795	17.2
IC97-56	74.37	75.74	1.37	0.31	0.009		0	ID97-36	99.3	100.89	1.59	0.02	0.002		0
IC97-56	75.74	77.11	1.37	0.7	0.014		0	ID97-36	100.89	102.41	1.52	0.01	0.003		0
IC97-57	9.75	11.12	1.37	0.418	0.002		1.6	ID97-36	102.41	104.09	1.68	0.01	0.003		0
IC97-57	13.25	14.8	1.55	2.96	0.021		6	ID97-36	107	108.51	1.51	1.41	0.047		4.8
IC97-57	14.8	16.5	1.7	4.24	0.019		3	ID97-36	108.51	110.33	1.82	0.88	0.043		3.4
IC97-57	16.5	18.29	1.79	3.72	0.021		4	ID97-36	110.33	112.15	1.82	0.76	0.021		2.6
IC97-57	18.29	19.81	1.52	5.78	0.028		6	ID97-36	112.15	113.08	0.93	0.36	0.018		2
IC97-57	19.81	20.8	0.99	11.6	0.058		9	ID97-36	113.08	114.6	1.52	0.01	0.015		0.2
IC97-57	20.8	22.1	1.3	3.78	0.017		0	ID97-36	114.6	116.13	1.53	0.15	0.018		1
IC97-57	22.1	22.9	0.8	3.97	0.022		0	ID97-36	116.13	117.65	1.52	0.01	0.009		0.6
IC97-57	22.9	24.84	1.94	2.32	0.014		0	ID97-36	117.65	119.18	1.53	0.01	0.012		0.6
IC97-57	24.84	26.35	1.51	2.87	0.015		0	ID97-36	119.18	120.7	1.52	0.01	0.008		0
IC97-57	26.35	28.25	1.9	4.26	0.061		3	ID97-36	120.7	122.22	1.52	0.02	0.008		0.2
IC97-57	28.25	29.35	1.1	4.09	0.059		7	ID97-36	122.22	124.21	1.99	0.02	0.010		0
IC97-57	29.35	30.48	1.13	4.37	0.043		7	ID97-36	124.21	125.57	1.36	0.01	0.007		0
IC97-57	30.48	31.7	1.22	2.26	0.013		1	ID97-36	125.57	127.1	1.53	0.01	0.006		0
IC97-57	31.7	32.92	1.22	3.57	0.025		3	ID97-36	127.1	128.63	1.53	0.01	0.008		0
IC97-57	32.92	34.14	1.22	2.87	0.022		1	ID97-36	128.63	130.15	1.52	0.01	0.007		0
IC97-57	34.14	35.66	1.52	1.3	0.032		1	ID97-36	130.15	131.67	1.52	0.01	0.007		0.2
IC97-57	35.66	37.19	1.53	1	0.026		0	ID97-36	131.67	133.2	1.53	0.02	0.010		0.6
IC97-57	37.19	38.7	1.51	1.05	0.033		1	ID97-36	133.2	134.72	1.52	0.01	0.006		0
IC97-57	38.7	40.5	1.8	1.07	0.016		0	ID97-36	134.72	135.95	1.23	0.40	0.006		0.4
IC97-57	40.5	41.76	1.26	0.39	0.021		0								
IC97-58	2	3.45	1.45	0.4	0.007		2								
IC97-58	13.11	14.63	1.52	0.33	0.003		0.8								

APPENDIX 5 - JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• HQ diamond drill core was drilled in 121 holes, with holes reduced to NQ deeper in the holes. Triple tube drilling was used to improve the drilling recovery. • Drill core was historically split using a core pressure splitter on site, for assaying by Chemex Laboratories. Re-sampled core was cut and quarter core submitted for assay, with the remaining quarter maintained for future reference. • Assays were typically 1.5 m assays, though thicknesses vary between approximately 1 and 2 m long, depending on mineralisation and core recovery.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Holes were all diamond drill holes with HQ core diameter, reducing to NQ diameter, depending on the hole depth. • It is unknown whether triple tubes were used in the drilling. Core was generally highly competent.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Drill cores were recovered to surface and placed in wooden core boxes, stored in core racks and on pallets. Core trays were labelled with aluminium tags, allowing identification of holes and core intervals. Sampled intervals were marked with flagging tape. • Core recovery was noted and is generally high, due to the compact nature of the basalt host rock. Samples were sent for analysis to the Chemex laboratory in Vancouver (now part of ALS laboratories).

Criteria	**JORC Code explanation**	**Commentary**
Logging	● *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* ● *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* ● *The total length and percentage of the relevant intersections logged.*	● A soil sampling grid was carried out across the ICE project area, with samples spaced every 25 m NW to SE, collected on lines with a general spacing of 50 m in the central deposit area, with samples on contour lines outside this area taken approximately every 50 m. ● The details of the soil sampling were not documented in available reports. However, they are believed to be conventional sieved soil samples, most likely taken at a depth of 20 to 30 cm, consistent with prevailing industry practice at the time. ● Longhand descriptive logs of drill holes were prepared during the drilling process and units and mineralisation summarised into codes and relative abundances as part of the geological logging. This information was collated in excel spreadsheets and a database. ● Logging was both qualitative and quantitative. No core photographs are available. ● 10,584 m of core were drilled historically.
Sub-sampling techniques and sample preparation	● *If core, whether cut or sawn and whether quarter, half or all core taken.* ● *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* ● *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* ● *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* ● *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* ● *Whether sample sizes are appropriate to the grain size of the material being sampled.*	● Core was sub-sampled for assay. Core was split using a core splitter. ● Details of the sample preparation are not certain, due to the historical nature of the activities. ● Drill hole orientations appear to have intersected mineralisation at a high angle, resulting in thicknesses that are close to true thicknesses of mineralisation. ● Quality control procedures are unknown, regarding the use of duplicate and standard or blank samples. There is no recorded QA/QC procedure. ● Given that the descriptions of core recovery generally appear to be acceptable (high recovery) it is likely that sufficient sample was submitted for analysis to produce repeatable results. ● Sample sizes were appropriate for the mineralisation style.
Quality of assay data and laboratory tests	● *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* ● *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* ● *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	● ICE Samples were crushed, pulverised to -50 mesh using a chrome steel ring mill and then digested with nitric-aqua regia, before being analysed for 32 elements using ICP equipment. This provided total digestion for Cu, Ag and Zn, but only partial digestion for some 14 of the elements analysed. Most of the primary massive sulphide samples were fire assayed for gold and results were reported in ppb from a 30 gram sample. ● Petrology was carried out by Vancouver Petrographics, who verified the mineral modes and textures on four core samples. Whole rock analyses were conducted on selected analyses.

Criteria	JORC Code explanation	Commentary
		- The assay results are considered appropriate, given the available information. However, given their historical nature not all the details of sampling and assaying are available. - Given the historical nature of the analyses it is likely that there were no QA/QC samples included with the primary samples.
Verification of sampling and assaying	- *The verification of significant intersections by either independent or alternative company personnel.* - *The use of twinned holes.* - *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* - *Discuss any adjustment to assay data.*	- The original ICE resource estimate and supporting information was reviewed by Mr Thompson of independent consultants Derry, Michener, Booth & Wahl (1998) following the resource estimate. - Bastion has conducted a check estimate with the assay results and an Inverse Distance Squared methodology to check that the resource is comparable to the documented historical and foreign non-JORC resource.
Location of data points	- *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* - *Specification of the grid system used.* - *Quality and adequacy of topographic control.*	- Drill collars were located on the local grid and were located with chain measurements. The location of the holes was surveyed with a Nikon DTM-A20 total station. They were subsequently converted to the UTM9N NAD27 coordinate system. - The project historically used a local grid, with a NE trending baseline and NW trending grid lines for drilling and geophysics. - Field validation of drill holes using GPS in UTM with the NAD83 datum located holes within 5 m of the location shown in historical maps converted to the NAD83 datum. This is within the GPS measurement error. - Topographic contours are available for the project, based on original surveying.
Data spacing and distribution	- *Data spacing for reporting of Exploration Results.* - *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* - *Whether sample compositing has been applied.*	- Soil sampling and the drilling data spacing is appropriate for the style of mineral deposit explored and to confirm geological and grade continuity.
Orientation of data in relation to geological structure	- *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* - *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	- The orientation is considered to be appropriate for the ICE deposit, with drilling intended to drill perpendicular to the deposit orientation, with the results showing this is generally the case.

Criteria	JORC Code explanation	Commentary
Sample security	- *The measures taken to ensure sample security.*	- It is unknown the details of how samples were sent to the assay laboratories on the project.
Audits or reviews	- *The results of any audits or reviews of sampling techniques and data.*	- A review and audit of the ICE project data and resource estimate was undertaken by an independent consultant Thompson (1998), upon completion of the original resource estimate. Bastion has conducted a check estimate, based on the available assay data and geology, which validates the contained metal of the original estimate.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	- *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* - *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	- The ICE project consists of 260 hard rock quartz claims covering an area of ~5,330 ha - The properties were originally staked in 1993 by Yukon Zinc Corporation, the 100% property owner. - The project is within an area of First Nations land rights.
Exploration done by other parties	- *Acknowledgment and appraisal of exploration by other parties.*	- Previous work at ICE was conducted by Yukon Zinc Corporation from soil samples, mapping, geophysics, drilling and resource estimation, before the owner concentrated on their priority of developing and operating the Wolverine zinc project.
Geology	- *Deposit type, geological setting and style of mineralisation.*	- The ICE project is a Cyprus-style volcanic massive sulphide (VHMS) deposit.
Drill hole Information	- *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* - *If the exclusion of this information is justified on the basis that the*	- Drillhole coordinates are provided in Table 3 of this report. Coordinates are in UTM9N, with the NAD27 data, converted from the local grid. The currently used datum in this part of Canada is the NAD83 datum. - Holes were surveyed downhole with a Pajari borehole instrument and were noted to have only minor deviation, with almost all holes < 200 m deep. - Elevations are shown in Table 3. - Holes are predominantly drilled at -50 degrees to 300 degrees, although some holes are drilled vertically and several are drilled towards the SE.

Criteria	JORC Code explanation	Commentary
	information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	• The deepest hole is 271 m and the average depth is 88.6 m.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• In the ICE project historical estimate drill assays were not cut or capped. • The details of the original resource estimate were documented in reasonable detail. Mineralised intersections in the individual resource cells were weighted based on copper grade and length of intersection. A maximum of 3 m of internal waste was included in the resource intervals. • The original resource estimate was calculated for copper only.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• Drill holes at ICE were oriented to cut the mineralised zone as close to perpendicular as possible. • The mineralisation dips in a consistent direction and was drilled accordingly. • Mineralised intersects represent close to true thickness, given the drilling orientation relative to the mineralisation.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Maps and tables are shown in the body of report
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Assay results from drilling samples, are provided (Tables 4). • Graphics are provided in the announcement showing relevant information. • In the opinion of the CP the Information provided gives a balanced view of the project and the potential.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Airborne magnetic geological survey data was obtained over the ICE project, as was helicopter EM. • The magnetic and EM survey data was acquired in 1997 by DIGHEM of Ontario, Canada. The survey covered 1320 line kilometres. • Magnetics used a Scintrex MP-3 proton precession and Scintrex MEP-710 caesium vapour magnetometers. • The EM system used was a frequency domain system, with maps produced for 900 and 7200 Hz coplanar data.

Criteria	JORC Code explanation	Commentary
		- The survey lines were flown with an approximate 200 m spacing. - QA/QC was conducted by an independent geophysicist, who subsequently conducted a full review of the data. - The ground geophysical survey (HLEM survey) was done on three frequencies with 100 m coil separation which theoretically could detect conductors up to 50 m below surface. The lower frequencies outlined two weak to moderate conductors, the strongest of which started at local grid Line 10950N, through the area of surface mineralization continuing north to grid Line 1 1800N. The core of this conductor is directly above the massive sulphide mineralization in Holes IC 96-02 and -13 (Table 4). - Specific gravity data was collected on 273 samples from ICE by Chemex laboratories in Vancouver.
Further work	- *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* - *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	- Full compilation of available data has been undertaken, including magnetic and Electromagnetic data, geological mapping, soil sampling and drilling information.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.) The resource discussed is historical, foreign and non JORC Code

Criteria	JORC Code explanation	Commentary
Database integrity	- *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* - *Data validation procedures used.*	- Data for the ICE project was imported and compiled from Excel spreadsheets available for individual holes. Data is stored on a BMO computer and backed-up regularly to a network drive. - Data was plotted to check the spatial location and relationship to drill hole locations on historical maps, with locations coinciding with drill pad locations when overlaid. - Basic checks were performed by HSC prior to this resource estimate to ensure data consistency, including checks for FROM_TO interval errors, missing or duplicate collar surveys, excessive down hole deviation, and extreme or unusual assay values. - All data errors/issues were reported to the BMO Database

Criteria	JORC Code explanation	Commentary
		Administrator to be corrected or flagged in the primary database.
Site visits	● *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* ● *If no site visits have been undertaken indicate why this is the case.*	● The JORC Competent Person has now visited the ICE project, and confirmed the presence of all the original drill core and checked the location of a selection of IC96, IC97 and ID97 drill hole locations on the ground, locating the collars and original tags confirming hole locations. The site winter access road is not currently in sufficient condition to allow access to the project site and access is by helicopter only. ● The Competent Person for the Mineral Resource Estimate has not visited site due to time and cost constraints.
Geological interpretation	● *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* ● *Nature of the data used and of any assumptions made.* ● *The effect, if any, of alternative interpretations on Mineral Resource estimation.* ● *The use of geology in guiding and controlling Mineral Resource estimation.* ● *The factors affecting continuity both of grade and geology.*	● The project is a Cyprus-style volcanic massive sulphide (VHMS) deposit, a well-known deposit type in a belt know for hosting for VHMS style mineralisation. ● BMO personnel have developed a geological interpretation of the ICE deposit based on geological logging, chemical assays and historical information. BMO personnel have a reasonable understanding of the geology of the ICE deposit, and this is reflected in the wireframe models they prepared, which formed a guiding framework for Mineral Resource estimation. ● The BMO interpretation included splits in the main mineralised lens and a fault offset across the Baseline Fault. ● HSC modified this by defining a single unsplit main mineralised lens at the top of the porphyritic basalt and the remaining mineralisation was included in a feeder zone in the lower brecciated basalt unit. The Baseline Fault was ignored because no offset was obvious during interpretation. The main mineralised lens was modified to include immediately adjacent mineralisation above a nominal 0.1% copper equivalent grade threshold and generally excluding material below this threshold. Sometimes lower grade material was included to maintain reasonable local continuity and unit thickness. ● Surfaces for the base of oxidation and top of fresh rock were also interpreted, based on original available geological logging, which recorded different mineral species, but not oxidation directly in the hole logs. It was not entirely clear what the oxidation codes represent because the oxide material is not necessarily depleted in copper, there are no sulphur assays to confirm the logging codes and iron assays are not particularly useful here. ● There is some scope for alternative geological interpretations of the deposit, principally in the correlation of intersections that comprise the

Criteria	JORC Code explanation	Commentary
		main mineralised lens. An alternative interpretation of the geology, and hence mineral resource, would have a limited impact on the final estimate number, as interpretation is fairly tightly constrained by the geology. ● Geology guides and controls Mineral Resource estimation by using stratigraphy and the local orientation of the main mineralised lens to guide the overall orientation of mineralisation. ● The continuity of geology and grade at ICE is controlled primarily by stratigraphy, with mineralisation having less continuity than geology.
Dimensions	● *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource*	● The Mineral Resource Estimate for the ICE deposit at a 0.3% Cu cut-off grade has an approximate extent of: ○ 560m east-west (plan width), ○ 480m north-south (~along strike), ○ From surface to 150m below surface. ● The mineralisation thins towards the edges of the ICE deposit. ● Mineralisation outcrops in the northwest corner of the deposit, dipping away to the southeast. ● Elevations are shown in sections and figures in the report.
Estimation and modelling techniques	● *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* ● *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* ● *The assumptions made regarding recovery of by-products.* ● *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).* ● *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* ● *Any assumptions behind modelling of selective mining units.* ● *Any assumptions about correlation between variables.* ● *Description of how the geological interpretation was used to control the Resource estimates.* ● *Discussion of basis for using or not using grade cutting or capping.* ● *The process of validation, the checking process used, the*	● Samples were composited to nominal 1.5m intervals within each unit for data analysis and resource estimation, based on the dominant historical sample length of 5 feet (1.52m). Missing gold values were derived from a regression against silver grades and other samples without assays were assigned low default values for Cu, Ag, Au, etc, except for iron. ● The resource model uses a parent block size of 12.5x12.5x2.5m, while drill hole spacing is nominally 25x50m in the better drilled areas of the deposit. The block size represents ½ to ¼ of the drill hole spacing, which is a little smaller than preferred but was deemed necessary to adequately accommodate the variable orientation of mineralisation. Sub-blocks at half the parent block size in each direction were used at zone boundaries, although estimates were generated at the scale of parent blocks. ● No specific assumptions were made regarding selective mining units (SMUs); therefore the model block size is effectively the SMU. ● The resource model was generated in NAD83 Zone 9 coordinates. ● Ordinary kriging (OK) was chosen as the appropriate estimation method for metal grades at the ICE deposit because grade distributions

Criteria	JORC Code explanation	Commentary
	comparison of model data to drill hole data, and use of reconciliation data if available.	are not particularly skewed, show reasonable continuity as defined by variography and do not contain extreme erratic values. ● OK estimates were generated using Datamine Studio RM version 2.1.125.0 software. ● The deposit was divided into four zones (Main Mineralisation, Feeder Zone, Footwall and Hanging wall) which were each estimated separately. Dynamic estimation was implemented, based on the orientation of the mid-plane of the Main Mineralisation, in order to deal with the variable orientation of mineralisation. ● A three pass search strategy was used for the OK grade estimates: ● 25x25x12.5m search, 12-32 samples, minimum of 4 octants, ● 50x50x25m search, 8-32 samples, minimum of 4 octants, ● 100x100x50m search, 8-32 samples, minimum of 4 octants. ● An additional larger pass was used for iron because low defaults for unassayed intervals were deemed inappropriate. ● The oxide and transition zones were estimated together with fresh rock because there was no obvious evidence of depletion or enrichment due to oxidation. ● The maximum extrapolation distance will be somewhat less than the maximum search radius due to the octant constraints requiring at least 2 drill holes. Maximum extrapolation distance is around 80m. ● It is assumed that a Cu-Au sulphide concentrate will be produced, with Co, Ag and Zn as possible by-products. All elements have been estimated independently for each domain, including Cu, Au, Ag, Co, Zn, Pb and Fe. No potentially deleterious elements were estimated; there are no sulphur assays but there are assays for other potentially deleterious elements such as As, Bi and Sb. ● No assumptions were made regarding the correlation of variables during estimation because each element was estimated independently. Some elements do show moderate to strong correlation in the drill hole samples, and the similarity in variogram models effectively guarantees that this correlation will be preserved in the estimates.

Criteria	JORC Code explanation	Commentary
		● The limited density data was used to calibrate a density formula based on assays, which implemented a normative approach to calculate sulphide species. Actual measurements were used where available and calculated otherwise. Dry bulk density was then estimated directly into the model from the drill hole samples, using a similar methodology to the metals. ● Metal grades were estimated using density weighting because density varies substantially between massive sulphides and disseminated mineralisation. ● The geological interpretation controls the Mineral Resource estimates through the use of stratigraphic and/or mineralisation boundaries. ● No grade cutting was applied to any of the metal estimates because metal grades at the ICE deposit do not have grade distributions that are particularly skewed, show reasonable continuity as defined by variography and do not contain extreme erratic values. ● The new model was validated in a number of ways – visual comparison of block and drill hole grades, statistical analysis, examination of grade-tonnage data, and comparison with a nearest neighbour check model and previous estimates. All the validation checks indicate that the grade estimates are reasonable when compared to the composite grades, allowing for data clustering. ● The new Mineral Resource Estimate represents similar copper metal content, with higher tonnage and lower grade than the 1998 polygonal resource. This is not an unexpected result for a comparison between a polygonal and OK estimate, because the former is essentially undiluted and unsmoothed. A 2025 nearest neighbour check estimate is almost identical globally to the 1998 resource. The 2025 OK model is considered to be a more reasonable representation of the mineable resource than the 1998 estimate. ● The deposit remains unmined so there is no reconciliation data.
Moisture	● *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	● Tonnages are estimated on a dry weight basis and moisture content has not been determined.
Cut-off parameters	● *The basis of the adopted cut-off grade(s) or quality parameters applied.*	● The cut-off grade of 0.3% Cu is considered likely to be economic for the mining method and scale of operation envisioned for ICE, based on comparison with similar deposits elsewhere. This parameter will be

Criteria	JORC Code explanation	Commentary
		evaluated further in the future, provided that sufficient resources are found that contribute to a mineable tonnage of mineralisation.
Mining factors or assumptions	- *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	- The deposit is considered to be primarily amendable to open pit mining, with the potential for underground exploitation of deeper mineralisation. Consideration of current economics would be required to assess the basis of extraction with recent commodity prices. - The OK estimation method implicitly incorporates internal mining dilution at the scale of the model block size. No specific assumptions were made about external mining dilution or mining losses in the Mineral Resource Estimate. - The maximum slope for the historical 1998 conceptual pit design was 50 degrees on the eastern side and 45 degrees on the other three sides. - The maximum stripping ratio for the historical pit outline was considered to be 10:1 for the massive sulphide mineralisation.
Metallurgical factors or assumptions	- *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	- No significant historical metallurgy has been conducted on the deposit, which consists primarily of chalcopyrite, with pyrite and minor bornite locally. There is gold associated with the massive sulphides, minor cobalt and silver and traces of zinc. - Metallurgical review is currently underway. Additional test work to determine metal recoveries and the potential recovery of by-products is planned.
Environmental factors or assumptions	- *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	- It is currently assumed that all process residue and waste rock disposal will take place on site in purpose built and appropriately licensed facilities. - All waste rock and process residue disposal will be done in a responsible manner and in accordance with any mining license conditions. - With pyrite in the upper part of the deposit there is some acid generating potential, which can be mitigated by disposal of tailings below the water level.
Bulk density	- *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* - *The bulk density for bulk material must have been measured by*	- Historically, 276 measurements of specific gravity were made on assay sample pulps from 21 holes during the original 1996-97 drilling programs on a variety of rock types. This indicates that specific gravity was measured using a pycnometer method, which does not

Criteria	JORC Code explanation	Commentary
	methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. - *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	adequately account for void spaces. - In 2024, 48 measurements were collected on quarter core samples of historical core by Aurora Geoscience using the water displacement method. Cores were not coated in wax, as they are generally quite solid and competent. - An additional 38 measurements were made by ALS on pulps from cores that were selected from the re-assaying program. These corresponded to the majority of the samples conducted by Aurora. - Comparison of the Aurora and ALS measurements showed that sample porosity is not an issue for fresh rock. However, analysis of historical measurements on oxidised and transitional samples showed these to be unreliable and biased high. - HSC derived alternative density values calculated from metal assays, implemented using a normative approach to calculate sulphide species, which matched the measured values reasonably well. Density was then calculated for all drill hole intervals using this process, and a preferred density value was selected, with actual measurements used where available and calculated values otherwise. Samples were then flagged and composited in the same way as the grade data, followed by variography. - Dry bulk density was estimated directly into the model from the preferred composite data using the same estimation scheme as the metal grades. To account for oxidation, HSC applied nominal factors of 2.5/2.8 for oxide and 2.7/2.8 for transitional material to the estimated density values. Detailed measurements should be made on future drill core.
Classification	- *The basis for the classification of the Mineral Resources into varying confidence categories.* - *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* - *Whether the result appropriately reflects the Competent Person's view of the deposit*	- Resource classification was based on estimation search pass, which was subsequently smoothed to minimise the "spotted dog" effect. - The majority of resources could be classified as Indicated, in line with the 1998 estimates, with around 10% of tonnage as Inferred occurring around the edges of the resource or in areas with wider spaced drilling, as might be expected. - This scheme is considered to take appropriate account of all relevant factors, including the relative confidence in tonnage and grade estimates, confidence in the continuity of geology and metal values,

Criteria	JORC Code explanation	Commentary
		and the quality, quantity and distribution of the data. - The classification appropriately reflects the Competent Persons' view of the deposit.
Audits or reviews	- *The results of any audits or reviews of Mineral Resource estimates*	- Bastion had conducted a check estimate of the deposit, using the available survey, geological, assay and bulk density data, resulting in a similar estimate to the 1998 foreign non JORC resource. - The new Mineral Resource Estimate has been reviewed by BMO and HSC personnel and no material issues were identified.
Discussion of relative accuracy/ confidence	- *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the Resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* - *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* - *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	- The relative accuracy and confidence level in the Mineral Resource estimates are considered to be in line with the generally accepted accuracy and confidence of the nominated JORC Mineral Resource categories. This has been determined on a qualitative, rather than quantitative, basis, and is based on the estimator's experience with a number of similar deposits elsewhere. The main factors that affect the relative accuracy and confidence of the Mineral Resource estimate are drill hole spacing and the interpretation of stratigraphy, because there are reasonably strong geological controls on the primary mineralisation. - The estimates are local, in the sense that they are localised to model blocks of a size considered appropriate for local grade estimation. The tonnages relevant to technical and economic analysis are those classified as Indicated Mineral Resources. - No production data is available because this deposit has not been previously mined.