DIATREME Resources

ASX ANNOUNCEMENT

19 May 2026

Significant 10.6% Mineral Resource Estimate upgrade at Si2 further underpinning development of the Northern Silica Project

- **Updated Si2 Mineral Resource Estimate increased from 272.5Mt to 301.5Mt materially expands the resource base and indicates mineralisation continues extending further to the South-East.**
- **62% of the Si2 MRE categorised as Measured.**
- **Results indicate a high-purity silica sand deposit with favourable mining geometries, supporting a long-life, low-strip operation for Queensland's critical minerals industry and Diatreme shareholders and our local communities.**
- **Updated MRE to form the geological basis for the Pre-Feasibility Study (PFS), which is currently in final drafting stage.**
- **Colour values now incorporated into the underlying grade model in addition to geochemical data, supporting stage-wise predictive processing studies and mine schedule optimisation.**
- **Technical work continues at the Casuarina deposit to support a future Mineral Resource Estimate, to be prepared and reported in accordance with the JORC Code (2012 Edition).**

Emerging silica sands developer Diatreme Resources Limited (ASX:DRX) today announced an updated Mineral Resource Estimate (**MRE**) for its Northern Silica Project Si2 Deposit (**Si2**), part of the Company's broader silica sand portfolio in North Queensland. The update materially expands the Si2 resource base and, importantly, infers mineralisation further toward the south east of the existing principal deposit.

The Si2 Deposit sits within the world-class Cape Bedford - Cape Flattery Dune Field, immediately adjacent to the Port of Cape Flattery, and is well positioned to supply growing global demand for low-iron, high-purity silica, the key component for photovoltaic glass used in solar panels. A key feature of this mineral resource update is the incorporation of colour attributes in addition to geochemical data, captured systematically during drilling and logging, directly into the underlying grade model. These attributes are expected to support stage-wise predictive processing studies and inform mine schedule optimisation and product blending as the project advances. The updated grade model in the MRE will form the geological basis for the Company's Pre-Feasibility Study (PFS), which is currently in final drafting stage. The results of the MRE are provided in Table 1.

Diatreme's CEO, Neil McIntyre, commented: *"This updated Resource is another meaningful step forward for the Northern Silica Project. Not only have we materially expanded the Si2 resource base, but we've also confirmed that mineralisation extends further towards the South-East. Just as importantly, we've laid the groundwork for stage-wise predictive processing studies that we expect will be a real differentiator when it comes to optimising and de-risking the initial mine schedule, which will allow Diatreme to tailor product to exacting customer requirements. This only further strengthens our strategy for the Northern Silica Project to become a multi-generational critical minerals project for Queensland, the communities we operate in and importantly our shareholders "*

RESOURCE CATEGORY	SILICA SAND MT	SIO_2 %	FE_2O_3 %	TIO_2 %	AL_2O_3 %
MEASURED	187.5	99.25	0.10	0.14	0.11
INDICATED	42	99.16	0.12	0.16	0.11
INFERRED	72	99.17	0.13	0.17	0.11
TOTAL	**301.5**	**99.20**	**0.11**	**0.15**	**0.11**

Table 1: May 2026 Si2 Deposit | Breakdown by MRE Category

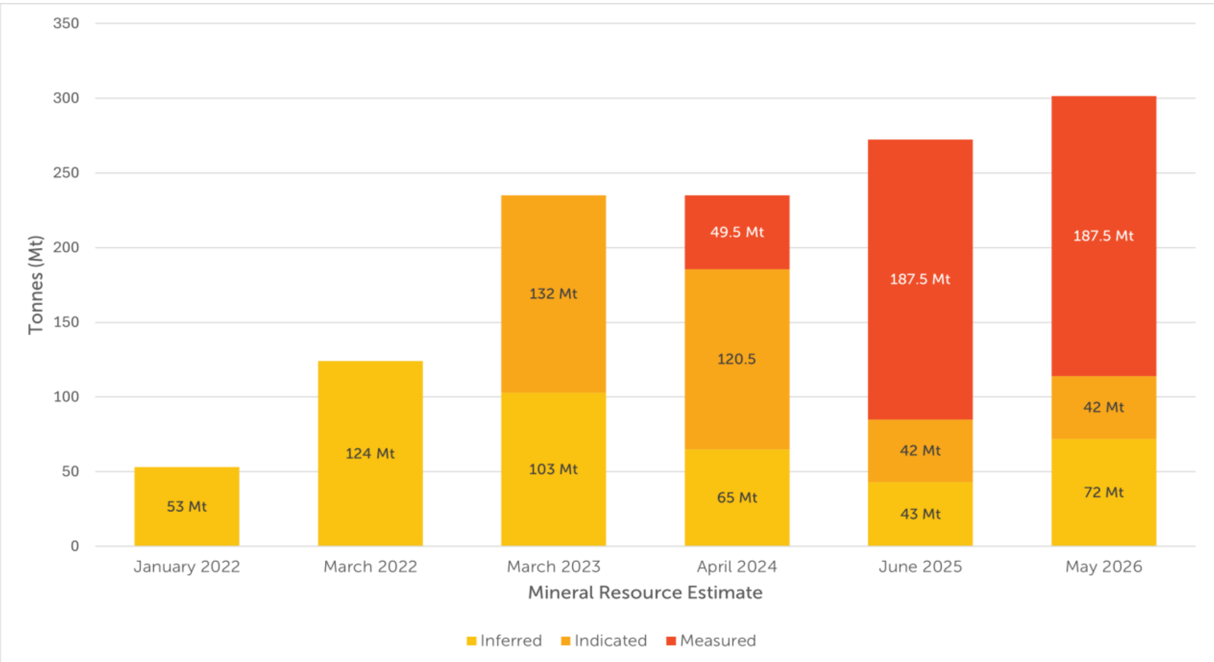
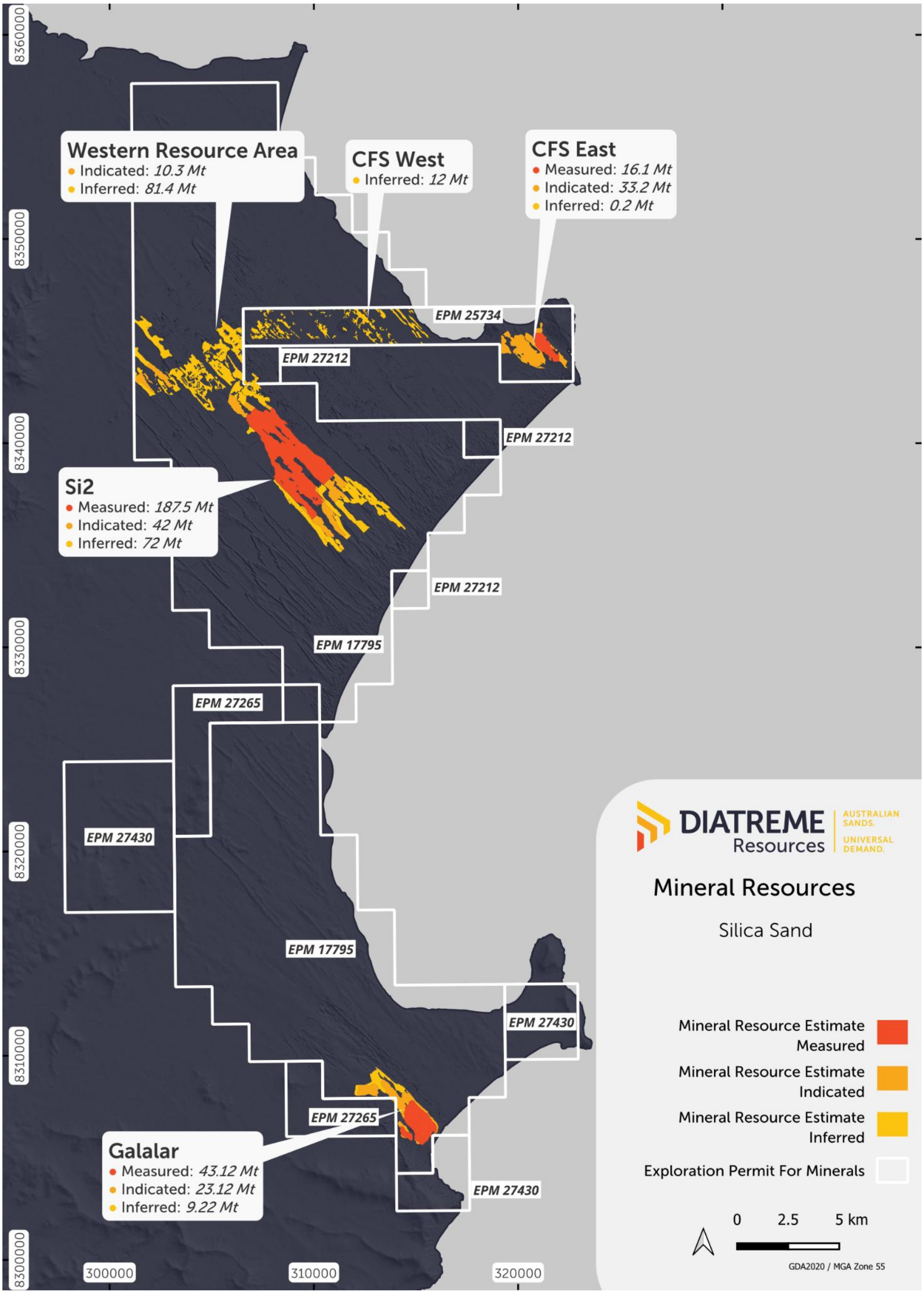


Figure 1: Si2 Mineral Resource growth since discovery in November 2021



Western Resource Area
Indicated: 10.3 Mt
Inferred: 81.4 Mt
CFS West
Inferred: 12 Mt
CFS East
Measured: 16.1 Mt
Indicated: 33.2 Mt
Inferred: 0.2 Mt
Si2
Measured: 187.5 Mt
Indicated: 42 Mt
Inferred: 72 Mt
Galalar
Measured: 43.12 Mt
Indicated: 23.12 Mt
Inferred: 9.22 Mt
EPM 25734
EPM 27212
EPM 17795
EPM 27265
EPM 27430
8360000
8350000
8340000
8330000
8320000
8310000
8300000
300000
310000
320000
DIATREME Resources
AUSTRALIAN SANDS. UNIVERSAL DEMAND.
Mineral Resources
Silica Sand
Mineral Resource Estimate Measured
Mineral Resource Estimate Indicated
Mineral Resource Estimate Inferred
Exploration Permit For Minerals
0 2.5 5 km
GDA2020 / MGA Zone 55

NEXT STEPS

The updated Mineral Resource Estimate materially expands the resource base at Si2 and, importantly, indicates mineralisation extending further towards the South-East, a finding that has positive implications for future exploration. The underlying block model also incorporates colour attributes captured systematically during drilling and logging, which Diatreme expects will prove a valuable input into mine schedule optimisation and product blending strategy.

Building on this, the next phase of work will focus on a program of metallurgical testwork over small-increment variability samples taken across the deposit. The objective is to determine whether colour can be used as a predictor of processability for given stage responses, and, if validated, to apply this relationship in stage-wise predictive processing tests. Outcomes from this program are expected to directly inform mine schedule optimisation, processing flowsheet selection and product consistency planning.

In parallel, the technical assessment supporting the Pre-Feasibility Study (PFS) is continuing across the mining, processing, infrastructure and economic workstreams, with the PFS currently in final drafting stage. The updated Mineral Resource Estimate will be incorporated into the PFS as the underlying geological and grade input, supporting mine design and schedule refinement.

Further metallurgical testwork will also continue to refine final product specifications and confirm suitability for photovoltaic, glassmaking and other high-purity industrial applications. These results will underpin ongoing engagement with prospective customers and support progression toward binding offtake discussions with targeted end-users in the global silica sand market.

Diatreme will also continue technical work at the Casuarina deposit, including drilling, sampling, geological logging and analytical programs designed to build the dataset required to support a future Mineral Resource Estimate. This work will be undertaken in accordance with the Company's standard QA/QC protocols. Any future Mineral Resource Estimate for Casuarina will be prepared and reported in accordance with the JORC Code (2012 Edition), and the Company will provide further updates on the Casuarina program as work progresses.

ASX LISTING RULE 5.8.1 SUMMARY

This executive summary outlines the Mineral Resource Estimate for the Si2 Deposit. It has been prepared in accordance with ASX Listing Rule 5.8.1 and takes effect from the date of issue.

GEOLOGY AND GEOLOGICAL INTERPRETATION

The Si2 Deposit sits within the Cape Bedford–Cape Flattery Dune Field, an extensive aeolian dune system spanning approximately 700 km² along the east coast of Cape York Peninsula. The dune field formed from quartz-rich sandstones of the Gilbert River Formation and Dalrymple Sandstone, with additional input from coastal granites and Hodgkinson Formation metasediments. Weathering and leaching within the Laura Basin aquifer system and through later surface erosion which liberated and concentrated the silica sand now hosted in dune forms.

Silica sand mineralisation is hosted primarily within the trailing arms and apices of elongate parabolic aeolian dunes. Interdunal areas typically lack thick aeolian sand and instead expose B1 horizons, clays, bedrock, or other sediments, with the sediments commonly reworked by successive deflationary events.

Deflation maintains a parabolic geometry and proceeds downward until it reaches a zone, usually groundwater or saturated clays where moisture limits further wind transport of sand grains. A podsol eluviated horizon is observable and is topographically elevated nearer the coast. Dune flanks are steeper on the seaward side and become more subdued inland. Figure 1 illustrates these features in an active elongate parabolic dune.

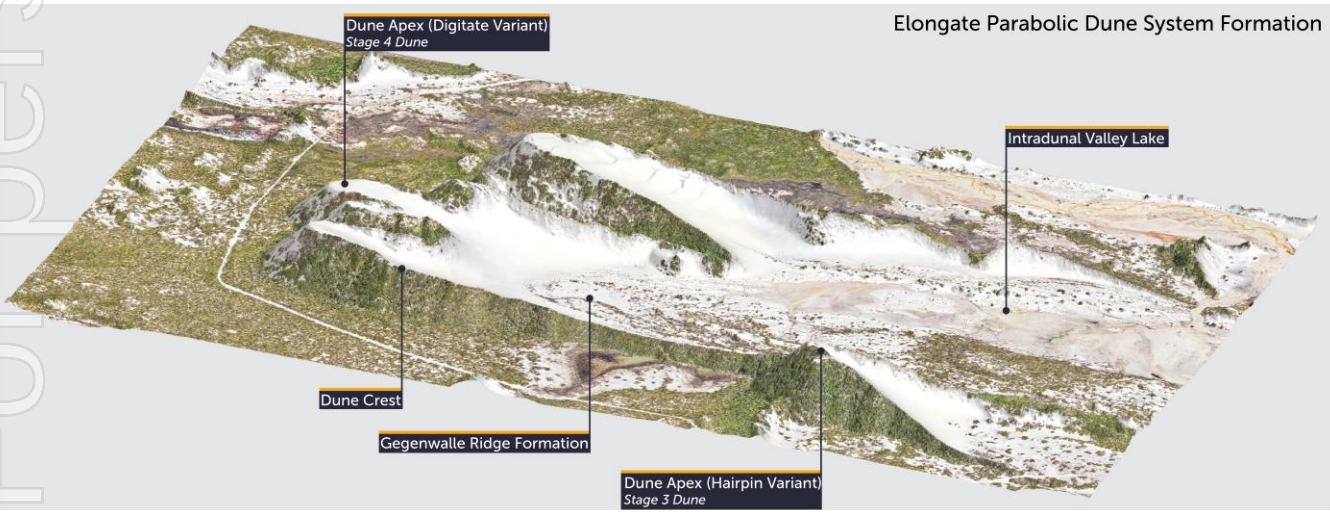


Figure 2: Evolution of active elongate parabolic dune system

SAMPLING PROGRAM	ID SERIES	# HOLES	DRILLING METHOD	COMMENTARY
NOVEMBER 2021 TO JANUARY 2022	PLTxxx	99	Vacuum	Vacuum drill collected 2-3 kg cuttings which reported to a return thick perspex canister mounted on the drill rig (100% of drill material returned by the vacuum drill rig) after passing through a single tiered (50/50) riffle splitter. Samples were collected in numbered calico sample bags, and sealed ready for assaying as drilling progressed. Primary Analysis Lab: ALS QA: Duplicates 1 in 50
SEPTEMBER 2022 TO NOVEMBER 2022	Si20xxx	82		1 m interval samples were collected from an aircore drill rig after passing through a single tiered (50/50) riffle splitter. The samples were collected in numbered calico sample bags, and sealed ready for assaying as drilling progressed. Primary Analysis Lab: Bureau Veritas QA: Introduction of ELIM22 CRM Duplicates 1 in 25
AUGUST 2023 TO NOVEMBER 2023	Si21xxx	88	Aircore	1 m interval samples were collected from an aircore drill rig after passing through a single tiered (50/50) riffle splitter. The samples were collected in numbered calico sample bags, and sealed ready for assaying as drilling progressed. Primary Analysis Lab: Bureau Veritas QA: Introduction of Coarse Blanks Samples were composited in 2024 to 3m and assayed at ALS on a target market size fraction, using ICP.
AUGUST 2024 TO DECEMBER 2024	Si22xxxx	154		1m interval samples were collected from an aircore drill rig, before being composited to a nominal 3m composite. All samples were assayed at a nominal 3m including XRF full sample, and target market production fraction. Primary Analysis Lab: ALS QA: Introduction of systematic recovery sampling. Introduction of NCS DC 60116a & NCS DC 60117a CRM
JULY 2025 TO SEPTEMBER 2025	Si24xxx	28		1m interval samples were collected from an aircore drill rig, before being composited to a lithologically controlled sample (1-6m variable). All samples were assayed with a full XRF suite. Primary Analysis Lab: ALS QA: Maintenance of existing established QA processes
DECEMBER 2021	AHxxx	1		1m interval samples were collected before being split in a 50/50 riffle splitter. The samples were collected in numbered calico sample bags and sealed ready for assaying. Primary Analysis Lab: ALS
SEPTEMBER 2022 TO DECEMBER 2022	Si2HAxxx	60	Hand Auger	1m interval samples were collected before being split in a 50/50 riffle splitter. The samples were collected in numbered calico sample bags and sealed ready for assaying. Primary Analysis Lab: BV for first part of season, ALS for second part of season.
JANUARY 2025 TO FEBRUARY 2025	Si23xxxH	14		1m interval samples were collected and retained in numbered calico sample bags and sealed. No assaying completed, strictly for geological observations

Table 2: Sampling Program Details

DRILLING TECHNIQUES

Every drill hole was photographed, logged, and sampled under the Competent Person's supervision. Samples are retained as bagged splits within clearly labelled chip trays at the Diatreme Resources facility in Cooktown. The Competent Person is satisfied that the drilling, sampling, and analytical work meets the standard required for public reporting of a Mineral Resource under the JORC Code (2012)

DRILLING TECHNIQUES

The Mineral Resource Estimate is defined by 529 drill holes, all drilled vertically. Sampling was carried out using vacuum drilling, aircore drilling, and hand augering.

Drilling programs were mainly concentrated on the trailing arms and apices of the elongate parabolic dunes. Additionally, hand augering was specifically carried out in the deflationary troughs between the dunes to ensure continuity in estimating resources. Table 1 highlights the drilling techniques and holes used in the Mineral Resource Estimate.

Vacuum drilling was completed by Yearlong Contracting on a 4x4 tractor-mounted rig fitted with a 60 mm blade bit (NQ-equivalent sample size) and 1.8 m rods. Aircore drilling was carried out on a Diatreme Resources track-mounted rig with a 3" blade bit and 3 m rods. Hand augering was performed by Diatreme personnel using a Dormer Sand Auger of 2" internal diameter, with five one-metre extension rods. Drilling was terminated at refusal on damp clay basement or wet sand. All programs were designed and supervised by Diatreme Resources geologists.

SAMPLE ANALYSIS METHOD

Project samples have been analysed at either Bureau Veritas (Adelaide) or ALS (Brisbane) over the life of the project. The two laboratories' XRF methods (ALS ME-XRF26 and Bureau Veritas XF100) are regarded as comparable. In 2024, a size fraction representative of the target market specification was additionally assayed at ALS by ME-ICP64 to better align with JORC Code Clause 49. This additional ICP work was not repeated in 2025; the company determined that the initial XRF assay round should be completed as a first pass.

ESTIMATION METHODOLOGY

The Mineral Resource Estimate was prepared by modelling the silica sand unit (locally termed the "A2"). Topography was captured by LIDAR survey at a resolution of 10 points/m^2, from which a 1 m gridded digital elevation model with 10 cm relative vertical accuracy was produced. The top surface of the resource volume was set 0.3 m below the LIDAR topography, corresponding to the base of the topsoil. The base of the resource was constructed using:

- The base depth of the A2 unit determined from drilling, or augering
- The depth of the groundwater table determined from drilling, and

- Interpretation of the dune edge from LiDAR survey and aerial imagery.

The resource boundary was defined through geological interpretation, supported by analysis of dune extents visible in LIDAR and aerial imagery. The top and base of the mineralised profile were interpreted using both assayed drill samples and geological observations from hand auger holes.

Coordinates of drill hole data and the block model were transformed so each dune base aligned to a single flattened RL, accounting for significant RL variations and dune thickness variability across the deposit. This allowed grade estimation to reflect podsolisation influences and reduce vertical smearing. Grades were interpolated within three semi-soft vertical domains (upper, middle, and lower sands) to capture observed vertical grade variations. After estimation, coordinates were transformed back to their original positions. A comparison with estimates run using untransformed coordinates showed comparable global tonnes and grades, confirming no material bias from the transformation.

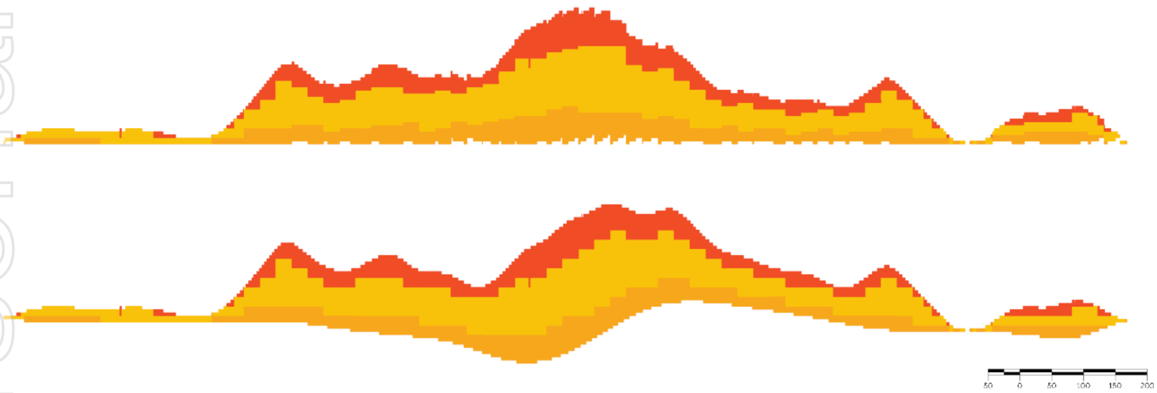


Figure 3: MRE Estimation Flattened Space vs Real Space

Hand auger holes were not used in grade estimation owing to potential sample contamination inherent to the method. As these holes sit predominantly at the deposit margins, their mineralised intervals were instead interpreted geologically and used to guide and constrain the resource boundary. The intervals corresponded closely to the interdunal level, providing additional support for the geological interpretation.

Deposit grades were estimated into a block model oriented to the dunes' average strike of 315°. Parent blocks were sized at 25 m across strike by 25 m along strike by 3 m vertical, with 1 × 1 × 1 m cubic sub-blocks used to honour the undulating geological model.

Drill hole data were composited to a nominal 3 m interval prior to estimation. Grades were estimated using IDW2 in a flattened space, with validation checks run via IDW2 in regular space and ordinary kriging in both flattened and regular space. The flattened space IDW2 estimate populated the block model for SiO_2, Fe_2O_3, TiO_2, Al_2O_3, and accessory geochemistry. Estimation was carried out in four sequential passes, with the search radii of each pass calibrated to inform classification into Measured, Indicated, and Inferred categories. Search axes for each block were oriented with the major axis horizontal along the dune strike (315°), the semi-major axis horizontal and perpendicular across the dune, and the minor axis vertical; pass-specific search distances were derived from a geological understanding of the dune system to honour the spatial structure of the data. Variogram analysis conducted in previous Mineral Resource Estimates supports the same search ellipse. A quadrant-based search was applied throughout, capped at 16 samples and requiring a minimum of two drill holes for a valid estimate. Block discretisation was set at 4 × 4 × 4 (X, Y, Z).

Bulk density was determined through laboratory testwork on dried and compacted samples collected from drilling across the Si2 Deposit. A total of 132 samples were tested. The dry bulk density was calculated as the average of the samples, and a value of 1.65 tonnes per cubic metre was adopted for tonnage estimation.

Crosschecks were run against alternative block sizes, alternative estimation methods (Inverse Distance Weighting versus Ordinary Kriging), and alternative treatments of domain boundaries and coordinate space (flattened versus real/regular). No material differences were observed across these comparisons, supporting the robustness and reliability of the final Mineral Resource Estimate.

CUT OFF GRADES

No cut-off grade was applied at the compositing, block estimation, or reporting stages. The Mineral Resource is reported from every classified block carrying an interpolated SiO_2 grade. Although no cut-off was applied, a minimum SiO_2 grade of approximately 98.5% was one of several criteria used when defining the base of the geological model in drill holes, with geological domains delineated on a combination of SiO_2 grade, sand colour, and contaminant levels. Minor internal intervals returning below 98.5% SiO_2 were retained within the high-purity silica domain where they did not materially affect overall resource quality and, as confirmed by metallurgical testwork, were not expected to impact minerals processing.

RESOURCE CLASSIFICATION

Classification of the Mineral Resource follows the principles of the JORC Code (2012 edition), with blocks assigned to Measured, Indicated, or Inferred categories reflecting high, moderate, and low confidence respectively in geological and grade continuity. The classification draws on a combination of factors, including depth of geological knowledge of the deposit, geological and mineralisation continuity, drill hole spacing, and quality control outcomes.

Additional inputs to the classification include drill hole logging, sample analytical results, geostatistical analysis, confidence in geological and grade continuity, and recent metallurgical and process test outcomes. Search and interpolation parameters, recently completed density data, and the requirements of JORC Code Clause 49 are also reflected in the classification process.

MINING AND METALLURGICAL METHODS AND PARAMETERS, AND OTHER MATERIAL FACTORS CONSIDERED TO DATE

Metallurgical testwork completed to date demonstrates that the silica sand resource responds readily to conventional washing and screening, producing a low-iron, high-purity silica sand suitable for photovoltaic glass applications.

The potential for economic extraction at the Si2 Project has been assessed against open-pit mining methods, anticipated product specifications, product marketability, and favourable logistics. On the basis of these factors, the Si2 Project is judged to have Reasonable Prospects for Eventual Economic Extraction (RPEEE) and is reported as an industrial mineral under JORC Code Clause 49.

Mineral Resource Estimate results are set out in Table 2, with the Resource Area shown in Figure 2 on the following page. Representative cross-section and long-section profiles through the Resource Area are presented in Figure 3 below. All Mineral Resources lie within EPM's held by the company.

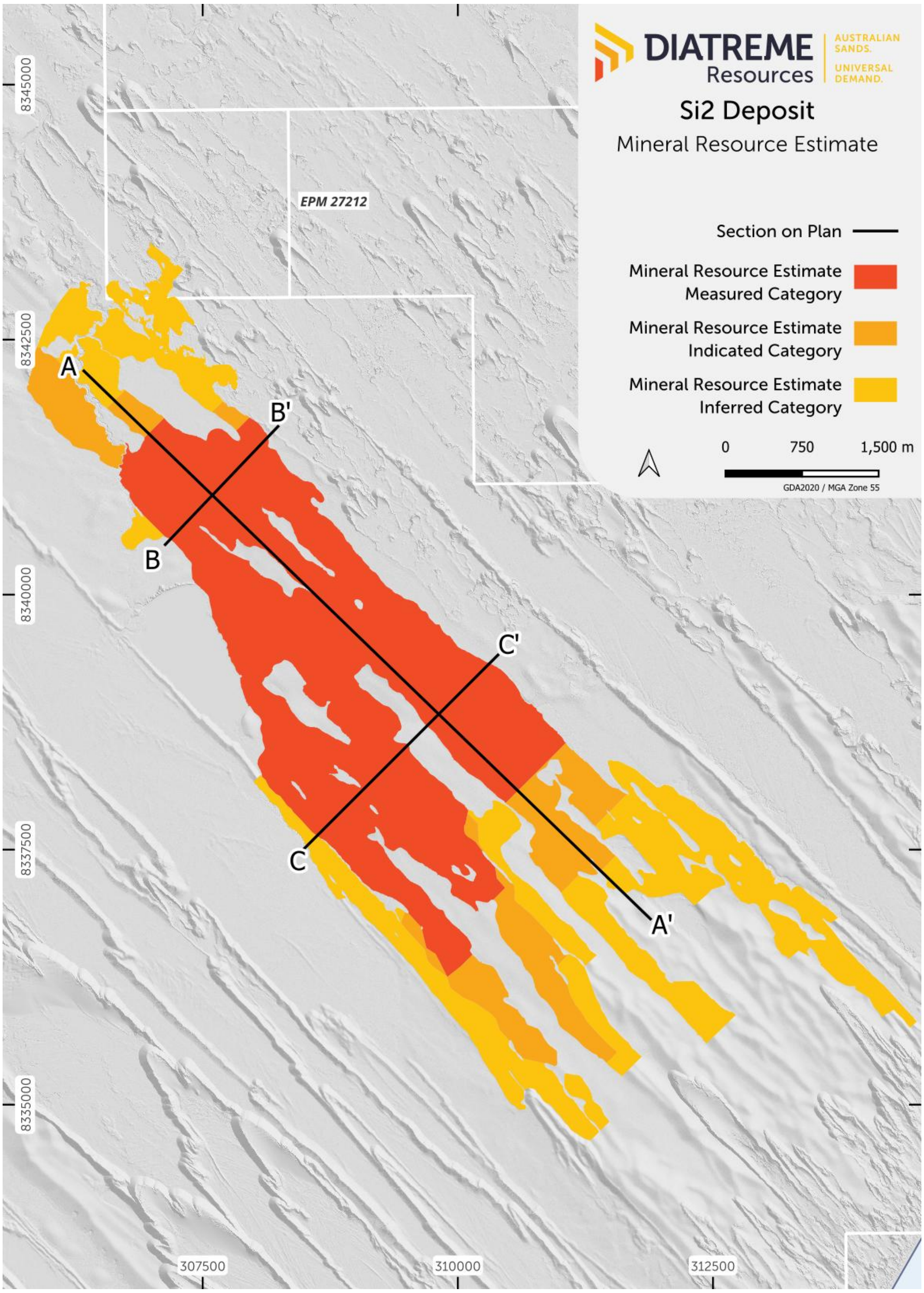


Figure 4: Mineral Resource Categories

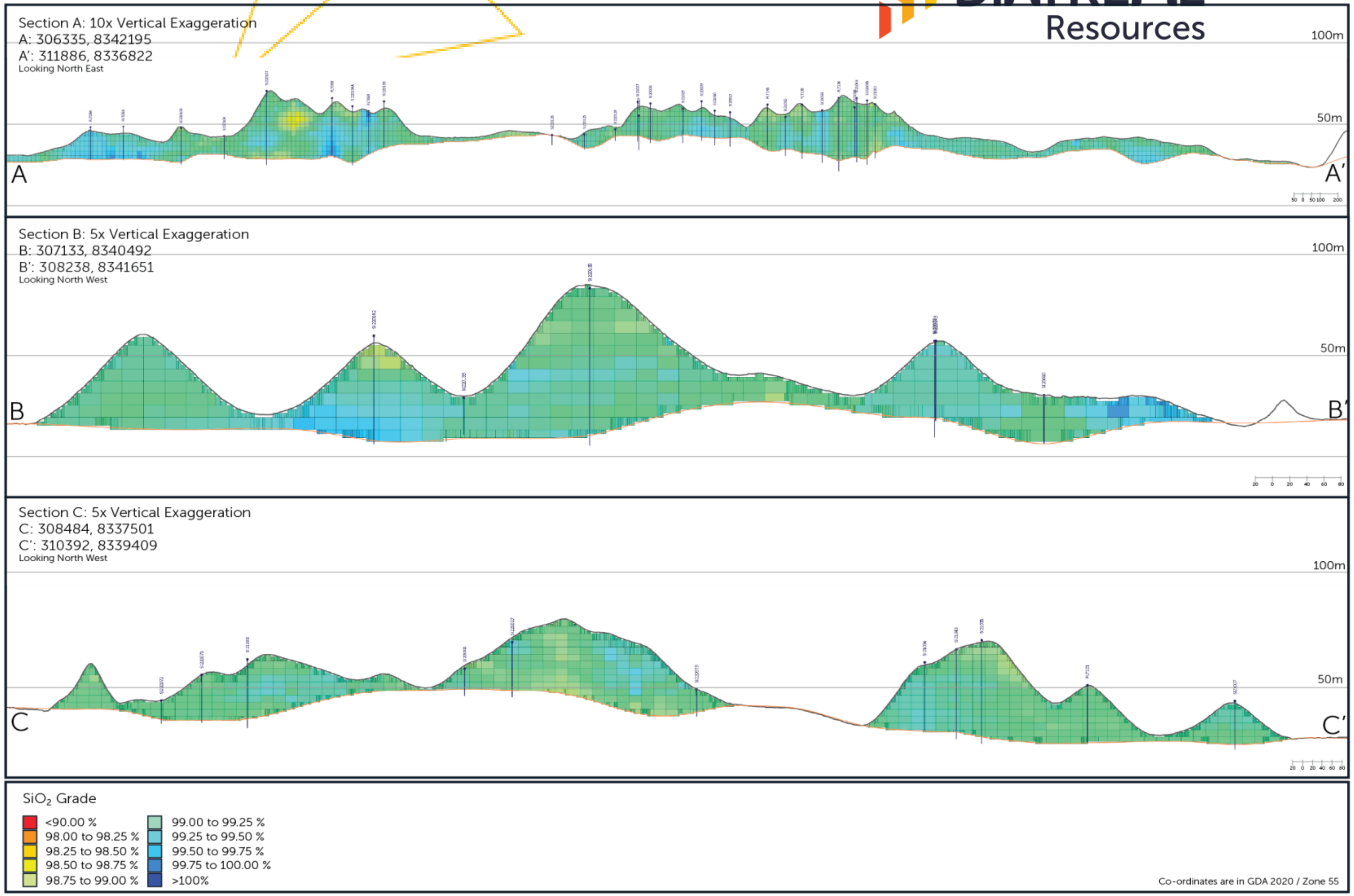


Figure 5: Sections indicating SiO2 grade across Si2.

DIATREME Resources

PROJECT	MINERAL RESOURCE CATEGORY	TONNES	SIO2	FE2O3	TIO2	AL2O3
		Mt	%	%	%	%
GALALAR	Measured	43.12	99.21	0.09	0.11	0.13
	Indicated	23.12	99.16	0.09	0.13	0.10
	Inferred	9.22	99.10	0.11	0.16	0.11
	Total	**75.46**	**99.18**	**0.09**	**0.12**	**0.12**
SI2	Measured	187.5	99.25	0.10	0.14	0.11
	Indicated	42	99.16	0.12	0.16	0.11
	Inferred	72	99.17	0.13	0.17	0.11
	Total	**301.5**	**99.20**	**0.11**	**0.15**	**0.11**
WRA	Indicated	10.3	99.2	0.15	0.24	0.16
	Inferred	81.4	99.38	0.09	0.15	0.06
	Total	**91.7**	99.36	0.10	0.16	0.07
CFS WEST	Inferred	12	99.15	0.09	0.16	0.12
	Total	**12**	**99.15**	**0.09**	**0.16**	**0.12**
CFS EAST	Measured	16.1	99.2	0.08	0.12	0.22
	Indicated	33.2	99.05	0.10	0.18	0.25
	Inferred	0.2	99.00	0.12	0.27	0.28
	Total	**49.5**	**99.10**	**0.09**	**0.16**	**0.24**
TOTAL SILICA SAND	Measured	246.72	99.24	0.10	0.13	0.12
	Indicated	108.62	99.13	0.11	0.17	0.16
	Inferred	174.82	99.26	0.11	0.16	0.09
	Total	**530.16**	**99.22**	**0.10**	**0.15**	**0.12**

Table 2: Diatreme Resources Mineral Resource Inventory across all Silica Sand Projects.

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This announcement is authorised for release by the Board.

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About Diatreme Resources

Diatreme Resources (ASX:DRX) is an emerging Australian producer of mineral and silica sands based in Brisbane. Our key projects comprise the Northern Silica Project and Galalar Silica Sand Project in Far North Queensland, located next to the world's biggest silica sand mine at Cape Flattery.

In Western Australia's Eucla Basin, Diatreme's 'shovel-ready' Cyclone Zircon Project is considered one of a handful of major zircon-rich discoveries of the past decade.

Diatreme has an experienced Board and management, with expertise across all stages of project exploration, mine development and project financing together with strong community and government engagement skills.

Global material solutions group Sibelco is Diatreme's development partner on its Queensland silica projects portfolio. Sibelco has completed a two-tranche investment of $35 million taking its total project interest to 26.8%, with the balance (73.2%) held by Diatreme. In addition, Sibelco made a $13.97 million investment at the corporate level.

Diatreme's silica sand resources will contribute to global decarbonisation by providing the necessary high-grade silica for use in the solar PV industry. It has a strong focus on ESG, working closely with its local communities and all other key stakeholders to ensure the long-term sustainability of our operations, including health, safety and environmental stewardship.

For more information, please visit www.diatreme.com.au

ASX releases referenced for this release:

- 13 April 2026 – Sale of CFS to DRX/Sibelco Silica J/V
- 26 March 2026 – Favourable Si2, Casuarina drilling boosts silica pipeline
- 09 September 2025 – Bulk metallurgical testwork confirms NSP product quality
- 23 June 2025 - Mineral Resource Estimate upgrade paves way for Northern Silica Project PFS
- 6 December 2023 – New maiden 91.7Mt silica resource at Western Resource Area
- 17 July 2023 – Cape Flattery Silica DFS Confirms Excellent Economics – *announced by MLM*
- 3 March 2023 – Maiden Inferred Mineral Resource of 12Mt at 99.15% SiO2, 0.09% Fe2O3 Estimated for Cape Flattery Silica West Project – *announced by MLM*
- 20 September 2021 – Galalar Silica Resource Expands by 22% to 75.5Mt

NOTE:
Diatreme confirms that it is not aware of any new information or data that materially affects the information included in the original releases and that all material assumptions and technical parameters underpinning the estimates in the original releases continue to apply and have not materially changed. Diatreme confirms that the form and context in which the competent person's findings are presented have not been materially modified from the original releases.

COMPETENT PERSONS STATEMENT

The information in this report that relates to Exploration Targets, Exploration Results, and Mineral Resources is based on information compiled by Mr Frazer Watson, a Competent Person who is a Member of The Australasian Institute of Mining and Metallurgy and the Australian Institute of Geoscientists. Mr Watson is a full-time employee of Diatreme Resources. Mr Watson has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Watson consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The corresponding JORC 2012 Table 1 is attached to this report and can be found in Appendix 1.

APPENDIX 1: JORC TABLE 1

SECTION 1: SAMPLING TECHNIQUES AND DATA

CRITERIA	EXPLANATION	COMMENTARY
SAMPLING TECHNIQUES	• Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	• For drill holes reported PLT001 to PLT247, Vacuum drilling samples were collected in 1m intervals, before being passed through a single-tiered 50/50 riffle splitter. The sample was sent to ALS Brisbane from which 250g was pulverised to produce a fused bead before being assayed by method code ME-XRF26. • For drill holes reported Si20001 through to Si20076, Aircore drilling samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The sample was sent to Bureau Veritas in South Australia from which 150g was pulverised to produce a fused bead before being assayed by method code XF100. • For drill holes reported Si20077 through to Si20082, Aircore drilling samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The sample was sent to ALS Brisbane from which 250g was pulverised to produce a fused bead before being assayed by method code ME-XRF26. • For hand auger hole reported AH001, hollow stem auger samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The sample was sent to Bureau Veritas in South Australia from which 150g was pulverised to produce a fused bead before being assayed by method code XF100. • For hand auger holes reported Si2HA0002 to SI2HA0013, hollow stem auger samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The sample was sent to Bureau Veritas in South Australia from which 150g was pulverised to produce a fused bead before being assayed by method code XF100. • For hand auger holes reported Si2HA0014 to SI2HA0061, hollow stem auger samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The sample was sent to ALS Brisbane from which 250g was pulverised to produce a fused bead before being assayed by method code ME-XRF26. • For hand auger holes reported Si23001H to Si23130H, hollow stem auger samples were collected in 1m intervals (~2kg). These samples were not sent for assay, instead were used primarily as geological observations. The full sample has been retained for any future analysis. • For drill holes reported Si21001 through to Si210088, Aircore drilling samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The sample was sent to Bureau Veritas in South Australia from which 150g was pulverised to produce a fused bead before being assayed by method code XF100. A second analysis program (focussing on grade of a particular size fraction) was conducted on the Si21 series drill holes. The original sample material was composited into nominal 3m composites and submitted to ALS Brisbane for sieving into three fractions +710µm, -710µm+106µm and -106µm. The respective fractions were then weighed, followed with the 710µm+106µm fraction pulverised and assayed by method code ME-ICP64. • For drill holes reported Si220001 to Si220153, Aircore drilling samples were collected in 1m intervals, before being composited by scoop into nominal 3m samples (~1kg). This material was submitted to ALS Brisbane for sieving into three fractions +710µm, -710µm+106µm and -106µm. The respective fractions were then weighed, followed with the 710µm+106µm fraction pulverised and assayed by method code ME-ICP64. In addition a sample representing the full particle size distribution was split, pulverised and then assayed by ME-XRF26. • For drill holes reported Si24001 to Si24028, Aircore drilling samples were collected in 1m intervals before being composited by scoop into nominal 2-6m composites controlled by lithological variables (~1kg). This material was then submitted to ALS Brisbane from which 250g was pulverised to produce a fused bead before being assayed by method ME-XRF26.

CRITERIA	EXPLANATION	COMMENTARY
		• Mr Watson considers the quality of the sampling method to be fit for the deposit style, and the stage of exploration, given the homogenous nature of this silica sand deposit.
DRILLING TECHNIQUES	• Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	• Three (3) types of drilling have been utilised for exploration, Aircore (AC), Vacuum (VX) and Hand Auger (HA). • AC drilling was by a track mounted drill rig with a 3” blade bit, and a rod length of 3m. • VX drilling was by a tractor mounted drill rig with a 60mm diameter blade bit, and a rod length of 1.8m. • Hand Auguring (HA) was conducted using a Dormer Sand Auger with an internal diameter of 2”. • Aircore and Vacuum drilling was to refusal, which occurs at geologically determined contact such as clayey sands at the base of mineralisation, or a water table. This is due to the limitations of AC drilling at the water table, and limitations of the AC drill rig when penetrating the clay layers. • Mr Watson considers the quality of the sampling method to be fit for the deposit style, as mineral sands are easily contaminated, or recoveries can be poor and not representative using other drilling methods.
DRILL SAMPLE RECOVERY	• Method of recording and assessing core and chip sample recoveries and results assessed. • Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	• Since 2024, sample recovery is monitored at the rig by recording sample mass of each 1m interval to observe for the presence or deviation from a consistent sample size. Weighing of samples at the drill site was not undertaken in a systematic manner in prior years. In the absence of systematic weighing, sample recovery was visually monitored on the rig for a consistent sample size. • Sample recovery is maximised within a closed system from the drill bit to the riffle splitter. • After encountering wet clays, sacrificial rods are drilled into clean dry sand, to flush out any contamination through the drilling hoses, prior to drilling the subsequent drill hole. • No relationship between recovery and grade has been observed, as the orebody is relatively homogenous. • Correct interval delineation on AC drilling is achieved with metre intervals marked on the drill mast, and samples are collected when the base of the top drive reaches a metre interval.
LOGGING	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography. • The total length and percentage of the relevant intersections logged.	• All drill holes have been logged in their entirety, with qualitative descriptions of grain size, sphericity, roundness, moisture content, lithology, and colour recorded. • Photography is captured on a chip tray basis firstly at the drill rig, and then later on a chip tray compartment by compartment basis when samples have dried. • Sample photography in a controlled setting using Imago software with a Canon EOS R5 and a Canon 24-50mm lens , a hexadecimal colour value is extracted from the imagery, and the RGB values are derived through python scripts. Colour photography is verified against a Calibrite ColorChecker. • The quality of logging is sufficient for this stage of exploration.
SUB-SAMPLING TECHNIQUES AND SAMPLE PREPARATION	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	• Prior to 2023, VX and AC samples were riffle split after the cyclone, and placed in sample bags representing 1m intervals. • Since 2024, AC samples were scooped from the sample bags representing 1m intervals, and composited to a nominal 3m composite. The single scoop is approximately 330g in mass. • Where sample preparation was completed at ALS in Brisbane. Full samples are dried at 105°C, then weighed (WEI-22g), then a split is screened (SCR-61) into three size fractions +710µm, -710µm+106µm and -106µm, with a split of the raw sample retained. A nominal 150g split of the raw sample, and a nominal 150g split of the -710µm+106µm fraction are then pulverised using a tungsten carbide ring mill (PUL-33), prior to being assayed. During 2024, the full sample was assayed, and a subsample was sieved into target fractions. • Where sample preparation was completed by BV in South Australia. Samples progressed through the PR001 method where samples are sorted, weighed wet, and then dried at 105°C, samples are then split using a rotary sample divider, and volumetrically weighed to a nominal 150g before undergoing the PR305 method where samples are pulverised in a tungsten carbide bowl.

CRITERIA	EXPLANATION	COMMENTARY
	• Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled.	• The Competent Person considers that the -710µm+106µm size fraction does not represent a final "product" grade, as heavy minerals are not removed through the sieving process, nor is the material washed, whereas in a final target specification, both of these processes would be undertaken. • The PUL-33 method has a QC check on a 20g split to ensure >85% passes -75µm • Coarse flushes of an unpulverized sample matching ELIM22 CRM has been introduced to both clean the lab pulveriser between drill holes, and test for any contamination. ELIM22 was prepared by OREAS, specifically for silica sand material in the Cape Bedford / Cape Flattery dune systems. • Field duplicate results are validated upon receipt of lab results, particular attention is paid to Fe_2O_3, and TiO_2. • A coarse flush of the raw ELIM22 sample is included after intersecting a deleterious horizon – and this is used to clean the Tungsten Carbide ring mill / pulveriser at ALS Brisbane. All samples are pulverised sequentially through the same pulveriser. • Crushing is not required as the grain size of the sample material is suitable for pulverizing. • Mr Watson considers the drill sample sizes as appropriate for the grain size of the material, the style of mineralisation and the nature of the drilling program. • These methods are determined to be appropriate by the Competent Person to avoid sample carry-over contamination, in addition Cr_2O_3 is monitored to ensure that pulverisation is performed in a non-ferrous pulverising bowl.
QUALITY OF ASSAY DATA AND LABORATORY TESTS	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	• As ME-XRF26, and XF100 methods are considered a total digest, it is considered appropriate for silica sand when assessing full sample geochemistry. • Loss On Ignition (LOI) determined by thermogravimetric analysis (TGA) using method code OA-GRA05x or ME-GRA05 at ALS or TG002 at Bureau Veritas) and, where a sample is placed in a furnace at ambient temperature and then heated to 1000°C, and then weighed. • Field duplicates were submitted at a nominal rate of 1 in 25 in line with the quality assurance procedure. Prior to 2023, this was nominally 1 in 50. • CRM (ELIM22) is utilised every 33rd sample. This CRM was introduced to the program in 2021. It has been noted that the variability in this sample has broadened in recent years, and that the number of samples submitted to the laboratory during drilling programs far exceeds the sample rates submitted during initial certification. • Either CRM NCS 60116a or NCS 60117a are used 2 in 100 – for samples drilled after 2024 • The quality control procedures adopted by Diatreme establish an acceptable level of accuracy and precision. Bureau Veritas, and ALS conduct their own internal checks, and these results have been provided to Diatreme and are monitored by both parties as part of the quality control process. • The variability observed between the primary sample and the field duplicate assay results are considered appropriate for the style of mineralisation by the Competent Person.
VERIFICATION OF SAMPLING AND ASSAYING	• The verification of significant intersections by either independent or alternative company personnel. • The use of twinned holes. • Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. • Discuss any adjustment to assay data	• Mr Watson and various Diatreme Resources' Exploration Geologists have personally inspected all sample intervals. • Several twinned holes have been completed, with minimal sampling bias observed, the only difference being the depth of refusal changed which is considered to be related to seasonal changes groundwater levels. • Collar and geological logging is captured by and stored within the geological logging/database software MX Deposit, in accordance with company procedures. • Photographic data is captured, and stored within Imago, a software package that acts as a repository and analysis tool for geoscientific imagery. • Assay data is recorded, and stored in MX Deposit, a drill hole Database software. • No adjustment has been made to assay data.

CRITERIA	EXPLANATION	COMMENTARY
LOCATION OF DATA POINTS	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control.	• All drill hole locations have been surveyed using Spectra Precision SP60, with a Trimble RTX CenterPoint DGPS correction ± 0.05m on the horizontal plane. • The collar data is recorded in the UTM coordinate system: Map Grid of Australia 1994 (MGA94) Zone 55, this is then reprojected to GDA2020 Zone 55 for compatibility with other spatial files. • All drill holes are shallow and vertical, no down-hole surveying is conducted. • Digital elevation models derived from LiDAR (December 2022) were used as the topographic surface to generate RL's for each collar. The DEM was generated via a cloth simulation function, using an approximate 10 ground classified points per square metre. Relative accuracy is considered to be ± 0.1m.
DATA SPACING AND DISTRIBUTION	• Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	• Auger drilling occasionally is performed at the edge of a given dune to provide geological observations of the contact between the eluviated sand and the illuviated horizon. • First pass drilling spaced nominally at 380m along dune crests, and infill drilling at a nominal 180 - 200m along the trailing arm of an elongate parabolic dune, and in the interdunal valleys, although the Competent Person considers data spacing at these intervals are not a material constraint on the development of geological grade or geological continuity, and as such, the Competent Person considers the data spacing to be more than appropriate for this style of deposit, at this stage of exploration. • Select samples have been composited to nominal 3m intervals, following recommendations from a variability assessment completed by Measured Group in 2024, and also on an assessment that the 3m compositing also aligns with likely SMU's for the deposit. This is defined in further detail in the Sampling Techniques section of this Table.
ORIENTATION OF DATA IN RELATION TO GEOLOGICAL STRUCTURE	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	• The deposit style is an unlithified aeolian sand deposit, comprised of a series of complex parabolic and elongate parabolic dune systems which are repeatedly deflated and are superimposed upon older dune systems. • The mineralisation process (podsolisation) is gravitationally controlled. The Competent Person has determined that vertical drilling intersects the bedforms at an angle which represents the true width of mineralisation. • The orientation of heavy mineral bedding (if present) is considered immaterial due to the processing methods of silica sand. The main grade control on economic extraction is the podsolisation profile. • No sampling bias is introduced by the orientation of drilling.
SAMPLE SECURITY	• The measures taken to ensure sample security.	• Sample bags were sealed by cable-tie, and transported in polywoven bags, then securely stored in a locked yard on-site until transported by courier to the respective labs. • Transport chain of custody forms have been reviewed for each sample dispatch. • Submission reconciliation reports are provided by the laboratory and checked against the sample submission forms.
AUDITS OR REVIEWS	• The results of any audits or reviews of sampling techniques and data.	• An audit in 2025 of the drill hole database was conducted by Measured Group. • A review of the sampling techniques was conducted by the Competent Person in 2025, indicating compliance to internal standards.

SECTION 2: REPORTING OF EXPLORATION RESULTS

CRITERIA	EXPLANATION	COMMENTARY
MINERAL TENEMENT AND LAND TENURE STATUS	• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. • The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	• These Exploration Results comprise exploration on the Si2 Deposit, which is the mineral resource within the Northern Silica Project, which is located adjacent to the coastline in Far North Queensland, approximately 53km north of Cooktown. The project is adjacent to the south of the Cape Flattery Silica Mines (CFSM) Mining Lease. CFSM has been in operation since 1967 and is Queensland's largest producer of high purity silica and is reported to have the highest production of high purity silica sand of any mine historically. • The project is located at the northern end of the Cape Flattery/Cape Bedford dune field complex within the Exploration Permits for Minerals (EPM) 17795 & 27212. • Most of the EPM, and the entirety of the Si2 Deposit is located on one land title, Lot 35/SP232620, a freehold lot of 110,000 hectares. • The Project and EPM is in the Mareeba Mining District and falls within the Hope Vale Aboriginal Shire Council area. This lies approximately 35km north of the township of Hope Vale, with a population of approximately 1,500 in the Hope Vale Aboriginal Shire Council. • EPM 17795, EPM 27265, EPM 25734, EPM 27212, and EPM 27430 comprise an "exploration project PROJ310". • PROJ310 is an extensive EPM package comprising approximately 625km2 covering the majority of the Cape Flattery-Cape Bedford Quaternary dune field complex. • PROJ310 is owned by Cape Silica Holdings Pty Ltd and its subsidiaries, which is a Joint Venture between Diatreme Resources 73.2% and Sibelco Silica Pty Ltd 26.8%. • Diatreme was granted a renewal on EPM 17795 "Cape Bedford" until 21 June 2026 based on continued targeting of heavy mineral sands and silica sand. The EPM was granted under protected Native Title Protection Conditions. As of May 2026, the tenure is in good standing. A renewal has been submitted. • EPM 27212 is due for renewal in Q4 2026. • The NSP / SI2 deposit area is covered by Mining Lease Applications (ML 100308, ML 100309, ML100310, ML100311, ML 100312, ML 100313), currently undergoing approvals processes.
EXPLORATION DONE BY OTHER PARTIES	• Acknowledgment and appraisal of exploration by other parties.	• Exploration for silica sand has been undertaken in the Cape Flattery – Cape Bedford area in 11 Authorities to Prospect (ATP's) or Exploration Permits for Minerals (EPMs) since the 1960's. In general, past exploration of the dune field has primarily focused on the prominent active parabolic dunes of clean white silica sand. • Historical exploration activities missed the Si2 Deposit in its entirety, until discovery by Diatreme Resources in late 2021. • As there are no assay certificates for this historic data, and the locations of which are dubious, the data is considered qualitative and is not used for Mineral Resource Estimation, or Exploration Targeting.
GEOLOGY	• Deposit type, geological setting and style of mineralisation.	• The Northern Silica Project is comprised of unlithified aeolian dune complexes. • The Cape Flattery & Cape Bedford dune fields are aeolian dunes established in the Pleistocene epoch and regularly remobilised during the Pleistocene and Holocene epochs. The dune fields are situated on a coastal plain overlying the Hodgkinson Formation basement with Dalrymple Sandstone forming mesa on basement highs. • Mineralisation is thought to be due to repeated eluviation and illuviation events on immobilised dune systems comprised of an existing quartzose sand source, with reactivated dune systems also exhibiting mineralisation. Intradunal valleys tend to be a surface expression of the B1 horizon, and typically are not considered mineralised. • Deleterious metals are thought to have been eluviated by organic acids, which are transported by gravity through the stratigraphic column and illuviated either by binding to clay rich horizons, or transported away from the deposit through the water table.

CRITERIA	EXPLANATION	COMMENTARY
DRILL HOLE INFORMATION	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: • easting and northing of the drill hole collar • elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar • dip and azimuth of the hole • down hole length and interception depth • hole length. • If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case	• All material collar information for drill holes has been aggregated in the Table of Material drill holes and Results attached in this appendix to this report.
DATA AGGREGATION METHODS	• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated	• Data aggregation used in this report is a calculation of the mean average for each reported variable across the respective mineralised profile for that drill hole. • All intercepts have been aggregated in the Table of Material drill holes and Results attached in this appendix to this report.
RELATIONSHIP BETWEEN MINERALISATION WIDTHS AND INTERCEPT LENGTH	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	• All drilling was vertical (-90°) intersecting undulating flat-lying aeolian dune sands. • Downhole length correlates with true width of mineralisation. • The deposit is a large homogenous mass of eluviated aeolian sands. Intercept length is an order of magnitude smaller than the mineralisation width. The eluviated zone is gradual, with in most cases a distinct delineable contact for the illuviated zone.
DIAGRAMS	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being	• Plan view of drill hole collar locations and appropriate sectional views are contained in this report.

CRITERIA	EXPLANATION	COMMENTARY
	reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	
BALANCED REPORTING	• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	• All mineralised silica sand results used in the estimation of this Mineral Resource are reported. • Where the results in the table are not published, there is either organics present in the first metre, or unmineralized sands / sandy clays below the mineralised horizon. The acknowledgement of these intervals/zones are considered material in the context that they exist and are used to constrain the resource geometry, but the results are considered immaterial in the context of populating the grade model.

OTHER SUBSTANTIVE EXPLORATION DATA	• Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	• Fe_2O_3 percentage is the most significant limiting factor on conversion of naturally occurring silica sand (in this region) to high purity silica sand product and determines value after SiO_2 percentage.
		• Fe_2O_3 when found in association with TiO_2, does not act as a contaminant or barrier to refining high- purity silica sand, with metallurgical testing showing gravity separation to accurately remove this impurity.
		• Colour (oranges, yellows, reds) tend to be a significant - but not limiting – indicator on the identification of deleterious or low yielding sands.
		• For the 1t bulk sample, a nominal 850g was composited from each of 1147 intervals drilled in 2023 selected to represent the Measured Category of the Si2 Mineral Resource. The relevant drill holes and intervals are included in this Appendix in the Table of Material drill holes and Results.
		• Geochemical results were performed at ALS Brisbane using ME-XRF26 for head grade & lower purity samples, and ME-PKG85 for higher purity product samples. ME-PKG85 and ME-XRF26 are considered a full digest.
		• Metallurgical testwork was performed at MT Carrara, and consisted of:
		  ◦ Receiving a 1t bulk sample,
		  ◦ Sample homogenisation, and then sub sampling 5kg of feed material.
		  ◦ Sieving and retaining the -1mm+0.045mm product stream
		  ◦ Sieving and retaining the -0.710mm+0.106mm product stream sample
		  ◦ Undertaking a Heavy Liquid Separation using Bromoform and Acetone to achieve a SG of 2.7 (This is a benchtop scale testwork method to simulate the gravity separation process)
		  ◦ The 2.7 SG floats are then attritioned for 5 minutes with 75% solids without any reagents
		  ◦ The material is then wet sieved at 0.106mm, with the oversize fraction then passed through two reading IRMS units at 3.0A, 11500 Gauss and 8.0A,18000 Gauss, respectively. Both with a Pole Gap of 4mm and a Roll Speed of 140rpm.
		  ◦ The Non Magnetic fraction is then considered representative of final product for this stage of study.

FURTHER WORK	• The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).
	• Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.
		• Mr Watson recommends the following programs to increase geological confidence on the deposit.
		  ◦ Undertake sizing analysis and ICP (or other suitable low Fe_2O_3 detection limit assay) on samples from 2021 & 2022 programs, and maintaining this on future drill programs.
		  ◦ In particular, the B1 horizon needs to be checked and tested in the interdune locations by drilling, or geological observations with hand augering to assist better defining geological continuity and support potential upgrade areas.
		  ◦ Further study stages may require an improved understanding of environmental and cultural constraints (currently being identified through an EIS) relevant to the development of the deposit.
		  ◦ Maintain regular bulk density measurements in future drill programs.
		  ◦ Complete mineralogical analysis on Fe bearing minerals (such as surface coats, and inclusions) within the silica sands, and with respect to the relevant size fractions.

CRITERIA	EXPLANATION	COMMENTARY
		• Establishment of a geometallurgical model to underpin the relationship between head grade and amenability to processing. • Submission of samples for umpire checks and bulk density assessment, is underway. • Testing of lateral extensions of the deposit toward the Southeast • Maintain the routine use of Certified Reference Materials (CRMs) to monitor and validate assay accuracy for primary and deleterious elements. • Geochemical analysis of the +710μm and -106μm fractions • Maintain regular collection of bulk density measurements to support accurate tonnage estimation. • Verify and refine the interpretation of topsoil thickness across the resource area, considering the observed variability in vegetation density.

SECTION 3: ESTIMATION AND REPORTING OF MINERAL RESOURCES

CRITERIA	EXPLANATION	COMMENTARY

DATABASE INTEGRITY	• Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.
	• Data validation procedures used.
		• The Mineral Resource Estimate for the Si2 Deposit is based on information provided by CSHPL. Mr Watson considers it appropriate and reasonable for the purpose of estimating Mineral Resources in accordance with the guidelines of the JORC Code (2012).
		• The data used for resource estimation, includes but was not limited to:
		  ◦ drill hole collar information, including total hole depths;
		  ◦ drill hole lithological logging data;
		  ◦ Sample data, including sample intervals and assay results
		  ◦ Metallurgical testwork results;
		  ◦ Density measurements;
		  ◦ Quality Assurance/Quality Control (QAQC) data.
		• Data validation procedures included checks on collar locations, assay results against laboratory certificates, lithological coding consistency, and QAQC performance. No material data errors were identified.

SITE VISITS	• Comment on any site visits undertaken by the Competent Person and the outcome of those visits. • If no site visits have been undertaken indicate why this is the case.	• The Competent Person (Mr Watson) has undertaken quarterly site visits since 2021. During the visits, active drilling and sampling procedures were observed, and field observations were made of the dune field characteristics. The site visit confirmed that drilling practices, sampling methods, and geological interpretations were consistent with the data provided.
GEOLOGICAL INTERPRETATION	• Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. • Nature of the data used and of any assumptions made. • The effect, if any, of alternative interpretations on Mineral Resource estimation. • The use of geology in guiding and controlling Mineral Resource estimation. • The factors affecting continuity both of grade and geology.	• The Si2 Deposit is located within the Cape Bedford–Cape Flattery Dune Field. Silica sand mineralisation is predominantly hosted within the trailing arms and apices of elongate parabolic aeolian dunes. • The Mineral Resource is generally constrained to these dune features, which are clearly defined by surface LiDAR imagery. Drilling often intersects overlapped dunal features, which are not represented by LiDAR or aerial photography. • Interdunal areas are often devoid of thick aeolian sand and predominantly exhibit exposed B1 horizons, clays, bedrock, or other sediments. Where drilling has intersected obscured silica sand mineralisation, the sampled sand has been included in the geological model. • There is an observable basement high coincident with the topographic high towards the coastline on the western dunes. • The interpreted geology of the Si2 Deposit is considered robust, and alternative interpretations are unlikely to materially impact the Mineral Resource Estimate.
DIMENSIONS	• The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	• The Mineral Resource Estimate spans a total area of 1611 hectares with varying dimensions: a maximum length along strike of 10.5 km and a width up to 3.5 km. The average thickness of the resource is 10-11 metres, though it can reach up to 55 metres. The top of the resource at the dune crest varies in elevation from 20 mRL to 114 mRL, corresponding to the topography, while the bottom ranges from 10 mRL to 96.5 mRL, aligning with the water table or resource basement level. • The depth of the resource below the surface is 0.3m, the deposit is effectively mineralised from surface.

CRITERIA	EXPLANATION	COMMENTARY

ESTIMATION AND MODELLING TECHNIQUES	• The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.
	• The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.
	• The assumptions made regarding recovery of by-products.
	• Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).
	• In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.
	• Any assumptions behind modelling of selective mining units.
	• Any assumptions about correlation between variables.
	• Description of how the geological interpretation was used to control the resource estimates.
	• Discussion of basis for using or not using grade cutting or capping.
	• The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.
		• The Mineral Resource Estimate was prepared by modelling the high-purity silica sand unit (A2). The geological model incorporated several key parameters. The topography surface was surveyed using LIDAR techniques to a resolution of 1 m horizontally and 10 cm relative vertical accuracy. The top surface of the resource volume was set at 0.3 m below the LIDAR topography, representing the base of the topsoil. The base of the resource was constructed from:
		  • The base depth of the A2 unit determined from drilling
		  • The depth of the groundwater table determined from drilling
		  • Interpretation of the dune edge from LiDAR survey and aerial imagery
		• The resource boundary was established by geological interpretation and analysis of surface dune extents visible in LIDAR and aerial imagery. Both assayed drill samples and geological observations from hand auger holes were used to interpret the top and base of the mineralised profile
		• Coordinates of drill hole data and the block model were transformed so each dune base aligned to a single flattened RL, accounting for significant RL variations and dune thickness variability across the deposit. This allowed grade estimation to reflect podsolisation influences and reduce vertical smearing. Grades were interpolated within three semi-soft vertical domains (upper, middle, and lower sands) to capture observed vertical grade variations. After estimation, coordinates were transformed back to their original positions. A comparison with estimates run using untransformed coordinates showed comparable global tonnes and grades, confirming no material bias from the transformation.
		• Hand auger holes were excluded from grade estimation due to concerns about sample contamination associated with the drilling method. These holes were predominantly located at the edges of the deposit, and their mineralised intervals were geologically interpreted to guide and constrain the resource boundaries. These intervals closely matched the interdunal level, further validating the geological interpretation.
		• A block model was used to estimate the deposit grade. The orientation of the block model was set to the average strike of the dunes (315 degrees). The dimensions for the parent blocks were determined as 25 m across strike by 25 m along strike by 3 m vertical, which were then subdivided into sub-blocks of 1 x 1 x 1 m to best fit the undulating geological model.
		• All drill hole data were composited to nominal 3 m intervals prior to grade estimation.
		• Grade estimation was completed using IDW at a power of 2 and a validation check estimate was completed using Ordinary Kriging.
		• In the 2025 estimate, Ordinary Kriging was used to populate the block model for SiO_2, Fe_2O_3, TiO_2, Al_2O_3, and LOI. For the current estimate the method was changed to IDW^2: the A2 silica sand is consistently high-purity and low-variability, producing high-nugget variograms in which kriging's weighting offers little practical benefit over a more transparent and reproducible distance-based estimator.
		• The grade estimation process was conducted over 4 (four) sequential passes, each defined by specific search radii that help to guide to the categories of 'Measured', 'Indicated' and 'Inferred' in resource classification.
		• This methodology involved setting the major sample search parameters for each block horizontally in the average strike direction of the dune (315 degrees), the semi-major search direction is also set horizontal (perpendicular to the major search direction) across the dune, and the minor search direction is set to vertical.
		• Search distances were informed by variographic analysis from prior estimates to align the interpolation with the spatial characteristics of the data, even though IDW does not strictly require it. All passes used a quadrant-based search with the maximum number of samples set at 16 and required a minimum of two drill holes for reliable grade estimation. Block discretisation of 4 x 4 x 4 (X,Y, Z) was employed.

MOISTURE	• Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	• Tonnages are estimated on a dry basis. Bulk density testwork was completed on dried and compacted samples, supporting a dry bulk density of 1.65 tonnes per cubic metre, which is typical for silica sand deposits.
CUT-OFF PARAMETERS	• The basis of the adopted cut-off grade(s) or quality parameters applied.	• No cut-off grade was applied during compositing, block estimation, or reporting. The Mineral Resource is reported from all classified blocks with interpolated SiO_2 grades.

CRITERIA	EXPLANATION	COMMENTARY
		• While no cut-off was applied, a minimum SiO_2 grade of approximately 98.5% was one of several factors considered when defining the base of the geological model in drill holes. Geological domains were based on a combination of SiO_2 grade, sand colour, and contaminant levels. • Minor internal intervals with SiO_2 grades below 98.5% were included within the high-purity silica domain where they did not materially affect the overall quality of the Mineral Resource.
MINING FACTORS OR ASSUMPTIONS	• Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	• The 2023 Northern Silica Scoping Study identified that mining operations will involve extracting material directly from the face using a Wheel Loader. Once extracted, the material will be transported to the processing plant either through a conveyor system or via a slurry pipeline. • The Scoping Study excluded selective mining. The entire face will be mined. • Some intervals of less than 98.5% SiO_2 are included within the high purity silica unit however, these do not materially dilute the resource. • The upper 300mm is considered topsoil and reserved for rehabilitation purposes. This overburden surface forms the upper boundary of the estimated geological domain and is not included in the Mineral Resource Estimate.
METALLURGICAL FACTORS OR ASSUMPTIONS	• The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	• Metallurgical testwork completed to-date confirms the silica sand resource is readily amenable to upgrading by screening, density separation, attritioning, and magnetic separation to produce a low iron, high purity silica sand for photovoltaic applications (solar panels). • Metallurgical testwork completed to date across the NSP has been benchtop in nature. However the benchtop methods are agreeable with bulk testwork undertaken at the Cape Flattery Silica deposit, and the Galalar Silica Sand project. • These initial metallurgical test results clearly demonstrate that low iron, high purity silica sands are potentially deliverable. As final products may require tight specifications, further systematic metallurgical testing should be considered from future infill and grade control drilling.
ENVIRONMENTAL FACTORS OR ASSUMPTIONS	• Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfield project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be	• CSHPL is currently undertaking an EIS on the Northern Silica Project. The study has not yet been completed, this Mineral Resource Estimate does not include a detailed environmental assessment at the Si2 Deposit, although early findings are considered material to acknowledge. • Based on the nature of the deposit and proposed mining method, environmental factors are not expected to present significant barriers to eventual economic extraction. • The 2023 Northern Silica Scoping Study identified in a processing flowsheet where high Fe, oversize, low grade, heavy minerals or slimes are rejected from product streams. The material will be stacked to form a replacement dune as a post mining surface, suitable for rehabilitation. The coagulants and flocculants used in processing are considered to be environmentally neutral. Early-stage considerations indicate that the proposed mining and processing activities are likely to have manageable environmental impacts, subject to future detailed assessments. • The Si2 dune system lies above a perched aquifer, and a deeper dune aquifer which are hydrogeologically connected to window lakes within the dune fields. At present there is no relationship established between mining and the water levels of these lakes.

CRITERIA	EXPLANATION	COMMENTARY
	reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	• The Si2 deposit area is proximal to several wetlands, vegetation types in the dune area are considered habitat for the Ctenotus rawlinsonii skink, and there are several protected plant species in the area such as Xanthostemon arenius, Acacia solenota, Dendrobium johannis, Myrmecodia beccarii. The impact of the presence of these species in the area, on potential extractive operations is unknown, and is currently in assessment.
BULK DENSITY	• Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. • The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit. • Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	• Bulk density was determined through laboratory testwork on dried and compacted samples collected from drilling across the Si2 Deposit. A total of 132 samples were tested. The dry bulk density was calculated as the average of the measured samples, and a value of 1.65 tonnes per cubic metre was adopted for tonnage estimation. Void spaces and porosity are not considered material given the aeolian dune nature of the deposit.
CLASSIFICATION	• The basis for the classification of the Mineral Resources into varying confidence categories. • Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). • Whether the result appropriately reflects the Competent Person's view of the deposit.	• The Mineral Resource has been classified according to the principles of the JORC Code (2012 edition). The resource has been divided into Measured, Indicated, and Inferred categories, corresponding to a high, moderate and low level of confidence in the geological and grade continuity of the resource. The classification integrates several key factors, including: depth of geological knowledge of the deposit, geological and mineralisation continuity, drill hole spacing, and the results of quality control measures. • The classification also considers drill hole logging, analytical results from drill samples, geostatistical analysis, and confidence in geological and grade continuity, along with recent metallurgical/process test outcomes. Additionally, search and interpolation parameters, recently completed density data, and considerations from JORC Code Clause 49 are factored into the classification process. • All relevant factors have been considered and the result reflects Mr Watson's view of the deposit.
AUDITS OR REVIEWS.	• The results of any audits or reviews of Mineral Resource estimates.	• Internal reviews of the Mineral Resource Estimate were conducted and confirmed that the results were robust and aligned with industry standards.
DISCUSSION OF RELATIVE ACCURACY/ CONFIDENCE	• Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the	• The Mineral Resource classification reflects the Competent Person's assessment of the confidence in the distribution of mineralisation and grade variability across the Si2 Deposit on a global basis. • A high degree of confidence is placed in the geological interpretation, supported by the known formation processes of the aeolian dune sands. High SiO_2 grades and strong geological continuity have been observed across the majority of drill holes. A detailed LiDAR survey provides high confidence in the topographic surface, with the base of the resource interpreted from drilling observations (geological & geochemical picks). • The interpreted geology of the Si2 Deposit is considered robust, and alternative interpretations are unlikely to materially impact the Mineral Resource Estimate. • No production data is available for comparison. Estimation was based on interpolation of composited drill hole data within geological domains guided by dune morphology and lithological logging.

CRITERIA	EXPLANATION	COMMENTARY
	factors that could affect the relative accuracy and confidence of the estimate. • The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. • These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	

APPENDIX 2: TABLE OF MATERIAL DRILL HOLES

Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Notes	m	From m	To m	Fe_2O_3 %	TiO_2 %	Al_2O_3 %	LOI %	Total %
AH001	8342968	306235	27.7	0°	-90°	1	2	0.3	2	0.07	0.53	0.12	0.09	100.05
PLT002	8342658	306128	32.7	0°	-90°	1	3.5	0.3	3.5	0.08	0.2	0.08	0.19	99.65
PLT003	8342713	306306	30.8	0°	-90°	1	6	0.3	6	0.04	0.08	0.05	0.08	99.71
PLT004	8342753	306470	28.8	0°	-90°	1	5	0.3	5	0.09	0.25	0.11	0.12	99.8
PLT005	8342691	306640	31.2	0°	-90°	1	4	0.3	4	0.1	0.22	0.06	0.2	99.63
PLT006	8342702	306874	31.2	0°	-90°	1, 2	2							
PLT007	8342825	307012	31.4	0°	-90°	1	2	0.3	2	0.02	0.04	0.04	0.41	99.71
PLT008	8342934	307025	30.9	0°	-90°	1	2	0.3	2	0.03	0.04	0.05	0.08	100.05
PLT009	8343040	307169	31.1	0°	-90°	1	2	0.3	2	0.04	0.07	0.03	0.19	99.67
PLT010	8343190	307275	31.3	0°	-90°	1	2.5	0.3	2.5	0.02	0.03	0.03	0.17	99.7
PLT011A	8343331	307086	33.8	0°	-90°	1, 3	4	0.3	4	0.09	0.17	0.04	0.13	99.62
PLT011B	8343326	307090	33.3	0°	-90°	1	6	0.3	6	0.11	0.22	0.07	0.05	99.5
PLT012	8342909	306693	33.7	0°	-90°	1	5.7	0.3	5.7	0.05	0.09	0.07	0.14	99.44
PLT057	8342503	306740	30.9	0°	-90°	1	2.5	0.3	2.5	0.06	0.15	0.06	0.2	99.7
PLT058	8342398	306945	32.4	0°	-90°	1	2.8	0.3	2.8	0.05	0.11	0.07	0.26	99.78
PLT059	8342263	307090	31.9	0°	-90°	1	1.7	0.3	1.7	0.05	0.13	0.07	0.39	99.77
PLT060	8342196	307299	35.7	0°	-90°	1	5	0.3	5	0.11	0.21	0.1	0.18	99.8
PLT061	8342014	307422	33.5	0°	-90°	1	3	0.3	3	0.06	0.1	0.1	0.11	99.71
PLT062	8341948	307592	37.8	0°	-90°	1	6.7	0.3	6.7	0.05	0.09	0.07	0.14	99.79
PLT063	8341783	307739	38.2	0°	-90°	1	7.5	0.3	7.5	0.1	0.16	0.08	0.16	99.78
PLT064	8341689	307909	39.5	0°	-90°	1	8.5	0.3	8.5	0.03	0.05	0.05	0.14	99.93
PLT065	8341524	308035	46.1	0°	-90°	1	17	0.3	14	0.04	0.08	0.06	0.13	99.99
PLT066	8341340	307874	53.7	0°	-90°	1	23.5	0.3	23.5	0.07	0.11	0.07	0.1	99.99
PLT067	8341466	307691	49.7	0°	-90°	1	19.5	0.3	19.5	0.13	0.22	0.08	0.18	100.06
PLT068	8341199	308033	51.9	0°	-90°	1	32.5	0.3	16	0.06	0.09	0.08	0.09	100.1
PLT069	8341078	307568	74.3	0°	-90°	1	40	0.3	40	0.24	0.33	0.11	0.15	99.95
PLT070	8342335	305852	41.7	0°	-90°	1	10	0.3	10	0.12	0.19	0.08	0.08	99.84
PLT071	8342239	305916	40.6	0°	-90°	1	9.7	0.3	9.7	0.05	0.06	0.05	0.11	99.89
PLT072	8341992	305924	46	0°	-90°	1	15.5	0.3	15.5	0.09	0.14	0.07	0.22	99.82
PLT073	8342028	306133	37	0°	-90°	1	8.5	0.3	8.5	0.06	0.09	0.06	0.07	99.96
PLT074	8341881	306057	41.2	0°	-90°	1	10.8	0.3	10.8	0.13	0.21	0.1	0.11	100.09
PLT075	8341683	306120	41.1	0°	-90°	1	11	0.3	11	0.09	0.15	0.09	0.14	100.02
PLT076	8341551	306266	34.2	0°	-90°	1	4.4	0.3	4.4	0.03	0.05	0.07	0.15	100
PLT077	8341495	306459	36.3	0°	-90°	1	7	0.3	7	0.11	0.19	0.08	0.13	99.77
PLT078	8341360	306596	34.1	0°	-90°	1	6	0.3	6	0.05	0.16	0.06	0.13	99.79
PLT079	8341253	307443	65.7	0°	-90°	1	37	0.3	28	0.19	0.28	0.1	0.1	99.92

Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing	Easting	RL	Azimuth	Dip	Notes		From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
PLT080	8341408	307348	58.2	0°	-90°	1	31	0.3	29	0.09	0.11	0.09	0.06	99.62
PLT081	8341496	307161	56.6	0°	-90°	1, 3	3	0.3	3	0.2	0.35	0.1	0.12	99.7
PLT081A	8341491	307167	57.1	0°	-90°	1	27	0.3	22	0.14	0.19	0.07	0.12	99.84
PLT082	8341625	307014	50.2	0°	-90°	1	22	0.3	22	0.08	0.09	0.08	0.14	99.85
PLT083	8341748	306847	49.4	0°	-90°	1	20.5	0.3	20.5	0.11	0.19	0.07	0.11	99.98
PLT084	8341870	306708	49.1	0°	-90°	1	20	0.3	20	0.06	0.1	0.06	0.14	99.95
PLT085	8342503	306552	30.3	0°	-90°	1	3	0.3	3	0.04	0.04	0.25	0.3	99.54
PLT086	8342301	306544	30.2	0°	-90°	1	3	0.3	3	0.05	0.08	0.1	0.34	99.95
PLT087	8342102	306612	31	0°	-90°	1	3	0.3	3	0.13	0.29	0.12	0.47	100.05
PLT088	8340916	307690	66.6	0°	-90°	1	35	0.3	35	0.13	0.16	0.08	0.13	100.02
PLT089	8340766	307833	58.8	0°	-90°	1	26	0.3	26	0.08	0.11	0.07	0.12	99.96
PLT090	8340691	307998	68.3	0°	-90°	1	30	0.3	30	0.12	0.18	0.08	0.11	99.85
PLT091	8341067	308189	48	0°	-90°	1	26.5	0.3	12	0.17	0.28	0.1	0.09	99.72
PLT092	8340920	308340	45.3	0°	-90°	1	14.5	0.3	8	0.18	0.32	0.11	0.13	99.98
PLT093	8340772	308511	44.8	0°	-90°	1	14.5	0.3	10	0.14	0.24	0.11	0.17	100.13
PLT094	8341354	307052	54.8	0°	-90°	1	26	0.3	26	0.12	0.15	0.08	0.08	99.66
PLT095	8341250	306983	60.3	0°	-90°	1	32	0.3	32	0.12	0.18	0.07	0.15	99.65
PLT096	8341213	306829	54.9	0°	-90°	1	26	0.3	26	0.07	0.11	0.05	0.16	99.72
PLT097	8341133	306930	63.4	0°	-90°	1	35	0.3	35	0.11	0.15	0.07	0.12	99.64
PLT098	8341119	307020	70.5	0°	-90°	1	42.5	0.3	42.5	0.09	0.13	0.06	0.14	99.58
PLT099	8341008	306929	71.1	0°	-90°	1, 3	42	0.3	42	0.08	0.11	0.06	0.08	99.56
PLT100	8341005	307049	68.5	0°	-90°	1	39.5	0.3	39.5	0.11	0.15	0.07	0.09	99.68
PLT101	8340923	306975	66.6	0°	-90°	1	36.5	0.3	36.5	0.08	0.11	0.06	0.1	99.75
PLT102	8340830	307040	58.6	0°	-90°	1	27	0.3	27	0.11	0.18	0.07	0.1	99.72
PLT103	8340756	307115	56.8	0°	-90°	1	25	0.3	25	0.11	0.18	0.06	0.1	99.92
PLT104	8340589	308561	63.3	0°	-90°	1	35	0.3	33	0.1	0.11	0.08	0.12	99.77
PLT105	8340432	308685	49.7	0°	-90°	1	26	0.3	23	0.09	0.16	0.08	0.13	100.07
PLT106	8340399	308891	42.3	0°	-90°	1	14	0.3	14	0.05	0.07	0.08	0.1	99.77
PLT107	8340251	309031	38.7	0°	-90°	1	10.5	0.3	10.5	0.09	0.15	0.09	0.12	99.6
PLT108	8340062	309147	52.2	0°	-90°	1	24	0.3	24	0.12	0.2	0.09	0.07	99.72
PLT109	8339886	309285	67.1	0°	-90°	1	39	0.3	39	0.17	0.25	0.09	0.09	99.7
PLT110	8339786	309472	69.8	0°	-90°	1	42	0.3	42	0.14	0.19	0.09	0.08	99.78
PLT111	8339677	309648	51.2	0°	-90°	1	23.5	0.3	23.5	0.09	0.1	0.08	0.13	99.71
PLT112	8339537	309796	50.1	0°	-90°	1	22	0.3	22	0.08	0.08	0.07	0.13	99.79
PLT113	8339410	309957	41.8	0°	-90°	1	14.5	0.3	14.5	0.1	0.15	0.09	0.08	99.7
PLT114	8339282	310121	44.5	0°	-90°	1	17.5	0.3	17	0.13	0.2	0.11	0.11	99.78
PLT115	8339163	310331	56.2	0°	-90°	1	29	0.3	29	0.24	0.36	0.12	0.1	99.77
PLT116	8339016	310475	48.1	0°	-90°	1	22	0.3	22	0.1	0.14	0.08	0.11	99.84
PLT117	8338868	310614	44	0°	-90°	1	18.5	0.3	18.5	0.13	0.16	0.11	0.1	99.85

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Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing	Easting	RL	Azimuth	Dip	Notes	Depth	From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
PLT118	8338620	310478	53.3	0°	-90°	1	28	0.3	25	0.07	0.06	0.08	0.08	99.72
PLT119	8338746	310316	63	0°	-90°	1	37	0.3	35	0.07	0.07	0.07	0.12	99.72
PLT120	8338882	310170	55.3	0°	-90°	1	29.5	0.3	29.5	0.08	0.11	0.07	0.12	99.81
PLT121	8339029	310024	51.1	0°	-90°	1	25	0.3	25	0.12	0.17	0.09	0.21	99.81
PLT122	8339171	309871	54.5	0°	-90°	1	29	0.3	29	0.08	0.1	0.07	0.12	99.86
PLT123	8339299	309731	56.5	0°	-90°	1	32	0.3	31	0.07	0.09	0.07	0.12	99.87
PLT124	8339449	309604	62.5	0°	-90°	1	40	0.3	40	0.19	0.31	0.11	0.16	99.94
PLT125	8339606	309477	59.1	0°	-90°	1	34	0.3	34	0.07	0.11	0.07	0.1	99.89
PLT126	8339726	309306	68.2	0°	-90°	1	42	0.3	42	0.12	0.17	0.08	0.09	99.97
PLT127	8339622	309236	62.5	0°	-90°	1	30	0.3	29	0.17	0.25	0.08	0.11	100.03
PLT128	8338612	310261	44.8	0°	-90°	1	12	0.3	10	0.06	0.08	0.08	0.13	99.89
PLT129	8338772	310109	59.5	0°	-90°	1	31	0.3	29	0.07	0.09	0.08	0.09	99.93
PLT130	8338278	310236	50.5	0°	-90°	1	21	0.3	18	0.07	0.1	0.1	0.07	99.89
PLT131	8338413	310091	54.9	0°	-90°	1	21	0.3	19	0.1	0.14	0.07	0.09	99.61
PLT132	8338566	309971	59	0°	-90°	1	31	0.3	23	0.12	0.18	0.09	0.08	99.7
PLT133	8338763	309885	63.5	0°	-90°	1	36.8	0.3	29	0.14	0.21	0.11	0.09	99.65
PLT134	8338903	309742	66.7	0°	-90°	1	44.5	0.3	38	0.09	0.11	0.1	0.11	99.62
PLT135	8339045	309590	62.6	0°	-90°	1	33	0.3	29	0.08	0.11	0.11	0.11	99.66
PLT136	8339160	309427	62.7	0°	-90°	1	25	0.3	22	0.05	0.09	0.08	0.11	99.74
PLT137	8339287	309276	57.1	0°	-90°	1, 3	2	0.3	2	0.06	0.2	0.09	0.16	100.25
PLT243	8342658	307200	47.2	0°	-90°	1, 3	9	0.3	9	0.05	0.05	0.06	0.1	99.73
PLT244	8340676	307226	54.8	0°	-90°	1	23	0.3	23	0.06	0.1	0.07	0.1	99.67
PLT245	8340880	307340	61.3	0°	-90°	1	30	0.3	30	0.09	0.12	0.06	0.13	99.75
PLT246	8340772	307531	49.6	0°	-90°	1	17.7	0.3	17.7	0.08	0.13	0.08	0.14	99.8
PLT247	8341060	307196	59.8	0°	-90°	1	33	0.3	32	0.04	0.08	0.07	0.12	99.9
SI20001	8340578	308145	56.9	0°	-90°	1	21	0.3	19	0.17	0.23	0.12	0.08	99.85
SI20002	8340437	308281	58	0°	-90°	1	30	0.3	16	0.13	0.15	0.14	0.12	99.77
SI20003	8340267	308422	56.4	0°	-90°	1	15	0.3	13	0.17	0.19	0.16	0.1	99.8
SI20004	8340152	308572	59.7	0°	-90°	1	28	0.3	19	0.12	0.13	0.11	0.17	99.84
SI20005	8340039	308705	58.4	0°	-90°	1	31	0.3	19	0.11	0.12	0.14	0.21	99.95
SI20006	8339894	308832	52.3	0°	-90°	1	18	0.3	16	0.15	0.2	0.16	0.17	99.95
SI20007	8339714	308948	56.1	0°	-90°	1	21	0.3	12	0.13	0.22	0.12	0.19	99.99
SI20008	8339610	308940	63.3	0°	-90°	1	24	0.3	23	0.14	0.16	0.17	0.23	99.95
SI20009	8339410	309149	64.6	0°	-90°	1	24	0.3	21	0.08	0.13	0.09	0.16	99.96
SI20010	8339299	309268	58.2	0°	-90°	1	21	0.3	16	0.06	0.08	0.1	0.13	99.8
SI20011	8339687	308773	44.4	0°	-90°	1	21	0.3	10	0.06	0.07	0.11	0.15	100.02
SI20012	8339815	308551	59.3	0°	-90°	1	36	0.3	22	0.07	0.12	0.12	0.12	99.94
SI20013	8339940	308175	62.6	0°	-90°	1	30	0.3	30	0.04	0.05	0.08	0.08	99.86
SI20014	8340021	308100	66	0°	-90°	1	39	0.3	36	0.07	0.09	0.07	0.09	99.94

Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Notes	m	From m	To m	Fe_2O_3 %	TiO_2 %	Al_2O_3 %	LOI %	Total %
SI20015	8340179	307848	56.3	0°	-90°	1	30	0.3	30	0.08	0.12	0.14	0.13	99.88
SI20016	8340356	307613	59.3	0°	-90°	1	30	0.3	30	0.11	0.15	0.1	0.13	99.86
SI20017	8340427	307511	61.8	0°	-90°	1	30	0.3	30	0.1	0.17	0.09	0.14	99.82
SI20018	8340566	307373	55.3	0°	-90°	1	27	0.3	27	0.06	0.1	0.09	0.14	99.86
SI20019	8336235	310064	107.4	0°	-90°	1	54	0.3	54	0.19	0.24	0.12	0.17	99.88
SI20020	8336619	309877	99.6	0°	-90°	1	40	0.3	37	0.1	0.11	0.12	0.19	99.94
SI20021	8336915	309662	79	0°	-90°	1	21	0.3	18	0.12	0.16	0.14	0.17	99.91
SI20022	8337162	309350	74	0°	-90°	1	21	0.3	18	0.08	0.11	0.09	0.11	99.9
SI20023	8337451	309132	75.9	0°	-90°	1	36	0.3	31	0.08	0.12	0.14	0.12	99.93
SI20024	8337756	308905	63.8	0°	-90°	1	27	0.3	25	0.11	0.19	0.17	0.2	99.95
SI20025	8338022	308704	74.9	0°	-90°	1	39	0.3	36	0.12	0.2	0.12	0.16	99.95
SI20026	8338229	308519	53.3	0°	-90°	1	21	0.3	18	0.11	0.15	0.13	0.18	100
SI20027	8338466	308283	57.1	0°	-90°	1	27	0.3	27	0.11	0.15	0.1	0.14	99.98
SI20028	8338754	308278	68.5	0°	-90°	1	36	0.3	36	0.09	0.13	0.1	0.13	99.94
SI20029	8338998	308085	51.9	0°	-90°	1	21	0.3	21	0.12	0.2	0.1	0.12	99.97
SI20030	8339382	307940	48.9	0°	-90°	1	18	0.3	18	0.1	0.17	0.09	0.11	99.88
SI20031	8339727	307770	60.7	0°	-90°	1	30	0.3	30	0.08	0.11	0.08	0.17	99.92
SI20032	8339539	308204	50.3	0°	-90°	1	30	0.3	30	0.08	0.12	0.08	0.17	99.85
SI20033	8339245	308496	44.1	0°	-90°	1	9	0.3	5	0.07	0.11	0.08	0.15	99.64
SI20034	8338987	308770	42.3	0°	-90°	1	9	0.3	3	0.09	0.16	0.15	0.19	99.93
SI20035	8338649	309044	62.2	0°	-90°	1	21	0.3	19	0.05	0.06	0.08	0.11	99.98
SI20036	8338378	309266	77.5	0°	-90°	1	34	0.3	33	0.11	0.15	0.09	0.1	99.95
SI20037	8338154	309315	96.3	0°	-90°	1	48	0.3	48	0.11	0.14	0.11	0.18	99.89
SI20038	8337961	309689	67.5	0°	-90°	1	36	0.3	29	0.12	0.18	0.1	0.16	99.84
SI20039	8337728	309931	61.4	0°	-90°	1	21	0.3	19	0.07	0.11	0.1	0.12	99.82
SI20040	8337442	310118	71.7	0°	-90°	1	21	0.3	20	0.18	0.25	0.13	0.15	99.87
SI20041	8337128	310338	78.7	0°	-90°	1	21	0.3	18	0.1	0.15	0.11	0.18	99.92
SI20042	8336831	310528	108.2	0°	-90°	1	51	0.3	49	0.16	0.19	0.11	0.12	99.87
SI20043	8336887	310178	69.8	0°	-90°	1, 2	6							
SI20044	8337151	310050	69.7	0°	-90°	1	9	0.3	7	0.24	0.37	0.13	0.18	99.91
SI20045	8337344	309807	68.2	0°	-90°	1	12	0.3	6	0.16	0.2	0.13	0.16	99.99
SI20046	8337584	309566	75.5	0°	-90°	1	18	0.3	16	0.33	0.49	0.15	0.5	99.77
SI20047	8337817	309357	58.3	0°	-90°	1	9	0.3	6	0.11	0.19	0.13	0.28	99.96
SI20048	8338117	309141	58.2	0°	-90°	1	12	0.3	9	0.08	0.16	0.09	0.2	100.01
SI20049	8337505	309932	61.4	0°	-90°	1	24	0.3	14	0.12	0.15	0.11	0.2	99.98
SI20050	8337744	309606	66.9	0°	-90°	1	18	0.3	15	0.12	0.15	0.14	0.14	99.86
SI20051	8338361	308937	67.2	0°	-90°	1	21	0.3	19	0.14	0.2	0.13	0.16	99.89
SI20052	8338547	308608	60.6	0°	-90°	1	24	0.3	22	0.13	0.21	0.12	0.15	99.88
SI20053	8338149	308189	47.8	0°	-90°	1	18	0.3	16	0.07	0.13	0.12	0.15	99.82

Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Notes	Depth m	Mineralised Interval From m	Mineralised Interval To m	Head Grade Fe_2O_3 %	Head Grade TiO_2 %	Head Grade Al_2O_3 %	Head Grade LOI %	Head Grade Total %
SI20054	8339986	307709	40.4	0°	-90°	1	12	0.3	12	0.05	0.1	0.15	0.23	99.78
SI20055	8339588	308408	34.3	0°	-90°	1	15	0.3	6	0.09	0.18	0.08	0.15	99.93
SI20056	8339043	308921	44.1	0°	-90°	1	21	0.3	17	0.09	0.17	0.13	0.15	99.96
SI20057	8338544	309577	41.8	0°	-90°	1, 2	17							
SI20058	8337965	310117	38	0°	-90°	1, 2	15							
SI20059	8337465	310608	48.1	0°	-90°	1, 2	18							
SI20060	8337676	310388	38.4	0°	-90°	1, 6	15	0.3	15	0.17	0.37	0.64	0.39	99.94
SI20061	8338299	309835	37.7	0°	-90°	1, 2	21							
SI20062	8338820	309305	35.6	0°	-90°	1	18	0.3	16	0.04	0.1	0.12	0.15	99.99
SI20063	8339308	308657	42.1	0°	-90°	1	21	0.3	19	0.09	0.17	0.32	0.71	99.87
SI20064	8339872	308425	49.9	0°	-90°	1	24	0.3	20	0.12	0.21	0.11	0.16	99.91
SI20065	8338040	310505	47.2	0°	-90°	1	21	0.3	13	0.08	0.14	0.11	0.18	99.99
SI20066	8337495	310852	67.7	0°	-90°	1	34	0.3	32	0.12	0.19	0.11	0.16	99.91
SI20067	8337770	310799	46.8	0°	-90°	1	15	0.3	10	0.17	0.31	0.14	0.16	100.06
SI20068	8338469	310389	39.7	0°	-90°	1	12	0.3	7	0.14	0.22	0.12	0.17	100.03
SI20069	8338015	310865	31.9	0°	-90°	1	12	0.3	11	0.05	0.1	0.14	0.28	99.84
SI20070	8337828	311098	30.4	0°	-90°	1, 2	12							
SI20071	8338238	310586	31	0°	-90°	1	15	0.3	9	0.05	0.07	0.11	0.3	99.83
SI20072	8338575	310881	35.2	0°	-90°	1	15	0.3	15	0.1	0.15	0.12	0.11	99.94
SI20073	8338123	311311	43.5	0°	-90°	1	24	0.3	24	0.33	0.47	0.17	0.14	99.89
SI20074	8338352	311101	38.2	0°	-90°	1	18	0.3	18	0.18	0.25	0.15	0.19	99.91
SI20075	8338727	310750	44.1	0°	-90°	1	21	0.3	21	0.17	0.23	0.14	0.14	99.89
SI20076	8341248	307662	46.2	0°	-90°	1	12	0.3	9	0.04	0.08	0.08	0.2	99.84
SI20077	8341375	307834	55.2	0°	-90°	1	27	0.3	26	0.07	0.1	0.08	0.08	99.79
SI20078	8341334	307879	53.5	0°	-90°	1	24	0.3	23	0.07	0.11	0.08	0.03	99.74
SI20079	8341608	308005	39.5	0°	-90°	1	12	0.3	12	0.04	0.07	0.13	0.16	99.56
SI20080	8341399	307996	39.9	0°	-90°	1	12	0.3	12	0.09	0.15	0.12	0.07	99.8
SI20081	8341278	307934	53.7	0°	-90°	1	21	0.3	19	0.07	0.1	0.1	0.05	99.72
SI20082	8341122	308130	44.4	0°	-90°	1	12	0.3	8	0.1	0.16	0.14	0.14	99.73
SI21001	8339979	309213	52.9	0°	-90°		30	0.3	30	0.17	0.2	0.12	0.14	99.99
SI21002	8339831	309383	60.8	0°	-90°		39	0.3	37	0.13	0.16	0.11	0.12	100
SI21003	8339731	309562	60.3	0°	-90°		36	0.3	36	0.14	0.17	0.11	0.17	99.98
SI21004	8339590	309728	51.6	0°	-90°		27	0.3	27	0.08	0.09	0.11	0.19	99.98
SI21005	8339460	309875	50.7	0°	-90°		27	0.3	27	0.08	0.08	0.1	0.15	99.97
SI21006	8339317	310036	48.4	0°	-90°		24	0.3	24	0.12	0.13	0.12	0.15	99.97
SI21007	8339233	310245	44	0°	-90°		21	0.3	19	0.14	0.17	0.13	0.18	99.97
SI21008	8339094	310405	55.5	0°	-90°		33	0.3	33	0.25	0.34	0.14	0.16	99.98
SI21009	8338948	310535	44.5	0°	-90°		24	0.3	24	0.15	0.18	0.12	0.15	99.96
SI21010	8338784	310685	47.5	0°	-90°		30	0.3	29	0.13	0.14	0.13	0.2	99.95

Hole ID	Collar Information: Northing (GDA 2020 Zone 55)	Easting (GDA 2020 Zone 55)	RL (m)	Azimuth	Dip	Notes	Depth (m)	Mineralised Interval: From (m)	To (m)	Head Grade: Fe_2O_3 (%)	TiO_2 (%)	Al_2O_3 (%)	LOI (%)	Total (%)
SI21011	8338651	310818	40.1	0°	-90°		24	0.3	24	0.12	0.13	0.14	0.32	99.98
SI21012	8338525	310962	35.4	0°	-90°		15	0.3	15	0.13	0.14	0.15	0.18	99.98
SI21013	8338672	310392	65.8	0°	-90°		40	0.3	36	0.1	0.09	0.1	0.13	99.98
SI21014	8338826	310239	56.2	0°	-90°		33	0.3	33	0.11	0.13	0.16	0.14	99.98
SI21015	8338932	310086	58.1	0°	-90°		34	0.3	33	0.12	0.14	0.1	0.13	99.98
SI21016	8339096	309940	53	0°	-90°		30	0.3	29	0.14	0.18	0.16	0.17	99.87
SI21017	8339240	309811	56.4	0°	-90°		33	0.3	33	0.09	0.07	0.1	0.15	99.85
SI21018	8339370	309660	59.7	0°	-90°		42	0.3	40	0.09	0.1	0.09	0.13	99.87
SI21019	8339515	309541	58.2	0°	-90°		36	0.3	36	0.08	0.11	0.14	0.16	99.9
SI21020	8339650	309367	60	0°	-90°		36	0.3	36	0.11	0.16	0.09	0.13	99.97
SI21021	8339760	309253	69.3	0°	-90°		45	0.3	45	0.14	0.2	0.09	0.1	100.01
SI21022	8339691	309266	66.8	0°	-90°		42	0.3	39	0.11	0.13	0.08	0.1	99.95
SI21023	8339591	309216	63.3	0°	-90°		33	0.3	28	0.23	0.29	0.17	0.14	99.92
SI21024	8339643	309105	62.4	0°	-90°		27	0.3	24	0.16	0.2	0.12	0.12	99.86
SI21025	8339674	309035	58.8	0°	-90°		21	0.3	20	0.19	0.17	0.13	0.16	99.91
SI21026	8339818	308909	52.4	0°	-90°		15	0.3	13	0.15	0.15	0.11	0.15	99.88
SI21027	8339668	308894	64.2	0°	-90°		24	0.3	23	0.15	0.18	0.11	0.11	99.87
SI21028	8339552	308992	55.2	0°	-90°		30	0.3	15	0.11	0.12	0.13	0.17	99.96
SI21029	8339495	309084	60.3	0°	-90°		21	0.3	16	0.08	0.1	0.11	0.1	99.82
SI21030	8339360	309205	59	0°	-90°		21	0.3	16	0.05	0.06	0.11	0.11	99.86
SI21031	8339223	309323	49	0°	-90°		9	0.3	6	0.07	0.08	0.13	0.14	100.09
SI21032	8339093	309504	55.3	0°	-90°		24	0.3	18	0.07	0.08	0.11	0.1	100.08
SI21033	8338969	309674	59.3	0°	-90°		32	0.3	27	0.07	0.07	0.1	0.11	99.96
SI21034	8338808	309776	61	0°	-90°		30	0.3	30	0.07	0.07	0.11	0.13	99.84
SI21035	8338897	309851	70.5	0°	-90°		45	0.3	42	0.1	0.13	0.15	0.11	99.84
SI21036	8339158	309562	56	0°	-90°		27	0.3	25	0.17	0.28	0.14	0.17	99.69
SI21037	8339224	309498	55.7	0°	-90°		36	0.3	36	0.21	0.24	0.24	0.2	99.81
SI21038	8339305	309438	56.6	0°	-90°		27	0.3	23	0.18	0.27	0.13	0.15	99.88
SI21039	8339386	309386	60.3	0°	-90°		27	0.3	23	0.11	0.14	0.11	0.13	99.86
SI21040	8339452	309303	63.2	0°	-90°		30	0.3	26	0.1	0.14	0.11	0.11	100.02
SI21041	8339512	309259	64.3	0°	-90°		30	0.3	28	0.23	0.33	0.16	0.14	99.96
SI21042	8338756	309887	62.9	0°	-90°		33	0.3	29	0.16	0.22	0.15	0.13	99.86
SI21043	8338846	309829	66.6	0°	-90°		39	0.3	36	0.12	0.17	0.13	0.05	99.9
SI21044	8338660	309909	58.9	0°	-90°		24	0.3	20	0.16	0.26	0.12	0.04	100.06
SI21045	8338489	310044	56.1	0°	-90°		21	0.3	20	0.07	0.1	0.1	0.11	99.94
SI21046	8338336	310171	52.8	0°	-90°		24	0.3	21	0.07	0.09	0.08	0.11	100
SI21047	8338217	310321	49	0°	-90°		15	0.3	13	0.06	0.07	0.09	0.13	99.98
SI21048	8338146	310386	49	0°	-90°		15	0.3	14	0.05	0.06	0.1	0.14	99.91
SI21049	8338099	310439	47.9	0°	-90°		15	0.3	10	0.08	0.13	0.13	0.18	99.94

	Collar Information							Mineralised Interval		Head Grade				
Hole ID	Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Notes	Depth m	From m	To m	Fe_2O_3 %	TiO_2 %	Al_2O_3 %	LOI %	Total %
SI21050	8338869	309942	62.2	0°	-90°		39	0.3	34	0.14	0.22	0.15	0.13	99.78
SI21051	8338673	310174	53.5	0°	-90°		24	0.3	20	0.08	0.11	0.13	0.14	99.89
SI21052	8338533	310327	40.3	0°	-90°		12	0.3	7	0.14	0.15	0.1	0.17	99.71
SI21053	8338390	310455	38.2	0°	-90°		18	0.3	18	0.13	0.14	0.27	0.27	99.8
SI21054	8338324	310529	33.3	0°	-90°		12	0.3	12	0.04	0.08	0.1	0.18	99.8
SI21055	8338577	310556	43.5	0°	-90°		21	0.3	20	0.03	0.06	0.09	0.15	99.73
SI21056	8338516	310650	38.5	0°	-90°		16	0.3	15	0.09	0.15	0.16	0.19	99.87
SI21057	8338450	310720	36.4	0°	-90°		15	0.3	12	0.1	0.15	0.14	0.15	100.24
SI21058	8338406	310764	34.5	0°	-90°		15	0.3	12	0.06	0.1	0.22	0.23	99.9
SI21059	8338236	311235	40.9	0°	-90°		21	0.3	21	0.18	0.19	0.21	0.2	99.76
SI21060	8338109	310272	36.4	0°	-90°	2	12							
SI21061	8338036	310205	38.1	0°	-90°	2	18							
SI21062	8337830	310250	37.3	0°	-90°	4	15	0.3	Excluded	0.07	0.1	0.94	0.74	99.86
SI21063	8337561	310510	47	0°	-90°	2	16							
SI21064	8338092	309981	37.3	0°	-90°	2	15							
SI21065	8338406	309721	39.6	0°	-90°	2	14							
SI21066	8338656	309418	38.1	0°	-90°	2	18							
SI21067	8338951	309137	33.2	0°	-90°		12	0.3	7	0.06	0.1	0.12	0.1	100.3
SI21068	8339158	308966	31.7	0°	-90°		9	0.3	3	0.08	0.14	0.18	0.48	99.75
SI21069	8339209	309117	34.7	0°	-90°	2	14							
SI21070	8339087	309240	33.8	0°	-90°	2	12							
SI21071	8338926	309406	34.9	0°	-90°	2	12							
SI21072	8339428	309014	43.9	0°	-90°		9	0.3	8	0.05	0.06	0.13	0.16	99.78
SI21073	8339307	308981	37.3	0°	-90°		9	0.3	8	0.05	0.07	0.14	0.18	99.9
SI21074	8339415	308835	34.6	0°	-90°		12	0.3	7	0.04	0.08	0.19	0.18	99.87
SI21075	8339516	308716	31.9	0°	-90°		12	0.3	11	0.05	0.1	0.19	0.22	99.84
SI21076	8339450	308535	32.3	0°	-90°		12	0.3	11	0.07	0.13	0.2	0.23	99.85
SI21077	8339192	308783	42.3	0°	-90°		23	0.3	15	0.08	0.14	0.14	0.15	99.95
SI21078	8339080	308633	45.9	0°	-90°		19	0.3	10	0.1	0.09	0.12	0.17	100.03
SI21079	8339386	308370	43.7	0°	-90°		9	0.3	6	0.07	0.09	0.11	0.16	99.98
SI21080	8339651	308002	59.4	0°	-90°		30	0.3	27	0.1	0.13	0.1	0.13	99.82
SI21081	8339574	307851	49.7	0°	-90°		18	0.3	18	0.13	0.21	0.11	0.17	99.83
SI21082	8339444	307858	51.1	0°	-90°		21	0.3	21	0.12	0.17	0.09	0.12	99.81
SI21083	8339206	307991	43.3	0°	-90°		15	0.3	15	0.08	0.1	0.09	0.08	99.82
SI21084	8338858	308178	57.1	0°	-90°		24	0.3	24	0.21	0.31	0.1	0.16	99.76
SI21085	8338615	308194	57.6	0°	-90°		27	0.3	27	0.08	0.11	0.09	0.14	99.89
SI21086	8338361	308383	52.6	0°	-90°		21	0.3	21	0.07	0.11	0.08	0.16	99.93
SI21087	8338160	308619	62.6	0°	-90°		27	0.3	23	0.09	0.13	0.11	0.13	99.79
SI21088	8337859	308773	62.3	0°	-90°		30	0.3	27	0.07	0.12	0.11	0.11	99.78

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Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing	Easting	RL	Azimuth	Dip	Notes		From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
SI220001	8339318	308084	40.7	0°	-90°		12	0.3	12	0.07	0.11	0.12	0.22	99.41
SI220002	8339166	308293	40.4	0°	-90°	2	15							
SI220003	8338973	308474	38.2	0°	-90°	2	15							
SI220004	8338777	308633	40.3	0°	-90°	2	15							
SI220005	8338609	308836	44.3	0°	-90°	2	12							
SI220006	8338468	308983	48.8	0°	-90°		9	0.3	4	0.07	0.1	0.08	0.15	99.33
SI220007	8338405	309170	84.3	0°	-90°		39	0.3	37	0.15	0.18	0.07	0.12	99.67
SI220008	8338323	309232	79.4	0°	-90°		34	0.3	32	0.09	0.09	0.07	0.14	99.43
SI220009	8338050	309348	85.2	0°	-90°		42	0.3	42	0.13	0.15	0.13	0.14	99.63
SI220010	8337920	309457	78.4	0°	-90°		36	0.3	36	0.15	0.18	0.32	0.21	99.67
SI220011	8337643	309751	67.8	0°	-90°		23	0.3	16	0.08	0.07	0.09	0.13	99.37
SI220012	8338099	309451	79.3	0°	-90°		41	0.3	33	0.1	0.11	0.1	0.15	99.39
SI220013	8338051	309572	79	0°	-90°		57	0.3	36	0.12	0.15	0.09	0.15	99.49
SI220014	8337894	309758	70.5	0°	-90°		39	0.3	36	0.18	0.2	0.52	0.34	99.41
SI220015	8337808	309872	64.7	0°	-90°		30	0.3	24	0.13	0.14	0.2	0.18	99.43
SI220016	8337577	310047	55.4	0°	-90°		30	0.3	10	0.08	0.12	0.09	0.16	99.47
SI220017	8337361	310196	65.5	0°	-90°		27	0.3	13	0.31	0.49	0.16	0.19	99.55
SI220018	8337241	310271	66.4	0°	-90°		27	0.3	9	0.18	0.28	0.17	0.15	99.25
SI220019	8336999	310463	71.7	0°	-90°		24	0.3	13	0.21	0.33	0.14	0.12	99.43
SI220020	8337049	310199	72.6	0°	-90°		18	0.3	9	0.12	0.13	0.14	0.15	99.42
SI220021	8337242	309926	67.6	0°	-90°		12	0.3	3	0.21	0.29	0.24	0.2	99.83
SI220022	8337487	309632	73.7	0°	-90°		24	0.3	15	0.27	0.36	0.19	0.16	99.66
SI220023	8337653	309480	77.5	0°	-90°		24	0.3	18	0.17	0.24	0.17	0.16	99.61
SI220024	8337951	309252	54.6	0°	-90°		18	0.3	5	0.14	0.18	0.2	0.19	99.46
SI220025	8338024	309192	53.7	0°	-90°		12	0.3	5	0.08	0.13	0.23	0.4	99.66
SI220026	8338197	309096	64.4	0°	-90°		18	0.3	15	0.08	0.11	0.11	0.18	99.39
SI220027	8338232	309163	69.7	0°	-90°		24	0.3	21	0.08	0.1	0.11	0.14	99.78
SI220028	8338290	309034	70.7	0°	-90°		25	0.3	23	0.15	0.12	0.15	0.21	99.55
SI220029	8338420	308852	64.8	0°	-90°		21	0.3	17	0.17	0.25	0.13	0.13	99.61
SI220030	8338495	308740	60.6	0°	-90°		21	0.3	17	0.11	0.16	0.12	0.13	99.63
SI220031	8338576	308518	56.3	0°	-90°		24	0.3	18	0.09	0.09	0.13	0.15	99.32
SI220032	8338662	308383	58.9	0°	-90°		30	0.3	28	0.08	0.08	0.1	0.2	99.71
SI220033	8338423	308200	44.9	0°	-90°		15	0.3	15	0.13	0.19	0.16	0.17	99.46
SI220034	8338292	308189	48.3	0°	-90°		18	0.3	18	0.11	0.18	0.07	0.15	99.62
SI220035	8338027	308260	42	0°	-90°		15	0.3	9	0.12	0.21	0.07	0.16	99.41
SI220036	8337638	308916	57	0°	-90°		26	0.3	18	0.08	0.11	0.06	0.09	99.49
SI220037	8337514	309002	63.7	0°	-90°		29	0.3	23	0.09	0.13	0.2	0.13	99.6
SI220038	8337218	309270	80.3	0°	-90°		29	0.3	27	0.13	0.16	0.1	0.08	99.58
SI220039	8337085	309487	80.6	0°	-90°		25	0.3	23	0.18	0.22	0.12	0.14	99.7

Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing	Easting	RL	Azimuth	Dip	Notes	Depth	From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
SI220040	8337003	309581	82.1	0°	-90°		24	0.3	23	0.11	0.13	0.12	0.11	99.73
SI220041	8336837	309779	77.1	0°	-90°		15	0.3	14	0.21	0.28	0.12	0.12	99.71
SI220042	8336705	309834	91.2	0°	-90°		32	0.3	32	0.15	0.16	0.15	0.12	99.6
SI220043	8336511	309912	99.7	0°	-90°		39	0.3	38	0.21	0.25	0.14	0.11	99.61
SI220044	8336362	310033	102.7	0°	-90°		45	0.3	43	0.17	0.18	0.12	0.12	99.68
SI220045	8336255	309897	78.5	0°	-90°		25	0.3	21	0.12	0.13	0.1	0.12	99.63
SI220046	8336384	309832	80.5	0°	-90°		27	0.3	24	0.14	0.15	0.09	0.12	99.68
SI220047	8336480	309782	73.4	0°	-90°		15	0.3	12	0.16	0.24	0.08	0.09	99.65
SI220048	8336537	309692	67.2	0°	-90°		21	0.3	7	0.12	0.19	0.11	0.13	100.03
SI220049	8336148	310186	92.1	0°	-90°		37	0.3	30	0.09	0.08	0.1	0.14	99.72
SI220050	8336097	310298	89.6	0°	-90°		29	0.3	27	0.11	0.11	0.11	0.13	99.58
SI220051	8335844	310372	79.9	0°	-90°		12	0.3	9	0.1	0.16	0.09	0.14	99.69
SI220052	8335856	310487	96.4	0°	-90°		26	0.3	25	0.18	0.21	0.12	0.11	99.59
SI220053	8335631	310681	102.7	0°	-90°		34	0.3	30	0.13	0.13	0.13	0.12	99.57
SI220054	8335499	310848	97	0°	-90°		17	0.3	15	0.12	0.08	0.12	0.12	99.5
SI220055	8335342	311025	91.8	0°	-90°	2	6							
SI220056	8335186	311129	105.3	0°	-90°		18	0.3	16	0.14	0.12	0.13	0.17	99.62
SI220057	8335336	311180	86.5	0°	-90°	2	6							
SI220058	8335488	311282	81.4	0°	-90°	2	6							
SI220059	8335670	311292	99.4	0°	-90°		24	0.3	21	0.09	0.12	0.06	0.09	99.7
SI220060	8335844	311127	101.7	0°	-90°		26	0.3	24	0.06	0.08	0.08	0.1	99.65
SI220061	8336009	311028	101.1	0°	-90°		30	0.3	27	0.06	0.07	0.09	0.09	99.69
SI220062	8336165	310905	103	0°	-90°		28	0.3	27	0.07	0.09	0.11	0.07	99.72
SI220063	8336345	310815	101.5	0°	-90°		25	0.3	24	0.11	0.16	0.11	0.18	99.7
SI220064	8336508	310705	95.4	0°	-90°		30	0.3	28	0.08	0.13	0.1	0.1	99.63
SI220065	8336656	310579	101.7	0°	-90°		33	0.3	31	0.11	0.16	0.1	0.13	99.54
SI220066	8336735	310751	82.5	0°	-90°		21	0.3	20	0.13	0.19	0.12	0.09	99.57
SI220067	8336645	310831	78.4	0°	-90°		15	0.3	13	0.11	0.17	0.12	0.08	99.83
SI220068	8337667	309333	63.6	0°	-90°		10	0.3	9	0.1	0.17	0.1	0.16	99.77
SI220069	8337873	308951	57.8	0°	-90°		15	0.3	13	0.09	0.13	0.1	0.91	100.71
SI220070	8337875	308705	70.2	0°	-90°		39	0.3	36	0.06	0.07	0.11	0.14	99.68
SI220071	8337736	308764	55.5	0°	-90°		21	0.3	19	0.09	0.14	0.12	0.1	99.73
SI220072	8337694	308690	44.2	0°	-90°		10	0.3	8	0.06	0.11	0.09	0.08	99.66
SI220073	8337716	308589	47.4	0°	-90°		10	0.3	8	0.07	0.11	0.1	0.06	99.41
SI220074	8337890	308439	45.8	0°	-90°		9	0.3	8	0.09	0.13	0.11	0.14	99.62
SI220075	8338521	309283	54.5	0°	-90°		18	0.3	16	0.07	0.11	0.12	0.16	99.81
SI220076	8338593	309190	54.1	0°	-90°		15	0.3	14	0.08	0.11	0.16	0.15	99.9

Hole ID	Collar Information Northing GDA 2020 Zone 55	Easting GDA 2020 Zone 55	RL m	Azimuth	Dip	Notes	Depth m	Mineralised Interval From m	To m	Head Grade Fe_2O_3 %	TiO_2 %	Al_2O_3 %	LOI %	Total %
SI220077	8338784	308903	51.3	0°	-90°		9	0.3	8	0.06	0.07	0.09	-0.02	99.9
SI220078	8338848	308824	54.8	0°	-90°		18	0.3	15	0.06	0.06	0.1	0.06	99.86
SI220079	8338486	309441	49.3	0°	-90°		12	0.3	10	0.11	0.16	0.16	0.17	99.93
SI220080	8338350	309474	62.4	0°	-90°		30	0.3	27	0.23	0.12	0.12	0.07	99.87
SI220081	8338269	309653	43.6	0°	-90°		6	2	4	0.17	0.26	0.18	0.15	99.8
SI220082	8338130	309791	44.8	0°	-90°		15	0.3	9	0.08	0.13	0.1	0.12	99.66
SI220083	8337991	309892	47.4	0°	-90°		12	0.3	9	0.09	0.14	0.16	0.18	99.69
SI220084	8337835	310018	46.6	0°	-90°		12	0.3	11	0.06	0.11	0.12	0.08	99.61
SI220085	8337754	310074	46.4	0°	-90°		12	0.3	9	0.09	0.14	0.12	0.09	99.71
SI220086	8337838	310249	37.5	0°	-90°	2	9							
SI220087	8337688	310386	37.6	0°	-90°		15	0.3	15	0.05	0.1	0.15	0.13	99.94
SI220088	8337657	310877	47.8	0°	-90°		24	0.3	24	0.08	0.12	0.09	0.15	99.92
SI220089	8337857	310710	46.8	0°	-90°		9	0.3	7	0.09	0.13	0.09	0.11	99.92
SI220090	8337957	310603	48.2	0°	-90°		12	0.3	9	0.06	0.08	0.11	0.21	99.98
SI220091	8337451	310960	65.7	0°	-90°		36	0.3	33	0.18	0.26	0.11	0.09	99.65
SI220092	8337381	311166	53.5	0°	-90°		24	0.3	23	0.1	0.14	0.1	0.14	99.73
SI220093	8337528	311211	37.4	0°	-90°	6	6	0.3	3					
SI220094	8337921	310968	32.5	0°	-90°	2	6							
SI220095	8338800	309865	65.1	0°	-90°		39	0.3	36	0.12	0.15	0.15	0.11	99.72
SI220096	8338754	309357	37.7	0°	-90°		15	0.3	15	0.09	0.2	0.42	0.39	99.74
SI220097	8338159	309307	96.4	0°	-90°		48	0.3	48	0.11	0.13	0.13	0.1	99.77
SI220098	8341223	307482	70.1	0°	-90°		35	0.3	32	0.21	0.34	0.13	0.12	99.81
SI220099	8341307	307393	64	0°	-90°		33	0.3	30	0.14	0.18	0.1	0.12	99.82
SI220100	8341389	307463	54.9	0°	-90°		28	0.3	23	0.08	0.13	0.08	0.15	99.68
SI220101	8341425	307273	52.3	0°	-90°		24	0.3	22	0.13	0.21	0.09	0.16	99.62
SI220102	8341578	307074	49.9	0°	-90°		21	0.3	21	0.08	0.12	0.11	0.18	99.91
SI220103	8341484	307048	48.3	0°	-90°		22	0.3	21	0.13	0.21	0.09	0.14	99.91
SI220104	8341329	307238	43.5	0°	-90°		14	0.3	11	0.06	0.1	0.08	0.11	99.64
SI220105	8341109	307242	52.1	0°	-90°		30	0.3	30	0.1	0.17	0.09	0.12	99.8
SI220106	8341143	307143	54.6	0°	-90°		30	0.3	29	0.06	0.1	0.07	0.12	99.83
SI220107	8341136	307386	71	0°	-90°		45	0.3	45	0.07	0.09	0.11	0.06	99.69
SI220108	8341322	307039	52.3	0°	-90°		26	0.3	24	0.1	0.17	0.07	0.13	99.85
SI220109	8341192	306978	57.9	0°	-90°		33	0.3	31	0.09	0.13	0.06	0.12	99.76
SI220110	8341010	306927	71	0°	-90°		45	0.3	45	0.07	0.1	0.06	0.1	99.86
SI220111	8340846	307027	58.9	0°	-90°		33	0.3	29	0.12	0.19	0.08	0.2	100.06
SI220112	8340717	307163	55.7	0°	-90°		27	0.3	27	0.09	0.14	0.08	0.15	99.88
SI220113	8340212	307727	50.5	0°	-90°		21	2	21	0.07	0.11	0.09	0.16	100.01
SI220114	8340071	307759	49.9	0°	-90°		20	0.3	19	0.09	0.15	0.08	0.12	99.6
SI220115	8339952	307918	49.5	0°	-90°		21	0.3	21	0.11	0.17	0.08	0.13	100.02

	Collar Information								Mineralised Interval		Head Grade				
Hole ID	Northing	Easting	RL	Azimuth	Dip	Notes	Depth	From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
SI220116	8339799	308045	46	0°	-90°		15	0.3	13	0.09	0.16	0.09	0.11	99.95
SI220117	8339874	307734	51.8	0°	-90°		24	0.3	21	0.12	0.19	0.09	0.06	99.81
SI220118	8340085	307959	50.6	0°	-90°		22	0.3	22	0.07	0.08	0.11	0.16	99.86
SI220119	8339958	308131	63	0°	-90°		33	0.3	33	0.06	0.08	0.13	0.22	99.89
SI220120	8339709	308323	35.1	0°	-90°		9	0.3	9	0.1	0.2	0.57	0.31	99.73
SI220121	8339887	308343	54.2	0°	-90°		29	0.3	29	0.08	0.12	0.17	0.17	99.99
SI220122	8339912	308511	66.8	0°	-90°		30	0.3	25	0.07	0.1	0.08	0.14	99.97
SI220123	8339664	308677	37.7	0°	-90°		11	0.3	8	0.07	0.09	0.21	0.16	100.03
SI220124	8339802	308848	47.5	0°	-90°		7	0.3	4	0.14	0.22	0.11	0.12	99.73
SI220125	8339911	308710	44.5	0°	-90°		9	0.3	8	0.1	0.18	0.09	0.19	100
SI220126	8340032	308571	44.1	0°	-90°	2	6							
SI220127	8339971	308762	55.1	0°	-90°		18	0.3	15	0.14	0.19	0.13	0.09	100.08
SI220128	8340104	308637	57.6	0°	-90°		24	0.3	18	0.14	0.11	0.13	0.23	99.94
SI220129	8340221	308473	56.2	0°	-90°		15	0.3	12	0.13	0.14	0.12	0.12	99.35
SI220130	8340368	308353	57	0°	-90°		15	0.3	14	0.11	0.12	0.13	0.2	99.83
SI220131	8340505	308200	55.5	0°	-90°		18	0.3	16	0.1	0.12	0.09	0.22	99.67
SI220132	8340638	308072	59.3	0°	-90°		24	0.3	21	0.13	0.2	0.12	0.14	99.76
SI220133	8340710	307902	64.5	0°	-90°		28	0.3	28	0.07	0.1	0.1	0.14	99.74
SI220134	8340805	307743	61.6	0°	-90°	5	6	0.3	6	0.21	0.37	0.13	0.16	99.55
SI220134A	8340805	307743	61.6	0°	-90°		36	0.3	35	0.12	0.19	0.1	0.1	99.83
SI220135	8340996	307650	66.6	0°	-90°		39	0.3	37	0.09	0.14	0.09	0.08	99.81
SI220136	8341180	307598	57.8	0°	-90°		21	0.3	19	0.09	0.14	0.12	0.13	99.79
SI220137	8341147	307539	67.9	0°	-90°		33	0.3	30	0.16	0.26	0.11	0.17	99.64
SI220138	8340987	307400	45.9	0°	-90°		27	0.3	27	0.05	0.07	0.08	0.17	99.79
SI220139	8340895	307543	39.3	0°	-90°		9	0.3	9	0.07	0.13	0.08	0.15	99.87
SI220140	8340767	307622	41.4	0°	-90°		12	0.3	10	0.07	0.11	0.09	0.2	99.7
SI220141	8340667	307791	41.8	0°	-90°	6	9	0.3	7					
SI220142	8340850	307438	54.8	0°	-90°		27	0.3	27	0.39	0.1	0.09	0.08	99.99
SI220143	8340997	307070	68.9	0°	-90°		42	0.3	42	0.07	0.11	0.07	0.1	99.79
SI220144	8340939	307143	59.6	0°	-90°		33	0.3	31	0.07	0.11	0.06	0.1	99.82
SI220145	8340884	307240	49.5	0°	-90°		21	0.3	21	0.06	0.1	0.12	0.15	99.89
SI220146	8341320	306842	37.5	0°	-90°		12	0.3	12	0.05	0.09	0.09	0.36	100.12
SI220147	8341281	307725	50.4	0°	-90°		15	0.3	14	0.11	0.11	0.1	0.23	99.86
SI220148	8340892	307953	44.1	0°	-90°		9	0.3	7	0.06	0.08	0.07	0.15	100.15
SI220149	8341289	307928	53.6	0°	-90°		20	0.3	18	0.05	0.06	0.07	0.12	99.74
SI220150	8340776	308387	47	0°	-90°		12	0.3	10	0.09	0.12	0.07	0.14	99.92
SI220151	8340519	308622	60.4	0°	-90°		36	0.3	34	0.05	0.05	0.07	0.16	100.02
SI220152	8340075	308907	44.4	0°	-90°		15	0.3	14	0.13	0.12	0.27	0.33	99.86
SI220153	8340363	308572	34.9	0°	-90°	1, 2	3							

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Hole ID	Collar Information							Mineralised Interval		Head Grade				
	Northing	Easting	RL	Azimuth	Dip	Notes	Depth	From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
SI23001H	8336702	309510	65.1	0°	-90°		4.7	0.3	4.7					
SI23013H	8340280	308917	31.4	0°	-90°		3	0.3	3					
SI23065H	8340512	308470	35.6	0°	-90°		3	0.3	2					
SI23066H	8340704	308357	41.9	0°	-90°	1, 2, 7	2							
SI23067H	8340260	308694	35.2	0°	-90°	1, 2, 7	1							
SI23080H	8341004	308005	29.5	0°	-90°		5	0.3	5					
SI23081H	8341042	307964	33.4	0°	-90°		3	0.3	2					
SI23106H	8336824	309552	62.3	0°	-90°		5	0.3	4					
SI23123H	8336882	309830	65.8	0°	-90°		3.2	0.3	3					
SI23124H	8336761	309970	67.1	0°	-90°	1, 2, 7	1.5							
SI23125H	8336621	310083	68.3	0°	-90°		3.4	0.3	3					
SI23129H	8336109	309975	74.6	0°	-90°	1, 3, 7	5	0.3	5					
SI23130H	8335006	310646	78.5	0°	-90°	1, 2, 7	1							
SI23130H_A	8335082	310648	82.3	0°	-90°		5.3	0.3	5.3					
SI2HA0002	8342276	306183	31.9	0°	-90°		3	0.3	3	0.05	0.09	0.11	0.17	99.64
SI2HA0003	8341048	307372	55.6	0°	-90°	1, 3	5	0.3	5	0.18	0.33	0.1	0.21	100.17
SI2HA0004	8340668	307609	40.8	0°	-90°	1, 3	5	0.3	5	0.06	0.12	0.09	0.16	99.87
SI2HA0005	8340076	308415	42.7	0°	-90°	1, 2	5							
SI2HA0006	8340489	307874	35.3	0°	-90°	1, 2	3							
SI2HA0007	8340256	308150	37.3	0°	-90°	1, 2	3							
SI2HA0008	8341095	307854	42.2	0°	-90°		5	0.3	4	0.08	0.17	0.21	0.23	100
SI2HA0009	8340942	308052	33.1	0°	-90°		5	0.3	4	0.02	0.07	0.07	0.27	99.83
SI2HA0010	8340739	308233	41.4	0°	-90°	1, 2, 7	4							
SI2HA0011	8340610	308388	37.3	0°	-90°	1, 2, 7	4							
SI2HA0012	8340632	306914	37.3	0°	-90°		5	0.3	5	0.08	0.16	0.1	0.09	99.96
SI2HA0013	8339375	308842	32.5	0°	-90°		5	0.3	5	0.03	0.09	0.07	0.13	99.77
SI2HA0014	8339858	309116	34.2	0°	-90°		5	0.3	4	0.06	0.11	0.07	0.17	99.19
SI2HA0015	8339388	309409	57.4	0°	-90°	1, 3	5	0.3	5	0.21	0.34	0.11	0.1	99.15
SI2HA0016	8339183	309660	38	0°	-90°	1, 3	5	0.3	5	0.07	0.11	0.08	0.09	99.16
SI2HA0017	8338934	309877	64	0°	-90°	1, 3	5	0.3	5	0.26	0.45	0.11	0.12	99.16
SI2HA0018	8339088	310165	29.1	0°	-90°	1	3	0.3	3	0.07	0.16	0.12	0.1	99.41
SI2HA0019	8338815	310448	30.1	0°	-90°	1	4	0.3	4	0.07	0.13	0.07	0.08	99.32
SI2HA0020	8339232	310443	29.2	0°	-90°	1	2	0.3	2	0.09	0.18	0.1	0.07	99.78
SI2HA0021	8339124	310534	29.9	0°	-90°	1	3	0.3	3	0.14	0.26	0.12	0.09	99.69
SI2HA0022	8339032	310600	28.3	0°	-90°	1	2	0.3	2	0.04	0.07	0.08	0.16	99.59
SI2HA0023	8339368	310180	29.1	0°	-90°	1	2	0.3	2	0.06	0.14	0.08	0.11	99.7
SI2HA0024	8339445	310039	29	0°	-90°	1	2	0.3	2	0.15	0.4	0.12	0.17	100.05
SI2HA0025	8341172	308363	33.6	0°	-90°	1	4	0.3	3	0.16	0.18	0.55	0.58	99.03
SI2HA0026	8341097	308456	33.7	0°	-90°	1	3	0.3	3	0.06	0.12	0.08	0.17	99.59

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Hole ID	Collar Information: Northing (GDA 2020 Zone 55)	Easting (GDA 2020 Zone 55)	RL (m)	Azimuth	Dip	Notes	Depth (m)	Mineralised Interval: From (m)	To (m)	Head Grade: Fe_2O_3 (%)	TiO_2 (%)	Al_2O_3 (%)	LOI (%)	Total (%)
SI2HA0027	8341032	308569	34.2	0°	-90°	1	3	0.3	3	0.1	0.17	0.1	0.13	99.44
SI2HA0028	8340974	308518	32	0°	-90°	1	2	0.3	2	0.07	0.15	0.13	0.1	99.99
SI2HA0029	8341345	308240	33.7	0°	-90°	1	3	0.3	3	0.09	0.19	0.09	0.18	99.9
SI2HA0030	8341255	308289	33.4	0°	-90°	1	3	0.3	3	0.06	0.14	0.07	0.15	99.67
SI2HA0031	8340835	308613	30.5	0°	-90°	1, 7	1	0.3	1					
SI2HA0032	8340748	308702	30.8	0°	-90°	1	2	0.3	2	0.03	0.08	0.05	0.12	99.67
SI2HA0033	8340689	308770	30.8	0°	-90°	1	2	0.3	2	0.04	0.1	0.09	0.07	100.1
SI2HA0034	8340556	308727	48.7	0°	-90°	1, 3	4	0.3	4	0.12	0.22	0.09	0.09	99.86
SI2HA0035	8340585	308862	30.8	0°	-90°	1	2	0.3	2	0.07	0.18	0.08	0.06	99.75
SI2HA0036	8340476	308933	30.1	0°	-90°	1	2	0.3	2	0.09	0.24	0.09	0.11	99.84
SI2HA0037	8340361	309025	30.6	0°	-90°	1	2	0.3	2	0.1	0.27	0.09	0.17	99.94
SI2HA0038	8340269	309118	29.7	0°	-90°	1, 7	1	0.3	1					
SI2HA0039	8340168	309210	30.1	0°	-90°	1	2	0.3	2	0.05	0.12	0.07	0.08	99.98
SI2HA0040	8340054	309310	30.2	0°	-90°	1	2	0.3	2	0.04	0.1	0.05	0.08	99.7
SI2HA0041	8339991	309410	29.7	0°	-90°	1	2	0.3	2	0.05	0.12	0.07	0.19	100.05
SI2HA0042	8339907	309574	30.7	0°	-90°	1	3	0.3	3	0.09	0.2	0.07	0.11	99.85
SI2HA0043	8339818	309677	30	0°	-90°	1	2	0.3	2	0.05	0.14	0.06	0.18	99.68
SI2HA0044	8339698	309791	30	0°	-90°	1	2	0.3	2	0.09	0.22	0.08	0.12	99.63
SI2HA0045	8339576	309916	30.1	0°	-90°	1	2	0.3	2	0.09	0.22	0.09	0.07	100.05
SI2HA0046	8339300	310316	29.6	0°	-90°	1	3	0.3	3	0.14	0.28	0.12	0.11	100
SI2HA0047	8338234	311372	23.6	0°	-90°	1	2	0.3	2	0.04	0.1	0.2	1.07	100
SI2HA0048	8338318	311280	23.9	0°	-90°	1	3	0.3	3	0.04	0.09	0.26	1.56	99.77
SI2HA0049	8338390	311189	25.2	0°	-90°	1	3	0.3	3	0.15	0.27	0.13	0.11	99.47
SI2HA0050	8338463	311115	23.8	0°	-90°	1	2	0.3	2	0.04	0.1	0.08	0.5	99.59
SI2HA0051	8338549	311032	25.3	0°	-90°	1	3	0.3	3	0.55	1.05	0.17	0.13	99.95
SI2HA0052	8338679	310919	26.2	0°	-90°	1	3	0.3	3	0.23	0.42	0.14	0.09	100.05
SI2HA0053	8338816	310811	26.7	0°	-90°	1	2	0.3	2	0.06	0.11	0.08	0.05	99.13
SI2HA0054	8338903	310719	27.5	0°	-90°	1	3	0.3	5	0.14	0.27	0.11	0.12	99.83
SI2HA0055	8338594	310546	44.6	0°	-90°	1, 3	5	0.3	5	0.13	0.22	0.1	0.17	99.88
SI2HA0056	8339574	309625	42.2	0°	-90°	1, 3	5	0.3	5	0.06	0.09	0.07	0.05	99.91
SI2HA0057	8339481	309721	42.9	0°	-90°	1, 3	5	0.3	5	0.14	0.24	0.11	0.09	99.77
SI2HA0058	8339402	309794	41.1	0°	-90°	1, 3	5	0.3	5	0.05	0.08	0.08	0.04	99.64
SI2HA0059	8339335	309875	38.7	0°	-90°	1, 3	5	0.3	5	0.09	0.14	0.08	0.03	99.7
SI2HA0060	8339257	309955	35.5	0°	-90°	1, 3	5	0.3	5	0.06	0.08	0.08	0.06	99.84
SI2HA0061	8339171	310060	30.5	0°	-90°	1	4	0.3	4	0.06	0.11	0.08	0.06	99.84
SI24001	8337921	311584	54.9	0	-90	1	36	0.3	23	0.13	0.31	0.07	0.44	99.51
SI24002	8337796	311887	37.9	0	-90	1	18	0.3	18	0.11	0.21	0.05	0.34	99.57
SI24003	8337599	312111	36.8	0	-90	1	15	0.3	15	0.11	0.14	0.09	0.19	99.67
SI24004	8337424	312352	27.5	0	-90	1	6	0.3	6	0.09	0.14	0.17	0.24	99.42

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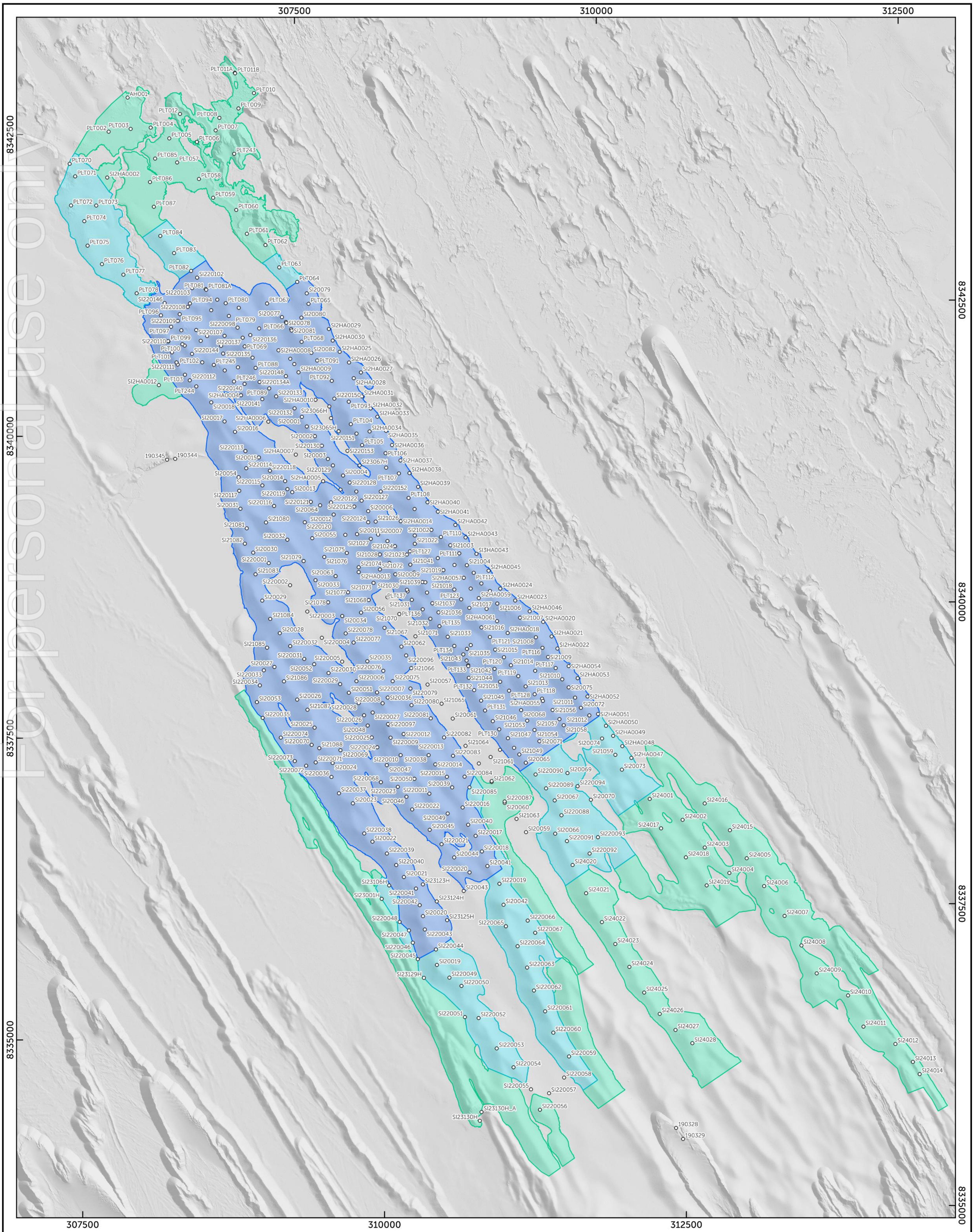
Hole ID	Collar Information						Depth	Mineralised Interval		Head Grade				
	Northing	Easting	RL	Azimuth	Dip	Notes	Depth	From	To	Fe_2O_3	TiO_2	Al_2O_3	LOI	Total
	GDA 2020 Zone 55	GDA 2020 Zone 55	m				m	m	m	%	%	%	%	%
SI24005	8337571	312474	41.9	0	-90	1	24	0.3	24	0.08	0.10	0.08	0.11	99.65
SI24006	8337366	312659	49.8	0	-90	1	30	0.3	5	0.12	0.21	0.08	0.30	99.70
SI24007	8337149	312872	36.2	0	-90	1	18	0.3	7	0.11	0.20	0.06	0.29	99.73
SI24008	8336929	313055	24.6	0	-90	1	6	0.3	6	0.15	0.42	0.07	0.74	99.60
SI24009	8336720	313222	43.5	0	-90	1	27	0.3	9	0.14	0.17	0.04	0.23	99.52
SI24010	8336583	313514	35.4	0	-90	1	21	0.3	5	0.15	0.41	0.06	0.66	99.83
SI24011	8336347	313687	28.1	0	-90	1	20	0.3	12	0.14	0.15	0.11	0.21	99.58
SI24012	8336250	313977	34.8	0	-90	1	27	0.3	14	0.12	0.13	0.12	0.12	99.65
SI24013	8336127	314148	23.7	0	-90	1	18	0.3	16	0.11	0.12	0.09	0.15	99.66
SI24014	8336036	314222	22.1	0	-90	1	18	0.3	18	0.10	0.12	0.07	0.16	99.58
SI24015	8337779	312294	51.5	0	-90	1	33	0.3	33	0.09	0.15	0.05	0.22	99.80
SI24016	8337964	312046	41.7	0	-90	1	24	0.3	21	0.10	0.15	0.04	0.22	99.89
SI24017	8337694	311721	44.4	0	-90	1	24	0.3	6	0.13	0.36	0.11	0.52	99.73
SI24018	8337490	311969	40.1	0	-90	1	21	0.3	21	0.11	0.22	0.10	0.35	99.69
SI24019	8337288	312182	33.3	0	-90	1	12	0.3	12	0.08	0.09	0.05	0.15	99.81
SI24020	8337261	311042	59.6	0	-90	1	27	0.3	34	0.09	0.17	0.06	0.24	99.64
SI24021	8337047	311195	71.3	0	-90	1	36	0.3	24	0.13	0.18	0.11	0.25	99.80
SI24022	8336831	311368	69	0	-90	1	27	0.3	16	0.11	0.11	0.08	0.15	99.64
SI24023	8336669	311511	72.6	0	-90	1	27	0.3	19	0.10	0.09	0.07	0.12	99.80
SI24024	8336500	311661	71.1	0	-90	1	31	0.3	18	0.10	0.09	0.05	0.13	99.62
SI24025	8336309	311821	75.1	0	-90	1	21	0.3	17	0.13	0.08	0.08	0.11	99.40
SI24026	8336155	311981	73.2	0	-90	1	15	0.3	12	0.10	0.08	0.03	0.12	99.76
SI24027	8336045	312135	73.6	0	-90	1	15	0.3	13	0.14	0.17	0.13	0.25	99.38
SI24028	8335960	312294	83.8	0	-90	1	24	0.3	21	0.13	0.15	0.10	0.14	99.77

Notes

1 No Sizing or ICP Data undertaken
2 Drill hole did not intersect significant mineralisation
3 Drill hole is considered open at depth
4 Excluded on quality control grounds, drill hole was later twinned
5 Excluded due to drilling issues
6 Contaminated assay samples, geology suitable for constraining model.
7 Hand auger geology was used to identify mineralised intercept



- Drilling
- Mineral Resource Estimate: Measured Category
- Mineral Resource Estimate: Indicated Category
- Mineral Resource Estimate: Inferred Category

0.5 0 0.5 1 1.5 km

Note: Refer to the Table of Material Drillholes for status of drillhole in Mineral Resource Estimate

Drill Locations

Mineral Resource Estimate (May 2026)

Document #: DRX_NSP_CP_260090	Scale: 1:27500
Version:	CRS: GDA2020 / MGA zone 55
Author: Frazer Watson	Date Created: 12/05/2026
Approved: Frazer Watson	Date Approved: 12/05/2026