Killi Acquires Major WA Iron Ore Project with Substantial Resource and Huge Growth Potential

The project, which is connected to the port by nearby road and rail, generated 69% Fe concentrate in testwork from a resource covering just 20% of the known mineralisation

HIGHLIGHTS

- **Killi Resources has entered into a Share Purchase Agreement to acquire the Lodestone Iron Ore Project, located in the heart of WA's Midwest Iron Ore District**
- **Lodestone is just ~200 km from the Port of Geraldton and is immediately adjacent to grid power and a road and rail network leading directly to the port**
- **The project already hosts an inferred resource of 110Mt at 33% mass recovery (Davis Tube), delivering a 69% Fe concentrate with very low impurities which typically attracts a substantial premium**
- **The current resource base covers ~20% of the known magnetite mineralization, highlighting the potential for significant resource growth**
- **Lodestone hosts a uniquely coarse crystalline magnetite body that extends for 25km; The highly favourable nature of the mineralisation means a high-grade concentrate can be produced using a potentially much cheaper processing route than required at other nearby magnetite operations**
- **Lodestone is being acquired from private interests associated with mining executives Hamish Halliday and Steve Parsons; Following the acquisition, Mr Halliday will join the Killi Board as a Non-Executive Director and Mr Parsons, along with Michael Naylor, will be consultants to the Company**
- **Killi's recently appointed Chairman, Nev Power, who was the long-standing Managing Director of Fortescue Metals Group, brings a wealth of iron ore experience**
- **Killi has received firm commitments for a $15 million (before costs) share placement, giving it a strong cash position of ~$18.5m following completion of the transaction**

Killi Chairman Nev Power said:

"Lodestone is a company-making acquisition which already has a substantial Mineral Resource with clear scope for rapid resource growth and a pathway to production and cashflow.

"Our immediate focus is to grow the resource by drilling out the 25km-long system with rolling campaigns.

"This will enable us to maximise what is a rare opportunity to capitalise on the high-purity, high-value, direct reduction magnetite market with a growing demand driven by the shift to green steel.

"Our growth and development strategy is also underpinned by the highly favourable coarse-grained nature of the deposit, delivering major advantages in capital and operating costs compared with other magnetite projects, and the close proximity to under-utilized infrastructure.

"This combination makes Lodestone a potential development opportunity rarely seen in the iron ore industry".

Killi Resources Limited (ASX: **KLI**) is pleased to announce that it has entered into Share Purchase Agreement to acquire the Lodestone Iron Project in WA's Mid-West region.

Lodestone has the distinct competitive advantage of being located just ~200km from the Port of Geraldton. The Project is surrounded by high quality, existing infrastructure including sealed roads, rail and grid power.

Lodestone's standout ore characteristics can potentially deliver a high-purity, high-quality magnetite concentrate in the range of 68 – 70% Fe achievable at very coarse grind sizes of up to 250 microns. These unique ore characteristics, combined with the high-quality existing infrastructure, point to relatively low capital costs. 68-70% Fe product typically attract a substantial premium which can drive much higher operational margins.

The current Inferred Resource stands at **110Mt at 33 % Davis Tube Recovery ("DTR") Mass Recovery ("MR"), grading 69% Fe in concentrate, at a 0% DTR MR lower cut-off.**

Table 1: Lodestone Iron Project Inferred Resources (Fresh Zone) for key elements by DTR Mass Recovery cut-offs. For more complete tabulation see Table 6.

Class	Lower cut-off DTR Mass Recovery %	Million Tonnes	DTR Mass Recovery %	DTR Concentrate		
				Fe %	SiO_2 %	Al_2O_3 %
Inferred	0	110	33	69	3.9	0.08
	10	110	33	69	3.9	0.08
	20	98	35	69	3.9	0.07
	30	77	38	69	3.4	0.05

Grades and tonnages rounded to 2 significant figures

Overview of the Lodestone Iron Ore Project

The Lodestone Iron Project is located in the Mid-West region of Western Australia, east of the wheatbelt town of Morawa, between the Karara (Ansteel - active) and Koolanooka (Baowu - inactive) iron ore mines (Figures 1 and 2).

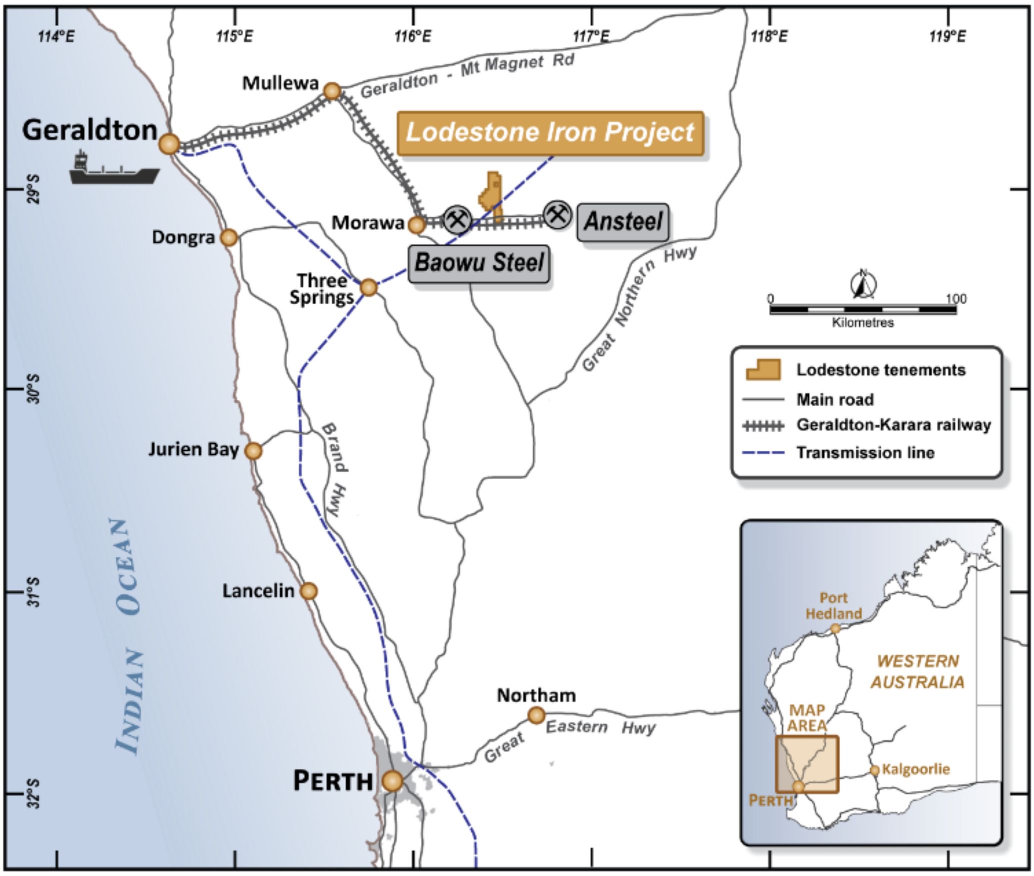

Figure 1: Lodestone Iron Project – **Located in the heart of the Mid-West Iron Ore District**

Access to the southern end of the Project is via the Mungada Road, which parallels the rail line connecting the Karara iron ore mine with Geraldton. The Lodestone resource area can be readily accessed by numerous station tracks leading from the Mungada Road

The Lodestone magnetite body is entirely covered by granted Exploration Licence 59/2163-I, granted to Yukon Resources Pty Ltd on 13 May 2020. The Lodestone Project also includes Exploration Licence application 59/3072 (Figure 2).

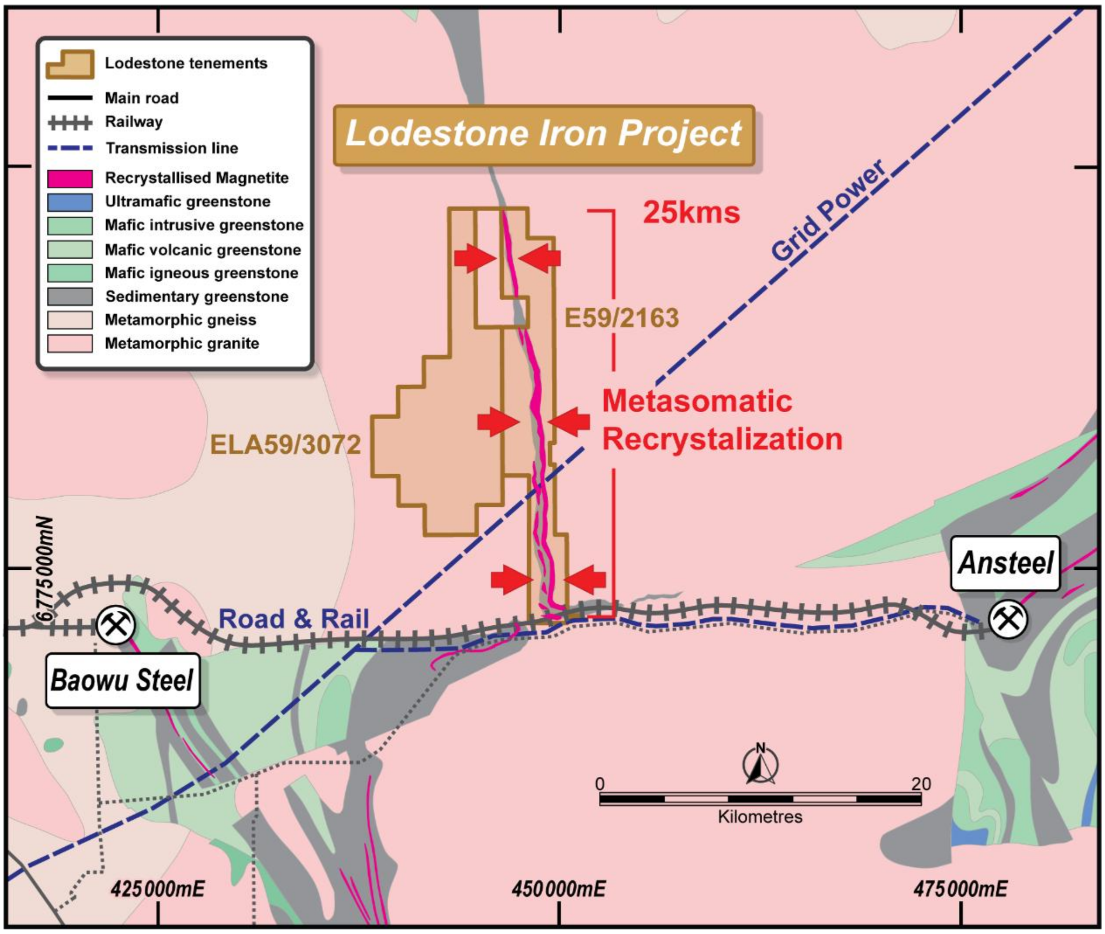

Figure 2: Tenure Summary – Adjacent to high quality existing infrastructure

Acquisition Terms

In accordance with the terms of the Agreement summarised below, Killi has agreed to acquire 80% of the issued capital of Yukon Resources Pty Ltd (ACN 609 082 591) (**Yukon**), the holder of the Lodestone Iron Ore Project.

Consideration

The consideration payable by Killi to the Vendors for the Acquisition comprises:

(a) 92,727,273 fully paid ordinary shares in Killi (**Consideration Shares**), having a total value of $20,400,000 based on a deemed issue price of $0.22 per share; and

(b) a 2.5% gross revenue royalty over all production from the Project.

Joint Venture

Following completion, the parties will form an incorporated joint venture on the following terms:

(a) Killi holding an 80% interest and the Vendors holding a 20% interest;

(b) the Vendors will be free carried until final investment decision;

(c) Killi will be the manager of the joint venture and will have sole discretion over all exploration and development activities during the free carry period; and

(d) following the free carry period, the parties must each fund expenditure on a pro-rata basis in proportion to their respective ownership interest in the Joint Venture (or have their interest diluted).

Vendors

The shareholders of Yukon (**Vendors**) comprise Steve Parsons and his related entities (holding 45% of Yukon), Hamish Halliday and his related entities (holding 45% of Yukon) and Karen McLean and her related entities (holding 10% of Yukon).

The Consideration Shares will be issued to the Vendors on completion subject to shareholder approval under ASX Listing Rule 7.1.

Consultant Performance Rights

The Company intends to engage two of the Vendors (Steve Parsons and Hamish Halliday) as consultants and subject to shareholder approval at the EGM, issue a total of 43,000,000 Performance Rights (**Consultant Performance Rights**) in return for consultancy services. The Consultant Performance Rights will have an expiry of 5 years from the date of issue subject to the following milestones:

Table 2: Performance Rights Milestones

Number of Performance Rights	Milestones
7,666,667	KLI Shares achieving a 20-day VWAP of $0.44 or higher and KLI announcing that it has completed at least 20,000 meters of drilling at the Project.
7,666,667	KLI announcing a Mineral Resource Estimate of 200Mt at greater than or equal to 25% mass recovery.
7,666,666	KLI announcing a positive economic study (being a scoping study, Preliminary Feasibility Study or Definitive Feasibility Study) for the Project which demonstrates, on the base-case assumptions, a positive Net Present Value and a positive Internal Rate of Return.
20,000,000	KLI announcing a Definitive Feasibility Study for the Project which demonstrates, on the DFS base-case assumptions, a positive Net Present Value and a positive Internal Rate of Return.

Conditions Precedent

Completion of the Acquisition is subject to the satisfaction or waiver of certain conditions precedent, the material of which include:

(a) the parties having obtained all approvals, consents or waivers of a third party which are necessary to implement the Acquisition;

(b) Killi receiving shareholder approval under ASX Listing Rule 7.1 to issue the Consideration Shares and the Tranche 2 Placement Shares; and

(c) the representations and warranties of each party remaining true and correct in all material respects at completion, and fulfilment of all pre-completion obligations,

(together, the **Conditions Precedent**).

If any of the Conditions Precedent are not satisfied or waived on or before 5:00pm (WST) on 8 September 2026 (3 months from execution date), Killi may terminate the Agreement by written notice to the Vendors.

The Agreement otherwise contains terms and conditions considered standard for agreements of this nature.

Placement

Killi has received firm commitments to raise $15 million (before costs) via a two-tranche placement (**Placement**). Under the Placement, the Company expects to issue a total of up to 68,181,818 new fully paid ordinary shares (**Placement Shares**) at $0.22 per share to high-quality existing and new institutional and sophisticated investors.

The Placement comprises:

- **Tranche 1**: the raising of approximately $10.8 million (before costs) via the issue of up to 49,073,583 Placement Shares (**Tranche 1 Placement Shares**), utilising the Company's available placement capacity pursuant to ASX Listing Rules 7.1 and 7.1A; and
- **Tranche 2**: the raising of approximately $4.2 million (before costs) via the issue of up to 19,108,235 Placement Shares (**Tranche 2 Placement Shares**), subject to shareholder approval which is to be sought at an extraordinary general meeting (**EGM**) expected to be held during July 2026. Directors of the Company will participate for up to a total of $200,000 (subject to shareholder approvals), which will settle in Tranche 2.

The offer price of $0.22 per Placement Share represents:

- a discount of 6.4% to Killi's last closing price of $0.235 on 23 April 2026; and
- a discount of 4.5% to Killi's 5-day volume weighted average price ("VWAP") of Shares ($0.215).

Proceeds from the Placement will be applied towards:

- exploration and development at the Lodestone Iron Ore Project, including infill and extensional drilling, metallurgical test work, engineering studies and environmental approvals;
- continued exploration and development at the Company's existing projects, including drilling programs at the Mt Rawdon West Project, regional exploration at Ravenswood North, and the West Tanami Project;
- costs associated with the Acquisition (including repayment of Yukon shareholder loans) and the Placement; and
- corporate costs and general working capital.

The Placement is not conditional on the Acquisition completing. Accordingly, if the Acquisition does not complete, the Company will use all funds raised from the Placement towards exploration activities at its existing projects and future value-accretive acquisition opportunities.

The Placement is not underwritten, and Tranche 2 (including the Director participation) is subject to shareholder approvals at the EGM.

Killi is expected to resume trading on the ASX from market open today, 11 June 2026. The Tranche 1 Placement Shares are expected to settle on 17 June 2026 and be issued on 18 June 2026, Placement Shares will rank equally with the Company's existing fully paid ordinary shares on issue.

Details of the time and venue for the EGM will be provided in a notice of meeting to be despatched to shareholders in due course.

Canaccord Genuity (Australia) Limited is acting as Sole Lead Manager and Sole Bookrunner to the Placement, with Argonaut Securities Pty Ltd acting as Co-Lead Manager to the Placement. Hamilton Locke is acting as Killi's legal counsel on the Acquisition and Placement.

Indicative Timetable

An indicative timetable of key dates is detailed below:

Table 3: Indicateive Timetable

Event	Date
Announcement of the Acquisition and Placement **Trading suspension lifted**	Thursday, 11 June 2026
Settlement of Tranche 1 Placement Shares	Wednesday, 17 June 2026
Issue and application for quotation of Tranche 1 Placement Shares	Thursday, 18 June 2026
Notice of EGM dispatched to shareholders	Late July 2026

EGM to approve the issue of Tranche 2 Placement Shares	Late July 2026
Settlement of Tranche 2 Placement Shares	Late July 2026
Issue and application for quotation of Tranche 2 Placement Shares and Completion of Acquisition.	Late July 2026

The dates in this announcement are indicative only and the Company reserves the right to vary the timetable at any time before the issue of the relevant securities without notice, subject to the ASX Listing Rules and the Corporations Act and other applicable laws. The commencement of trading and quotation of the Placement Shares is subject to ASX confirmation. The Company gives no assurance that such quotation will be granted. Nothing contained in this announcement constitutes investment, legal, tax or other advice. Investors should seek appropriate professional advice before making any investment decision. All amounts are in Australian dollars unless otherwise indicated.

Effect on Capital Structure

The indicative effect of the Acquisition and Placement on Killi's capital structure is set out below:

Table 4: Indicative capital structure post Acquisiton and Placement

Capital Structure	Shares	%	Options	Performance Rights
Existing securities	197,994,339	55.2	5,956,611	2,360,000
Consideration Shares	92,727,273	25.8	-	-
Consultant Performance Rights	-	-	-	43,000,000
Placement Shares	68,181,818	19.0	-	-
Total	**358,903,430**	**100.00**	5,956,611	**45,360,000**

Notes:

1. The Tranche 2 Placement Shares and Consideration Shares are subject to shareholder approval at the upcoming EGM.
2. 43,000,000 Consultant Performance Rights to be issued to Stephen Parsons and Hamish Halliday in connection with consultancy services, subject to shareholder approval at the upcoming EGM. Further details of the Consultant Performance Rights will be set out in the Notice of Meeting to be circulated to shareholders in due course.

Board Changes

In connection with the Acquisition, Mr Hamish Halliday has joined the Board as a Non-Executive Director, effective today. Mr Halliday is a geologist with 30 years of corporate and technical experience, having been involved in the discovery and funding of multiple, large scale, mineral projects across five continents. Mr Halliday has founded or co-founded a number of successful junior mining companies and has held numerous executive and non-executive roles in the mining industry since 2001.

Geology, Geological Interpretation and Mineralisation

Iron ore was identified in the area in the 1960's, with the Koolanooka mine being the source of Australian's first iron ore shipment to Japan in 1966.

Archaean basement within E59/2163-I is largely covered by shallow alluvium with colluvial fans of ironstone and pisolitic gravel emanating from the central Lodestone BIF ridges. The southeastern edge of the E59/2163-I is partly covered with lacustrine and aeolian deposits associated with Lake Weelhambye which is part of an extensive palaeochannel system west and south of the tenement. Granite and granitic gneiss are widely exposed to the east of the Lodestone BIF ridges.

Approximately 12 km of the Lodestone BIF is exposed and magnetic imagery indicates an essentially continuous 25 km of BIF horizon extending the length of E59/2163-I. The Lodestone BIF dips about 50-60° west and comprises an eastern unit (up to ~80 m true thickness) flanked by narrower BIF lenses (~10 m thickness) in both hanging and foot walls, and a poorly defined (largely unexposed and sparsely drilled) western BIF unit (~40 m thickness) located 150-200 m west of the eastern BIF zone. The western BIF unit is not exposed. The Lodestone BIF units are flanked and interleaved with magnetite and biotite amphibolites, shale, granitic and pegmatite dykes, minor felsic and ultramafic schists, and in the north a lenticular sheared sulfide-rich horizon which has been lightly previously explored for base metal sulfides deposits.

The Lodestone BIF is conspicuously coarsely metamorphically recrystallised, especially in the central and southern part of the tenure, comprising laminated to banded medium to coarse grained (1-5 mm) grained magnetite and quartz, with minor amphibole. Small scale (to few metres) tight to isoclinal folding of bedding is widespread. At surface the magnetite is partly to largely oxidised to haematite, limonite and goethite, and wall rocks are variably weathered to clay saprolite. Drilling indicates weathering extends to 10-30 m beneath the BIF ridge crest, and up to ~70 m depth in areas that have minor alluvial cover.

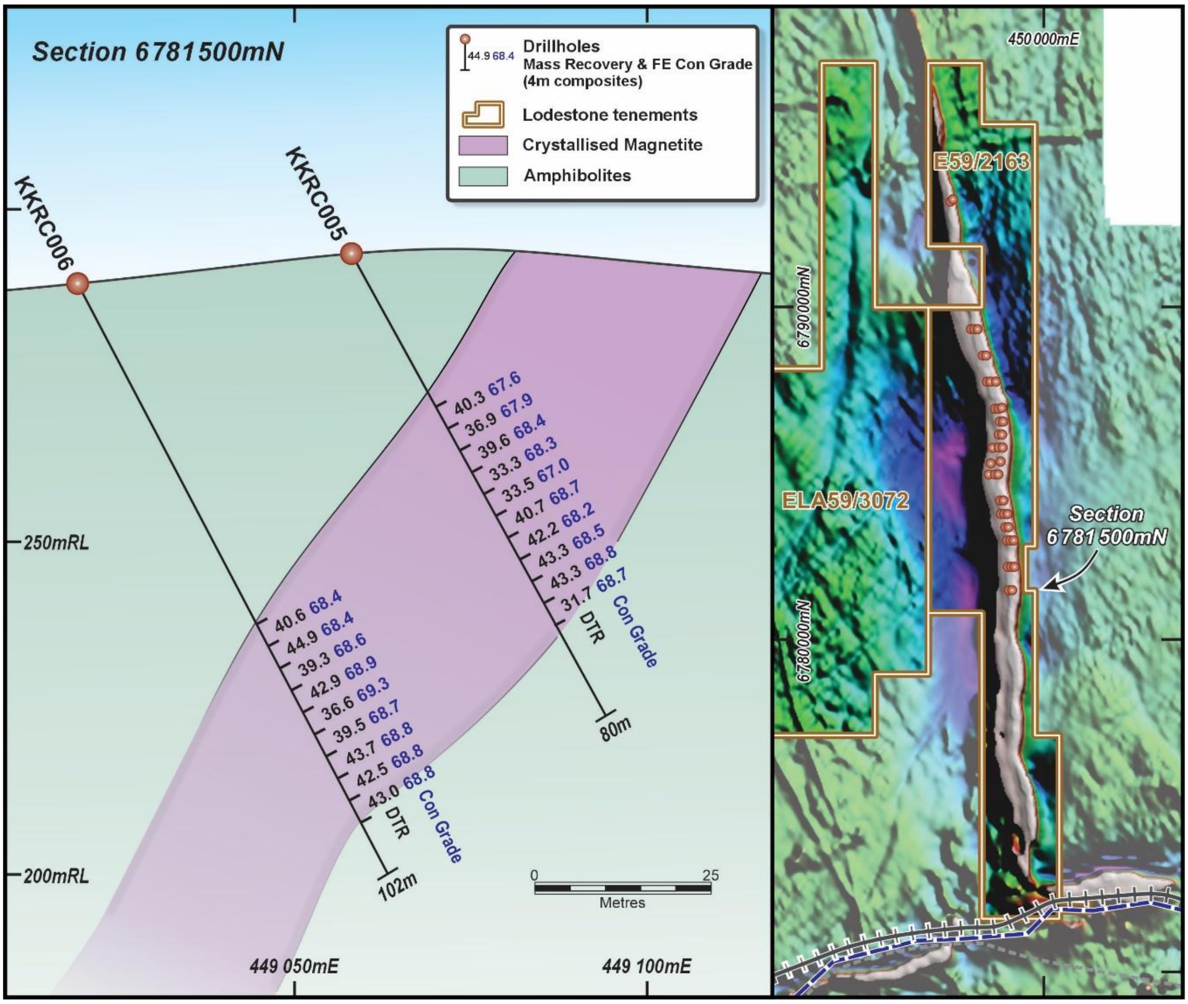

Figure 3: Representative Drill Hole Cross Section- annotated with DTR Mass Recovery and Fe % concentrate grade, from (4m composites samples. Image on the right is an aeromagnetic image annotated with tenements and drill hole collar locations.

Drilling, Sampling and Sub-Sampling Techniques

Drilling within the Lodestone Project includes 40 reverse circulation ("RC") drill holes totalling 5,023 metres, drilled across three campaigns (2012, 2021, and 2023–24) (Figure 4, Tables 5 and 7).

All drilling was undertaken by Reverse Circulation (RC), using 4.5 and 5 inch face sampling hammer. Some 38 holes were drilled on fifteen east-west traverses situated approximately 400 and 800 metres apart and covering approximately 8 km strike of the eastern magnetite BIF unit. A further three holes were drilled to explore the alluvial covered western magnetite BIF unit. Drill hole collars were located in MGA Zone 50 GDA94 coordinates by handheld Garmin GPS with better than 5 metre precision.

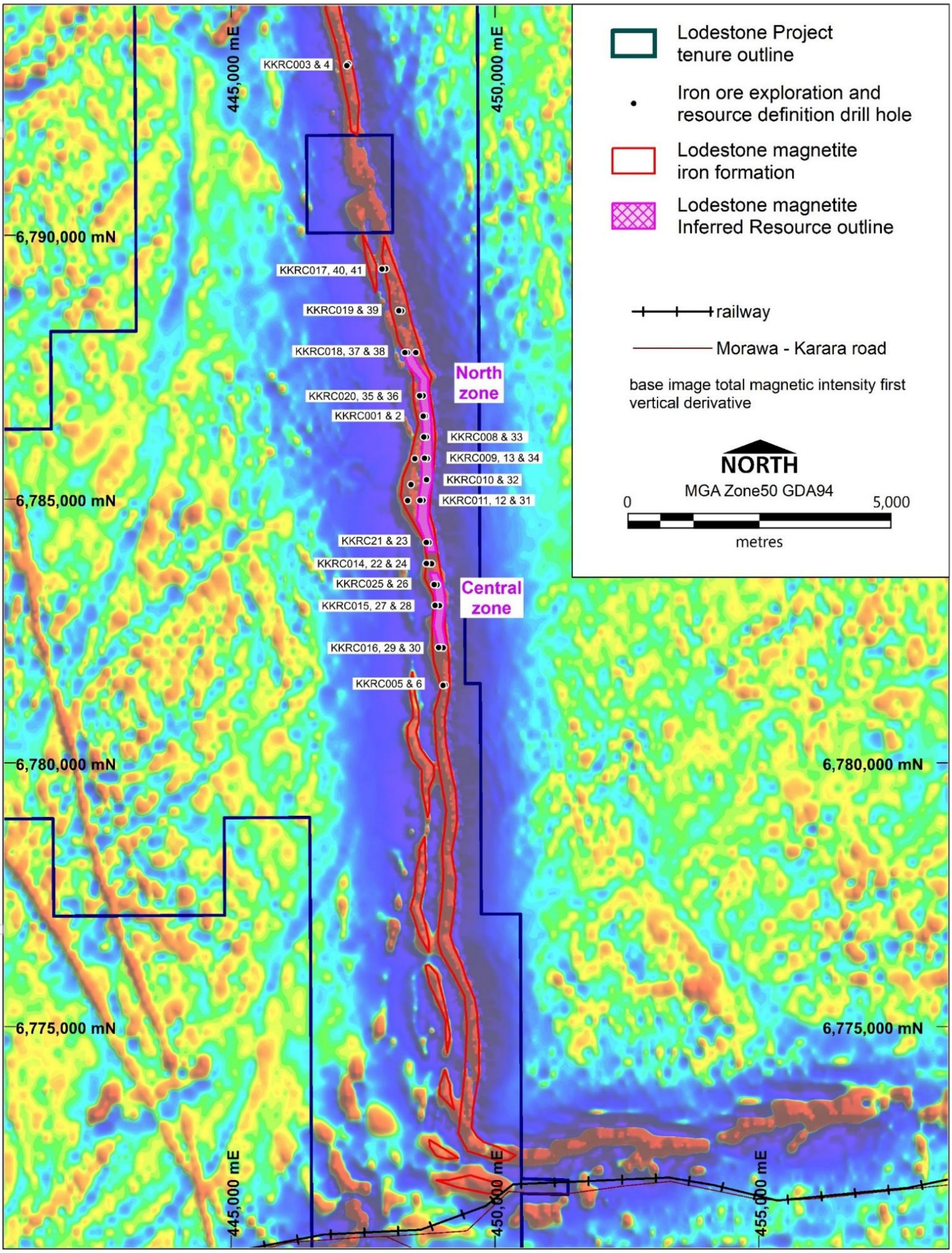

Figure 4: Lodestone Project drill hole collars, Mineral Resource Estimate outline and defined magnetite mineralisation trend, over Reduced to Pole, Total Magnetic Intensity image.

Holes KKRC008 to KKRC041 were down hole surveyed using a north seeking gyroscope hired and operated by the drilling contractors. Significant (>10 degrees) magnetic interference is apparent proximal to the target BIF units and the north seeking gyroscope was also used to line the drill rig up on the planned azimuths.

Bulk one (1) metre RC chip samples were collected from drill rig cyclone and subsampled via a rig-mounted splitter to produce 2–5 kg splits per metre for direct submission.

Four (4) metre composite samples were used for grade estimation. The 4m composite samples were collected via cone and quarter compositing, for submission to ALS Metallurgy and Geochemistry in Perth for Davis Tube Recovery ("DTR") test work and X-ray fluorescence ("XRF") fusion assay. Assay results are provided in Tables 8 and 9.

Table 5: Lodestone Iron Project drilling summary

Company	Holes	Number of holes	Drilled metres	max hole depth m	Drill Co	Drill rig	Period
Black Peak Holdings	KKRC001 to KKRC006*	6	616	140	K & J Drilling	track mounted RC rig 350psi/1200cfm	May - June 2012
Yukon Resources	KKRC008 to KKRC020	13	1211	102	Westside Drilling	MK10 Atlas Copco rig with an onboard 350psi/900cfm compressor, 12 rod carousel and rig mounted cyclone and cone splitter	October 2021
Yukon Resources	KKRC021 to KKRC041	21	3196	192	KTE Drilling	Schramm 450 mounted on an 8x8 Mercedes truck with on board 350psi/1200cfm air compressor and an auxiliary truck mounted air pack (total air capacity nominally 700psi/1800cfm)	December 2023 - January 2024
Total	KKRC001 to KKRC041	41	5023				

Note: KKRC007 is approximately 9 km outside of the current Lodestone Iron Project area and not relevant to the MRE

The initial MRE reported here relates to approximately 5 km strike section of the eastern magnetite BIF unit that is largely covered by 400 metres section lines, and is underpinned by 25 RC holes totalling 3,112 metres (Figure 4). All drill holes were inclined at -60 degrees to the east (BIF units dip west), average hole length was 124 m, with a maximum length of 180 m (example cross-sections provided in Figures 5 and 6).

Metallurgical Test Work and Grade Determination

Davis Tube Recovery ("DTR") test work was the primary analytical technique, with a total of 315 composite samples submitted from drilling within the Project. Orientation test work at grind sizes from 25 to 600 microns established that a 75-micron grind size is appropriate for the initial MRE. The majority of samples (196 of 272) were tested at 75 microns, with 76 samples tested at 150 microns and corrected to 75-micron equivalents via regression.

Within the MRE, a total of 238 DTR assays were modelled.

Key results from metallurgical testwork completed to date are summarised below:

- Concentrate Fe grades consistently exceed 65% at a 75-micron grind, with the southern Central zone returning grades exceeding 70% Fe at coarser grinds, reflecting increasing magnetite grain size.
- Bond Work Index (BWI) bulk sample test work (approximately 30 kg composites) confirmed DTR results, with mass recoveries of 30–36% and concentrate Fe grades of 66.6–69.3% Fe at a 106-micron grind.

- Silica is the only significant concentrate impurity. Al_2O_3 (<0.2%), S, P and Mn are negligible.
- A strong correlation between magnetic susceptibility and DTR mass recovery (R^2 = 0.90) was used to estimate DTR parameters for the 8% of intervals without direct DTR test results.

Drilling Data QA/QC

The resource estimation was based on the available exploration drillhole database which was compiled in-house. The database has been reviewed and validated prior to commencing the resource estimation study. Checks made to the database prior to use included:

- Check for overlapping intervals.
- Downhole surveys at 0 m depth.
- Consistency of depths between different data tables.
- Check gaps in the data.
- Replacing less than detection samples with half detection.
- Replacing intervals with no sample or assays not received with numerical blanks.

All drilling included in the mineral resource estimate (MRE) have been drilled since 2012 by Reverse Circulation (RC) drilling. Surface trench samples which were used to guide the interpretation have been excluded from the estimation. RAB drilling was used for modelling of oxidation depths only, and did not have suitable Fe or DTR assay data and were excluded from the estimation.

DTR test work and associated assaying was conducted by ALS Metallurgy and associated assaying by ALS Geochemistry, Perth.

- DTR QC (duplicate analysis) demonstrated Half Relative Differences (HRD) of <10% for all key parameters (DTR mass recovery, feed Fe, concentrate Fe and Si).
- DTR concentrate impurity elements Al, Mg, Ca, Na, K, Ti, P, S, and Mn are below the grade range of interest and the elevated (>10%) HRDs for these elements are significantly impacted by proximity to elemental detection limits for methods XRF12 and XRF21u.
- Internal ALS standards and duplicates reported within the target ranges.
- Three composites of c. 30 kg each were produced from the bulk 1 m RC bags and submitted to ALS Metallurgy, Perth for Bond Work Index (BWI) and DTR test work and represent a useful verification of the downhole DTR data used in the resource estimate. The BWI test work DTRs were conducted at a 106 µm grind and show 30-36% magnetic recovery at 3000 gauss and a concentrate grade of 66.6 to 69.3% Fe, 3.3 to 6.8% SiO2, <0.2% Al2O3 and -3.06 to -3.12% LOI at 1000° C. DTR test work on the BWI samples was conducted at a 106 micron grind and is therefore not directly comparable with the resource DTR work which was levelled to the dominant (73% of data set) 75 micron grind. However, the results are substantially comparable, and where deviation of >10% occurs it is in accordance with the relationship whereby lower mass recovery and higher grade concentrates are obtained at finer grind size.

Resource Classification and Methodology

Mineralisation envelops were interpreted from drilling and constructed as three-dimensional wireframes in Micromine software.

Mineralisation was defined on the basis of DTR testwork and magnetic susceptibility. Grade estimation was performed using Inverse Distance Squared (IDW2) with hard domain boundaries interpreted between the Fresh (FR) and Partly Oxidised (POX) zones.

Fresh zone BIF mineralisation ("Primary Material") has been classified as Inferred based on:

- Outcrop continuity and simple BIF geometry providing high structural confidence across most of the strike.
- Continuous magnetic anomaly between drill sections confirming BIF strike continuity.
- At least two RC drill holes per section through the BIF, with sections spaced no greater than approximately 400m apart.

The Partly Oxidised Zone (POX) does not form part of the Mineral Resource estimate due to insufficient sample support, variable recovery and limited drill piercement of the weathering profile. It is not included in JORC resource reporting.

The Inferred classification is supported by drill sections spaced approximately 400 m apart, with 1–3 (typically 2) RC holes per section, across approximately 5.5 km strike length of the resource area (Figure 4). The Inferred Mineral Resource includes material estimated by interpolation on mainly 400m section spacing with extrapolation to industry typical half section spacing or clipping to the end sections as considered most geologically reasonable. Approx 20% of the MRE is extrapolated beyond the dominant 400 m drill section spacing. Drilling and geological modelling indicates continuity of the iron formation beyond the MRE end sections which is expected to be upgraded to resource status with further drilling and metallurgical testwork.

A diagrammatic representation of the Inferred Mineral Resource identifying the extrapolated portions is included in Figure 4 and cross sections below in Figures 5 and 6.

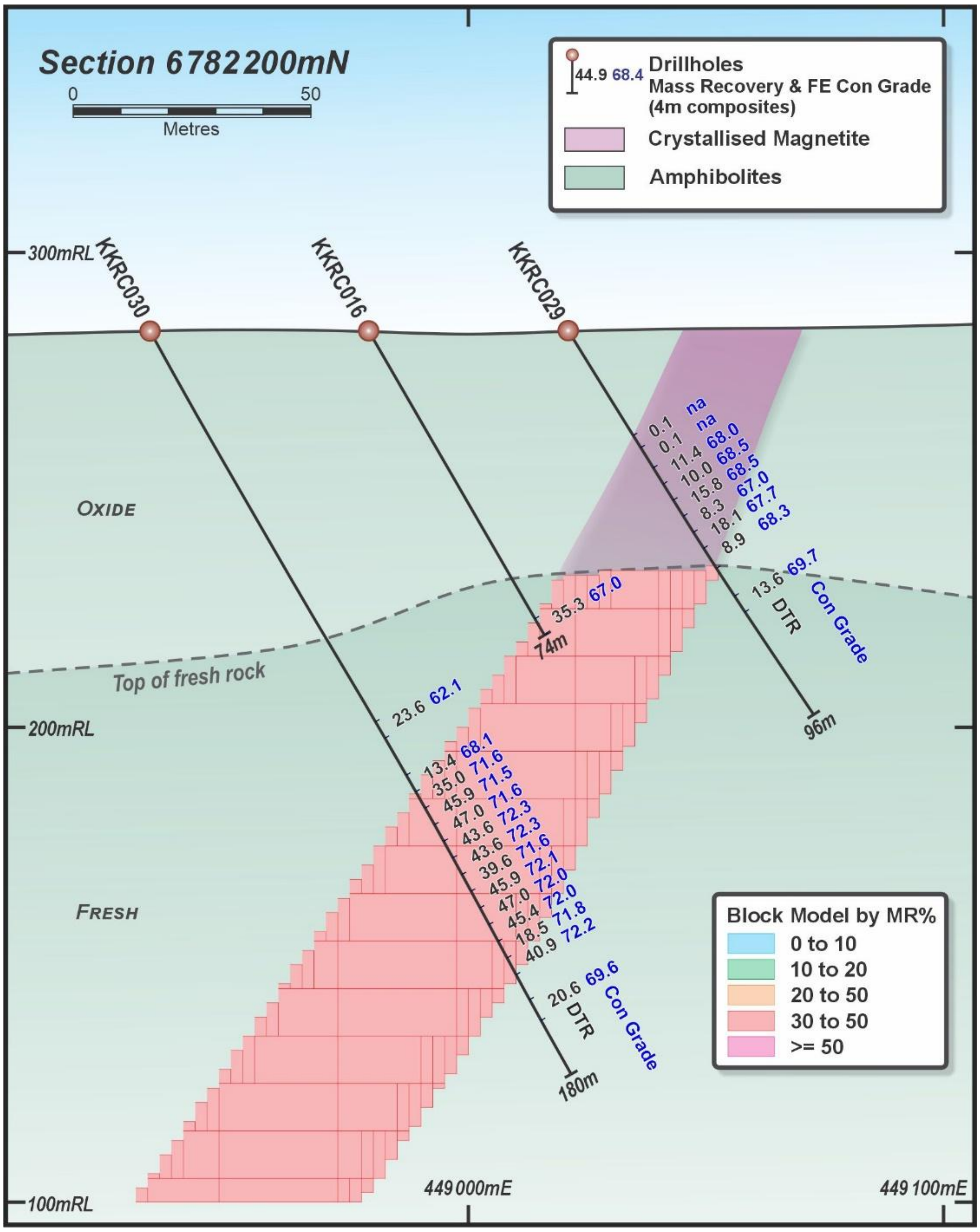

Figure 5: Interpreted drill hole cross-section with block model. Drill traces labelled with DTR Mass Recovery (MR%) and Fe% grade in DTR concentrate.

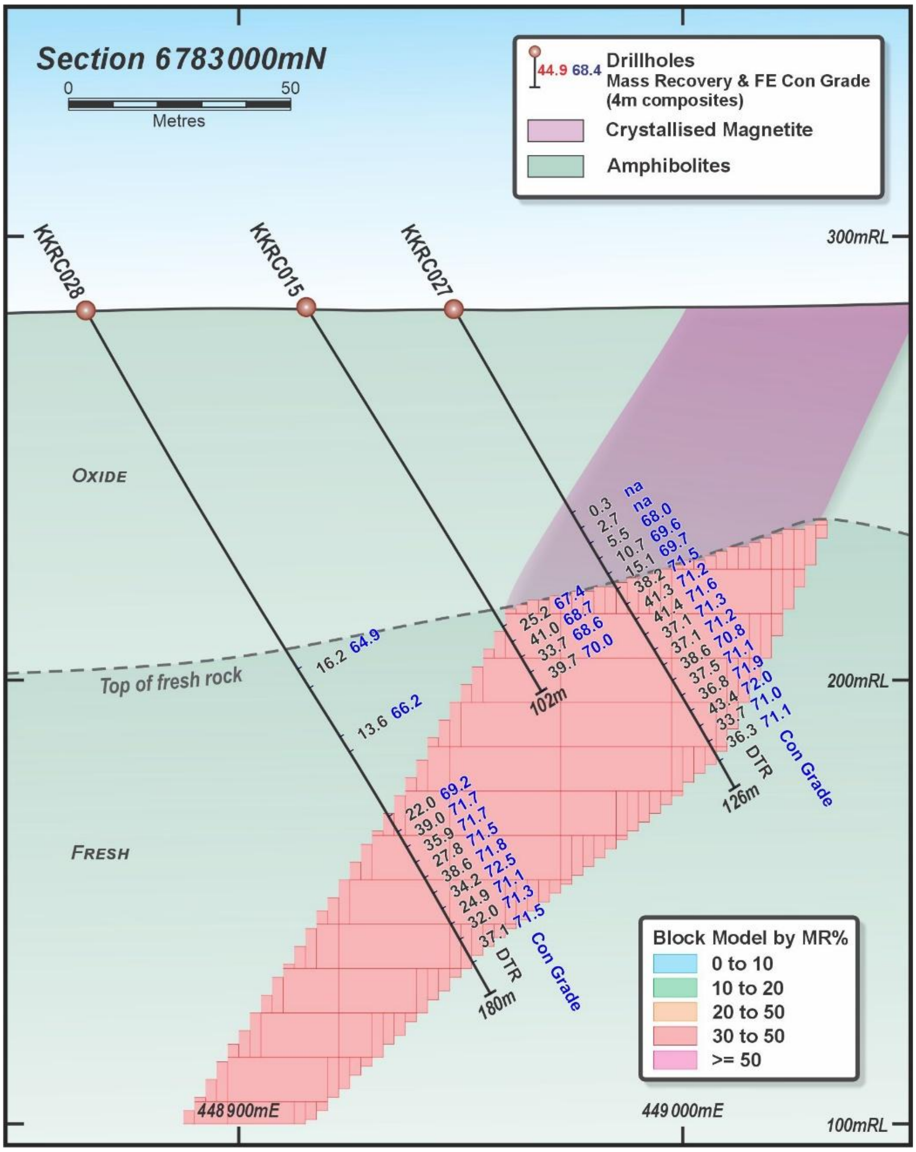

Figure 6: Interpreted drill hole cross-section with block model. Drill traces labelled with DTR Mass Recovery (MR%) and Fe% grade in DTR concentrate.

Table 6: Lodestone Inferred Resources according to DTR Mass Recovery cut-offs for estimated elements. DTR data was leveled to 75 micron grind for estimation

Class	Lower cut-off DTR Mass Recovery %	Million Tonnes	DTR Mass Recovery %	DTR Concentrate			DTR Feed				
				Fe %	SiO2 %	Al2O3 %	Density t/m3	Fe %	SiO2 %	Al_2O_3 %	P %
Inferred	0	110	33	69	3.9	0.08	3.2	28	48	2.3	<0.01
	10	110	33	69	3.9	0.08	3.2	28	48	2.3	<0.01
	20	98	35	69	3.9	0.07	3.2	29	49	2	<0.01
	30	77	38	69	3.4	0.05	3.2	30	50	1.6	<0.01

Notes: MRE reported in accordance with the 2012 JORC Code. Figures are rounded to 2 significant figures and back-calculation simplification from the above tabulation will occur because of rounding. DTR MR = Davis Tube Recovery Mass Recovery. Conc = DTR concentrate. N & C BIF = North and Central Banded Iron Formation zones.

Estimation Methodology / Cut-off Grades

A total of 313 DTR tests with assays were available for the mineralisation modelling, with a mean, minimum and maximum down hole sample lengths of 4.1, 1 and 10 m respectively. Of these 238 were included in the modelled mineralisation wireframes with a mean, minimum and maximum sample lengths of 4.1, 2 and 8 m respectively. All DTR tested samples have magnetic susceptibility determinations and a magnetic susceptibility DTR regressions were used to estimate magnetic mass recovery and Fe concentrate grade to the 25 sample intervals (8% of samples) of mean 4.4 m length within the mineralisation wireframes which did not have DTR test results at the time of the resource estimation. Impurity elements (Si, Al etc.) do not have a significant relationship to magnetic susceptibility and concentrate grades of impurities were not estimated into the DTR data gaps (therefore treated as blanks in the estimation process).

Of the 238 DTR tested intervals some 174 tests were done at 75 µm grind and remaining 64 tests were performed at a 150 µm grind (see DTR test work and assaying section above). With decreasing grind size and feed Fe grade the DTR recovery and concentrate Fe grade decrease and increase respectively such that a correction

Iron mineralisation wireframes to a vertical depth of about 190 m were manually created in Micromine software via sectional interpretation of drill hole logging, DTR, and magnetic susceptibility data. Because magnetic susceptibility was used to guide the DTR test work sampling the magnetite BIF wireframe interpretation is typically snapped to the edge of the DTR intersections.

In the weathered (POX) zone logging was used to guide DTR sampling, and again the BIF wireframes are typically snapped to the edges of the DTR data. DTR Mass Recovery lower threshold for BIF wireframing was 15-20% in the fresh zone according to what is expected to be economically reasonable. The weathered zone (partially oxidised) was geologically modelled but excluded from the current resource estimate on the basis that metallurgical recovery work has yet to be completed and data spacing remains too coarse for satisfactroty estimation.. Minimum downhole thickness for wireframing was 4 m, maximum internal dilution of approximatyely 6 m.

Modifying Factors

Open pit mining has been assumed as the likely extraction method based on the near-surface, tabular geometry of the BIF units. Minimum mining dimensions, dilution factors, and mining recovery have not been formally assessed at this stage, consistent with the Inferred classification of the resource.

The deposit has reasonable prospects for eventual economic extraction based on:

- proximity to the operating Karara magnetite mine (~25 km east) and associated infrastructure including rail to Geraldton port;
- high-quality magnetite concentrate (>65% Fe) producible at coarse grind;
- scale of resource.

Exploration and Resource Upside

The Project has significant resource growth potential:

- The full 25 km strike of the Lodestone magnetite BIF remains largely undrilled. Magnetic imagery and surface exposures confirm continuous magnetite formation extension along strike;
- Several narrower (<20 m) hanging wall and footwall magnetite zones are identified but remain insufficiently drilled for resource estimation;
- A concealed and parallel magnetite BIF unit approximately 30 m in thickness is located about 250 m west of the current resource was intersected by reconnaissance exploration drilling and also offers potential for future resource growth.

From the drilling and mapping completed at Lodestone to date, the mineral grain size and metallurgical performance of the BIF's appear to improve to the south, associated with an increase in the paleo-metamorphic temperature gradient (that has altered the mineralisation). As a priority for exploration, there is 9 kms of BIF south or the resource, that has yet to be drill tested.

Next steps

The maiden resource establishes a clear pathway for resource growth and confidence upgrades.

Killi's immediate focus at Lodestone is to increase geological confidence, improve metallurgical understanding and position the project for future resource upgrades.

Priority work includes infill drilling between existing sections, extensional drilling along strike and further DTR and density test work to support future resource updates and development studies.

Additional work on the partly oxidised zone, including higher-intensity magnetic separation test work and improved weathering definition, will assess its potential to support future classified resource estimates.

About Killi Resources Limited

Killi Resources Ltd ('Killi" (ASX: KLI) is an Australia-based and focused explorer employing a methodical and disciplined approach to exploring for valuable mineral deposits in forgotten mineral provinces (Figure 7).

The Company has agreed to acquire the Lodestone Iron Ore Project in the heart of the Midwest Iron Ore District in Western Australia. The Lodestone Iron Ore Project hosts an Inferred Mineral Resource Estimate of approximately 110Mt at 33% mass recovery.

The Company's other projects include the 100% ownership of the West Tanami Gold Project in Western Australia, and two gold-copper exploration projects in Queensland - the Mt Rawdon West Project near Bundaberg and the Ravenswood Project in the Charters Towers region, both well-endowed mineral provinces that are significantly underexplored and amenable to new large-scale discoveries. The Company also retains copper rights to the Balfour Project in the Pilbara of Western Australia (tenure held by Black Canyon (ASX: BCA)).

The Lodestone Iron Project

The Lodestone Iron Project is located approx. 200 km east of Geraldton and 410 km north of Perth by road in the Mid-West region of Western Australia. The Banded Iron Formation (BIF) units were first targeted for iron ore exploration around 2011 and have been subject to ongoing geological mapping, geophysical surveying, surface sampling, Reverse Circulation (RC) drilling and metallurgical test work to define the extent of the iron ore mineralisation and processing flow sheets. The Lodestone Banded Iron Formation is more coarsely crystalline than most other BIF units in Western Australia and in the fresh zone magnetite is the key iron phase with Davis Tube Recovery (DTR) test work showing a high-quality magnetite product (65-71 % Fe without significant deleterious elements) can be produced at relatively coarse grind sizes (>75 microns). At this stage the project is relatively sparsely drilled (40 reverse Circulation drill holes for holes for 5,023 m) on section spacings c. 400 to 800 m apart and in addition to magnetite resources already identified the project offers considerable potential for resource growth.

A first pass mineral resource estimate (MRE) has been completed in compliance with the JORC code of reporting for a better drilled (mainly 400 m section spacing) 5 km section of the Lodestone magnetite BIF unit.

The Inferred MRE confirms presence of a significant magnetite resource with excellent recovery and Fe concentrate grade with low impurities. Work to date indicates that further drilling and metallurgical test work should be undertaken to refine and extend the resources and underpin future mining and processing studies.

The Mt Rawdon West Project is Killi's flagship exploration asset, comprising of tenement EPM27828 which covers 309 km^2 of prospective gold and copper ground between Evolutions Mt Rawdon Gold Mine and SolGold's Mt Perry Project, located inland 60 kilometres from Bundaberg in Queensland. The project is an early-stage exploration play and hosts a large Cu-Au-Mo soil geochemical anomaly at the intersection of major structural breaks, extending from the Mt Perry and Mt Rawdon deposits.

The Ravenswood North Project consists of five granted tenements totalling ~580 km^2, mostly covering the prospective Ravenswood-Charter Towers gold corridor, host to Ravenswood Gold Mine, Charter Towers, Golden Valley, Kitty O'Shea, Mt Success and Piccadilly. The Company believes this project has the potential to host an Intrusive-Related Gold System.

The West Tanami Project in Western Australia includes 100% ownership of 1,634 km^2 in granted tenure, hosting over 100 kilometre strike of a major gold corridor. The existing gold endowment of the Tanami Gold Province is greater than 19M oz Au and includes the Callie, Tanami, Twin Bonanza, Coyote and Kookaburra mines.

Exploration at West Tanami is being undertaken by Gold Fields Limited (JSE: GFI), who have the right to earn up to an 85% interest in the project by spending $13 million within seven years. The Joint Venture agreement between Killi and

Gold Fields ensures the project will be adequately and systematically explored in the coming years, leveraging it to the financial market's sentiment for gold.

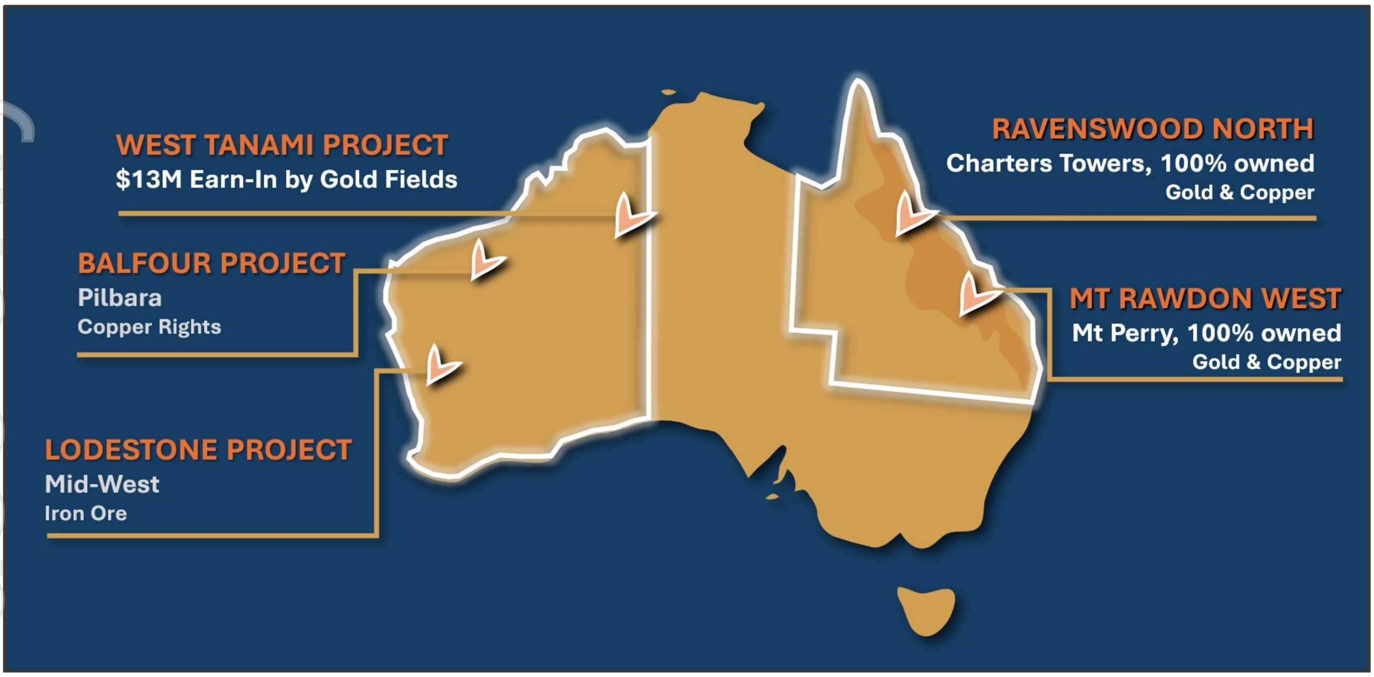

Figure 7: Location of all Killi Resources Projects in Australia.

Table 7: Lodestone Reverse Circulation Drilling collar location and setup details. Datum MGA Zone 50 GDA94.

Hole ID	East MGA50 GDA94	North MGA50 GDA94	RL m	Azimuth MGA	Dip	Depth m	Date Finish
KKRC001	448678	6786595	302	110	-60	90	29/04/2012
KKRC002	448641	6786594	301	111	-65	140	30/04/2012
KKRC003	447220	6793271	288	040	-51	84	1/05/2012
KKRC004	447191	6793241	287	040	-52	120	3/05/2012
KKRC005	449054	6781500	291	100	-58	80	3/05/2012
KKRC006	449014	6781491	288	101	-59	102	4/05/2012
KKRC008	448700	6786199	301	075	-60	102	7/10/2021
KKRC009	448715	6785794	302	086	-60	96	7/10/2021
KKRC010	448703	6785389	293	073	-60	96	8/10/2021
KKRC011	448637	6784999	286	089	-60	78	8/10/2021
KKRC012	448346	6784996	282	092	-60	102	9/10/2021
KKRC013	448482	6785791	293	090	-60	96	10/10/2021
KKRC014	448751	6783803	283	089	-60	102	11/10/2021
KKRC015	448915	6783009	284	091	-60	102	12/10/2021
KKRC016	448979	6782210	284	089	-60	74	13/10/2021
KKRC017	447896	6789387	289	089	-60	75	16/10/2021
KKRC018	448340	6787801	289	094	-60	102	17/10/2021
KKRC019	448227	6788593	297	090	-60	102	18/10/2021

Hole ID	East MGA50 GDA94	North MGA50 GDA94	RL m	Azimuth MGA	Dip	Depth m	Date Finish
KKRC020	448599	6786984	299	090	-60	84	18/10/2021
KKRC021	448748	6784202	284	090	-60	120	14/12/2023
KKRC022	448798	6783798	283	090	-60	168	15/12/2023
KKRC023	448701	6784202	284	090	-60	172	16/12/2023
KKRC024	448701	6783801	282	090	-60	192	17/12/2023
KKRC025	448902	6783399	284	090	-60	120	17/12/2023
KKRC026	448848	6783402	284	090	-60	162	18/12/2023
KKRC027	448948	6783005	284	090	-60	126	18/12/2023
KKRC028	448865	6783007	284	090	-60	180	19/12/2023
KKRC029	449021	6782208	284	090	-60	96	19/12/2023
KKRC030	448933	6782212	283	090	-60	180	6/01/2024
KKRC031	448581	6784998	284	090	-60	160	6/01/2024
KKRC032	448408	6785299	285	090	-60	160	7/01/2024
KKRC033	448650	6786201	299	090	-60	180	8/01/2024
KKRC034	448663	6785797	299	090	-60	150	9/01/2024
KKRC035	448640	6786984	300	090	-60	108	10/01/2024
KKRC036	448574	6786985	298	090	-60	166	11/01/2024
KKRC037	448500	6787803	293	090	-60	160	12/01/2024
KKRC038	448291	6787800	288	090	-60	138	13/01/2024
KKRC039	448179	6788594	295	090	-60	180	14/01/2024
KKRC040	447931	6789390	292	090	-60	100	15/01/2024
KKRC041	447857	6789387	288	090	-60	178	16/01/2024

Table 8: Lodestone Reverse Circulation Drilling sample assay results

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC001	35	39	KK1003	30.8	23.2	1.24	0.508	524	-0.09
KKRC001	56	60	KK1004	24.3	26.7	1.88	0.259	557	-0.02
KKRC001	60	64	KK1005	25.5	25.7	1.68	0.36	612	0.15
KKRC001	64	69	NS1003	10.7	na	na	na	na	na
KKRC001	69	73	KK1006	27.4	24.9	1.33	0.228	557	-0.48
KKRC001	73	77	KK1007	27.8	25.3	0.99	0.048	386	-0.41
KKRC001	77	81	KK1008	31.8	23.1	0.5	0.019	529	-0.75
KKRC001	81	86	KK1009	23.4	25.5	2.89	0.066	582	-0.15
KKRC002	94	98	KK1010	29.5	24.6	0.51	0.06	447	-0.78
KKRC002	98	102	KK1014	24.1	26.7	1.69	0.175	534	-0.46

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC002	102	106	KK1015	26.7	25.5	0.95	0.098	426	-0.56
KKRC002	106	110	KK1016	28	24.8	1.19	0.007	536	-0.83
KKRC002	110	114	KK1017	29.4	24.1	0.86	0.024	584	-0.91
KKRC002	114	118	KK1018	20.1	27	2.69	0.261	572	0.85
KKRC002	118	121	KK1019	11.4	29	4.95	0.328	606	1.03
KKRC002	121	124	KK1020	26	25.2	1.62	0.041	547	-0.55
KKRC002	138	140	NS1004	18.7	na	na	na	na	na
KKRC004	40	44	KK1025	30.6	21	1.38	0.308	772	0.58
KKRC005	25	29	KK1033	34	23	0.37	0.001	452	-0.1
KKRC005	29	33	KK1034	33.4	23.2	0.28	0.243	479	0.25
KKRC005	33	37	KK1035	31.3	24.9	0.28	0.105	583	-0.45
KKRC005	37	41	KK1036	31.9	24.8	0.24	<0.001	415	-0.21
KKRC005	41	45	KK1037	25.7	26.5	1.24	0.105	471	-0.44
KKRC005	45	49	KK1038	31.5	24.1	0.19	<0.001	501	-1.1
KKRC005	49	53	KK1039	33.7	22.4	0.26	<0.001	617	-1.23
KKRC005	53	57	KK1043	31.5	23.4	0.43	0.037	773	-1.19
KKRC005	57	61	KK1044	33.5	22	0.26	0.028	820	-1.15
KKRC005	61	66	KK1045	32.8	21.3	0.78	0.159	662	-1.06
KKRC006	58	62	KK1046	31.8	23.7	0.22	0.072	460	-0.97
KKRC006	62	66	KK1047	32.8	22.9	0.26	0.011	411	-1.23
KKRC006	66	70	KK1048	30.2	24.5	0.49	0.089	504	-0.91
KKRC006	70	74	KK1049	32	23.7	0.28	0.016	494	-1.21
KKRC006	74	78	KK1050	27.7	24.2	1.39	0.023	460	-0.94
KKRC006	78	82	KK1051	30.8	24.1	0.25	0.061	423	-1.1
KKRC006	82	86	KK1052	33.3	22.7	0.18	<0.001	583	-1.11
KKRC006	86	90	KK1053	32.4	22.5	0.46	0.046	791	-1.1
KKRC006	90	93	KK1054	32.6	23.1	0.16	0.055	729	-1.2
KKRC008	40	43	KK1057	30.8	22.7	1.85	0.008	520	3.62
KKRC008	54	58	KK1058	34.6	22.8	0.28	0.005	310	1.52
KKRC008	58	61	KK1059	22.4	27.2	2.82	0.004	210	1.34
KKRC008	61	66	KK1060A	33.7	22.8	0.44	0.022	370	-0.83
KKRC008	66	70	KK1061	32	23.7	0.29	0.164	500	-0.46
KKRC008	70	74	KK1062	27	25.6	0.89	0.056	360	-0.6
KKRC008	74	78	KK1063A	27.1	24.3	1.86	0.031	630	-0.65
KKRC008	78	82	KK1064	32.7	22.7	0.17	0.057	710	-0.78
KKRC008	82	85	KK1065	31.9	22.8	0.2	0.15	940	-0.73

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC008	85	88	KK1066	35.3	21.4	0.17	0.021	720	-0.94
KKRC008	92	94	KK1067	8.6	32.7	3.8	0.336	720	0.98
KKRC008	96	102	KK1069	29.9	22	1.8	0.307	610	-0.57
KKRC009	40	44	KK1070	31.6	23.8	1.25	0.004	130	1.59
KKRC009	44	48	KK1071	33.5	22.8	0.67	0.002	320	1.23
KKRC009	48	52	KK1072	33.5	23.2	0.38	0.003	460	1.24
KKRC009	52	54	KK1073	23.4	26.4	2.68	0.018	320	0.66
KKRC009	54	58	KK1074	33.3	23	0.39	0.001	500	-0.76
KKRC009	58	62	KK1075A	35	21.9	0.19	0.01	630	-0.92
KKRC009	62	66	KK1076	34.2	21.8	0.24	0.051	730	-0.77
KKRC009	66	69	KK1077	32	22.4	0.55	0.253	650	-0.64
KKRC009	76	78	KK1078	10.7	29.5	3.34	0.108	290	1.34
KKRC010	49	52	KK1079	21.8	25.8	3.64	0.008	430	4.22
KKRC010	52	57	KK1080	29.1	24.3	1.64	0.004	310	1.34
KKRC010	57	61	KK1081	35.1	22.1	0.28	0.001	360	0.01
KKRC010	61	65	KK1082	29.7	24.5	0.91	0.282	530	-0.23
KKRC010	65	69	KK1083	31.7	23.7	0.24	0.017	340	-0.87
KKRC010	69	73	KK1084	31.6	23.1	0.57	0.007	420	-0.91
KKRC010	73	77	KK1085	29.8	23.7	1.45	0.021	620	-0.77
KKRC010	77	82	KK1086	25	24.9	2.58	0.068	710	-0.31
KKRC010	89	90	KK1087	21.5	23.5	3.37	0.105	380	0.48
KKRC011	27	31	KK1088	34.5	22	0.65	0.006	410	1.85
KKRC011	31	35	KK1089	36.6	21.1	0.55	0.003	420	1.35
KKRC011	35	39	KK1090	34	22.1	1.23	0.007	600	2.43
KKRC011	39	43	KK1091	33.5	23	0.6	0.004	360	1.62
KKRC011	43	47	KK1092	33.9	23	0.33	0.001	280	1.39
KKRC011	47	51	KK1093	36.7	20.7	0.34	0.001	400	1.92
KKRC011	51	55	KK1094	32.9	22.6	1.03	0.005	650	1.59
KKRC011	55	59	KK1095	21.6	23.9	2.92	0.378	350	1.19
KKRC011	59	62	KK1096A	32.5	21.1	1.61	0.04	640	0.63
KKRC013	87	90	KK1101	36.8	20.3	0.62	0.142	850	1.43
KKRC013	90	94	KK1102A	29	22.3	1.39	0.877	490	0.48
KKRC014	85	89	KK1103	32.3	12.6	8.73	0.026	220	8.9
KKRC015	85	89	KK1104	28.6	24.4	0.9	0.549	480	0.89
KKRC015	89	93	KK1105A	31.9	23.1	0.75	0.065	320	-0.32
KKRC015	93	97	KK1106	29.5	23.7	0.94	0.18	440	-0.01

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC015	97	102	KK1107	31	23.9	0.25	0.031	400	-1.22
KKRC016	70	74	KK1110	27.7	24.1	1.78	0.047	360	0.08
KKRC017	35	39	KK1111	21.2	27.4	3.07	0.729	450	-0.05
KKRC017	39	43	KK1112A	26.3	25.3	2.01	0.144	390	-0.67
KKRC017	43	48	KK1113	24.6	26.1	2.14	0.501	640	-0.12
KKRC017	48	51	KK1114	5.4	35.1	4.71	0.206	390	0.25
KKRC017	51	55	KK1115	23	25.9	2.59	0.658	480	0.05
KKRC017	55	59	KK1116	26	25.4	1.79	0.239	450	-0.68
KKRC017	59	63	KK1117	21.6	26.7	2.9	0.16	420	-0.57
KKRC017	63	67	KK1118	6.6	30.4	6.75	0.211	580	0.26
KKRC017	67	71	KK1119	20.4	27.5	2.95	0.158	480	-0.35
KKRC017	71	75	KK1120	23.4	26.3	2.42	0.09	460	-0.55
KKRC018	30	35	KK1121	25.7	25.3	2.05	0.004	410	1.9
KKRC018	35	39	KK1122	33.1	22.8	0.47	0.138	520	0.02
KKRC018	39	43	KK1123	20.5	27	3.53	0.061	420	0.03
KKRC018	43	47	KK1124	24.6	25.7	2.39	0.05	500	-0.03
KKRC018	47	50	KK1125	20.6	22.8	4.19	0.076	520	1.56
KKRC018	50	54	NS1016	6.6	na	na	na	na	na
KKRC018	54	57	KK1126	29.8	21.9	1.7	0.111	730	0.33
KKRC018	71	75	KK1127	30.5	22.4	1.36	0.22	620	-0.73
KKRC018	75	79	KK1128	21.5	25.3	3.83	0.194	610	0.03
KKRC018	79	83	KK1129	27.6	23	2.68	0.215	700	-0.13
KKRC018	83	86	KK1130	13.9	26.9	5.72	0.682	590	0.95
KKRC019	47	52	KK1132	24.6	25	3	0.1	660	-0.21
KKRC019	52	54	NS1010	7	na	na	na	na	na
KKRC019	54	58	KK1133	29.2	23.4	1.93	0.061	600	-0.8
KKRC019	58	62	KK1134	32.3	21.6	1.48	0.138	620	-0.6
KKRC019	62	66	KK1135	24.4	24.4	3.03	0.121	610	-0.04
KKRC019	66	70	KK1136	21	26.2	3.72	0.125	560	-0.08
KKRC019	70	74	KK1137	28.7	23.1	2.15	0.129	590	-0.56
KKRC019	74	79	NS1011	7.5	na	na	na	na	na
KKRC019	79	82	KK1138	17.8	28	3.41	0.597	490	0.5
KKRC019	82	85	KK1139	30.9	21.7	0.88	0.61	600	-0.4
KKRC019	95	100	KK1140	23	25.7	2.73	0.78	590	0.18
KKRC020	36	38	KK1143	16.5	24.8	4.69	0.173	320	0.75
KKRC020	45	47	KK1144	29.2	25.1	0.23	0.199	820	-0.25

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC020	47	50	KK1145	28.6	23.1	1.19	1.055	820	1.14
KKRC020	56	59	KK1146	23.7	24.8	2.26	1	520	0.27
KKRC020	59	63	KK1147	30.4	23.3	1.39	0.047	440	-1.16
KKRC020	63	68	KK1148	29.6	23.6	1.32	0.054	370	-0.97
KKRC020	68	72	NS1005	6.1	na	na	na	na	na
KKRC020	72	76	KK1149	27.4	24.5	2.1	0.014	550	-0.65
KKRC020	76	80	KK1150	34.5	21.7	0.57	0.002	620	-1.2
KKRC020	80	84	KK1151A	33.8	22	0.32	0.028	600	-0.93
KKRC021	50	54	KK1152	31.8	23.7	0.57	0.025	400	-0.18
KKRC021	54	58	KK1153	30.1	24.7	0.37	0.232	560	-0.7
KKRC021	58	62	KK1154	27.8	25.9	0.58	0.053	360	-0.75
KKRC021	62	66	KK1155	30.4	23.9	0.63	0.046	440	-0.85
KKRC021	66	70	KK1156	31.6	23.1	0.49	0.126	570	-0.88
KKRC021	70	74	KK1157	33.8	21.4	0.22	0.072	750	-1.33
KKRC021	74	77	KK1158	29.9	21.9	1.46	0.038	630	-0.64
KKRC021	108	112	KK1159	25.2	22.3	2.46	0.11	690	-0.33
KKRC022	139	143	KK1160	19.4	30.1	0.97	0.552	370	-0.02
KKRC022	152	156	KK1161	17.8	25.8	3.46	0.138	630	0.28
KKRC023	89	93	KK1162	29.6	24.6	0.48	0.25	340	-0.97
KKRC023	93	97	KK1163	31.9	23.8	0.27	0.091	380	-1.22
KKRC023	97	101	KK1164	26	25.6	1.55	0.044	400	-0.88
KKRC023	101	105	KK1165	27.2	25.5	0.78	0.131	340	-0.85
KKRC023	105	109	KK1166	31.9	22.4	0.35	0.022	380	-1.02
KKRC023	109	113	KK1167	29.9	23.7	1.12	0.065	490	-1.01
KKRC023	113	117	KK1168	33.2	22.1	0.26	0.086	850	-0.82
KKRC023	117	120	KK1169	35.2	21	0.15	0.058	700	-1.26
KKRC023	152	157	KK1170	16.9	23.5	3.76	0.472	490	3.32
KKRC024	71	75	KK1171	8.5	32.3	6.19	0.003	50	4.39
KKRC024	75	79	KK1172	25.9	21.1	5.35	0.015	80	6.11
KKRC024	79	82	KK1173	36.6	11.8	7.12	0.022	170	7.25
KKRC024	97	102	KK1174	20.9	25.7	3.88	0.008	600	4.26
KKRC024	102	106	KK1175	20.2	26.8	3.82	0.372	870	2.61
KKRC024	106	111	KK1176	20.7	26.7	3.5	0.356	940	1.09
KKRC024	176	180	KK1177	32	21	0.93	0.388	450	-0.53
KKRC024	180	184	KK1178	22.8	25.8	0.46	0.077	450	-0.04
KKRC024	184	189	KK1179	18.2	22.5	3.83	0.066	360	1.1

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC025	60	64	KK1180	15.7	35.3	0.73	0.005	70	1.01
KKRC025	64	68	KK1181	25.3	29.2	0.47	0.002	60	0.82
KKRC025	68	72	KK1182	29.7	26.4	0.37	0.001	50	0.53
KKRC025	72	76	KK1183	28.8	26.8	0.3	0.001	60	0.43
KKRC025	76	80	KK1184	28.2	26.7	0.7	0.001	80	0.93
KKRC025	80	84	KK1185	28.7	26.3	0.46	0.005	140	1.78
KKRC025	84	88	KK1186	31	24.5	0.44	0.016	240	1.93
KKRC025	88	92	KK1187	30.8	24.7	0.41	0.01	370	1.13
KKRC025	92	96	KK1188	30	25.3	0.14	0.006	410	0.07
KKRC025	96	100	KK1189	30.1	24.1	0.74	0.059	610	-0.68
KKRC025	100	104	KK1190	31.5	22.9	0.49	0.065	660	-0.98
KKRC025	104	108	KK1191	31.9	22.9	0.51	0.049	570	-1.03
KKRC026	102	107	KK1192	7.9	34.2	5.29	0.656	180	4.02
KKRC026	107	111	KK1193	28.4	24.9	1.54	0.413	190	1.44
KKRC026	111	115	KK1194	30.9	24.7	0.47	0.057	360	-0.54
KKRC026	115	119	KK1195	33.4	22.3	0.19	0.022	380	-1.11
KKRC026	119	123	KK1196	28.6	25.5	0.3	0.06	350	-1.1
KKRC026	123	127	KK1197	26.9	26	0.35	0.106	330	-1.03
KKRC026	127	131	KK1198	27.5	26	0.25	0.03	310	-1.19
KKRC026	131	135	KK1199	28.1	25.6	0.25	0.035	280	-1.19
KKRC026	135	139	KK1200	30.4	24.1	0.19	0.052	400	-1.24
KKRC026	139	144	KK1201	30.3	23.4	0.68	0.077	590	-1.03
KKRC027	54	58	KK1202	20.1	27.3	3.46	0.031	430	5.22
KKRC027	58	62	KK1203	33.8	22.4	0.57	0.005	370	2.1
KKRC027	62	66	KK1204	35.9	21.4	0.32	0.001	340	1.42
KKRC027	66	70	KK1205	32.6	23.3	0.43	0.026	380	1.82
KKRC027	70	74	KK1206	30.8	24.4	0.28	0.013	360	0.91
KKRC027	74	78	KK1207	31.4	23.8	0.18	0.027	360	-0.96
KKRC027	78	82	KK1208	32	23.2	0.13	0.006	490	-1.22
KKRC027	82	86	KK1209	33.7	22.2	0.11	0.014	430	-1.27
KKRC027	86	90	KK1210	31.4	22.8	0.42	0.044	520	-1.1
KKRC027	90	94	KK1211	31.7	22.6	0.22	0.053	540	-1.31
KKRC027	94	98	KK1212	32.1	22.3	0.53	0.031	570	-1.33
KKRC027	98	102	KK1213	30.8	23.1	0.24	0.083	660	-1.3
KKRC027	102	106	KK1214	32.7	21.5	0.12	0.045	800	-1.26
KKRC027	106	110	KK1215	33.9	20.5	0.73	0.027	830	-0.9

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC027	110	114	KK1216	27.2	24.2	1.43	0.041	740	-0.92
KKRC027	114	119	KK1217	30.7	23	0.56	0.781	740	-0.22
KKRC028	95	100	KK1218	28.2	21.7	1.53	1.65	750	6.75
KKRC028	113	117	KK1219	18.5	24.9	3.05	0.284	480	0.96
KKRC028	134	138	KK1220	26.5	25.1	0.94	1.285	450	-0.12
KKRC028	138	142	KK1221	31.5	22.8	0.61	0.085	340	-1.11
KKRC028	142	146	KK1222	29.1	23.6	1.28	0.164	350	-0.66
KKRC028	146	150	KK1223	26.2	23.7	1.33	0.067	520	-0.66
KKRC028	150	154	KK1224	33	21.1	0.14	0.056	720	-0.81
KKRC028	154	158	KK1225	29.7	23.4	0.44	0.176	750	-0.82
KKRC028	158	162	KK1226	23.2	26.8	0.91	0.176	890	-0.67
KKRC028	162	166	KK1227	27.1	24.4	1.41	0.266	600	-0.75
KKRC028	166	172	KK1228	30	22.5	0.98	0.084	730	-1
KKRC029	26	29	KK1229	7.6	34.6	4.92	0.012	60	3.74
KKRC029	29	34	KK1230	18.3	24	7.28	0.019	100	6.96
KKRC029	34	38	KK1231	33	21.6	1.28	0.005	270	2.29
KKRC029	38	42	KK1232	34	21.8	0.88	0.005	370	2.4
KKRC029	42	46	KK1233	35.9	20.5	0.68	0.004	610	2.13
KKRC029	46	50	KK1234	29.4	22.7	2.28	0.001	410	1.9
KKRC029	50	54	KK1235	38.5	19	0.67	0.001	610	1.69
KKRC029	54	59	KK1236	22.2	26.4	3.52	0.001	370	1.41
KKRC029	66	70	KK1237	14.9	31.6	2.03	0.469	300	0.86
KKRC030	95	99	KK1238	22.2	25.2	2.19	0.164	550	0.67
KKRC030	108	112	KK1239	26.5	23.3	1.8	0.983	600	0.64
KKRC030	112	116	KK1240	29	23.7	0.68	0.205	320	0.18
KKRC030	116	120	KK1241	35.3	21.2	0.14	0.008	390	-0.7
KKRC030	120	124	KK1242	35.9	21.1	0.19	0.012	350	-1.33
KKRC030	124	128	KK1243	33.9	22.4	0.22	0.162	420	-1.19
KKRC030	128	132	KK1244	34.7	21.9	0.18	0.019	340	-1.33
KKRC030	132	136	KK1245	33.5	22.5	0.33	0.026	280	-1.16
KKRC030	136	140	KK1246	35.1	21.5	0.19	0.007	450	-1.32
KKRC030	140	144	KK1247	35.3	20.6	0.52	0.018	480	-1.45
KKRC030	144	148	KK1248	34.8	21	0.16	0.045	470	-1.43
KKRC030	148	152	KK1249	15.9	27.9	4.69	0.057	650	-0.23
KKRC030	152	156	KK1250	30.7	22.4	1.46	0.025	580	-1.19
KKRC030	162	167	KK1251	18	31.4	1.16	0.49	380	-0.04

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC031	70	75	KK1252	24.6	23.7	2.27	0.285	610	0.86
KKRC031	83	87	KK1253	23.4	23.5	2.45	0.58	490	1.02
KKRC031	87	91	KK1254	29.5	23.5	0.78	0.192	310	-0.73
KKRC031	91	95	KK1255	32.6	23.3	0.3	0.138	420	-0.91
KKRC031	95	99	KK1256	31	23.7	0.41	0.058	360	-0.49
KKRC031	99	103	KK1257	35.1	21.3	0.22	0.016	550	-0.53
KKRC031	103	107	KK1258	34.3	18.7	1.21	0.537	910	1.06
KKRC031	107	110	KK1259	28.1	22.5	1.94	0.056	580	0.34
KKRC031	110	120	NS1001	13	na	na	na	na	na
KKRC031	120	123	KK1260	30.6	20.1	1.87	0.046	550	-0.63
KKRC031	144	150	KK1261	30.5	21.1	2.42	0.143	730	-0.79
KKRC032	78	82	KK1262	28.6	21.9	1.79	0.405	510	0.76
KKRC032	82	86	KK1263	29.3	21.7	2.19	0.306	530	1.08
KKRC032	86	90	KK1264	26.2	23.3	2.88	0.19	620	0.21
KKRC032	90	94	KK1265	25.6	23.7	2.93	0.272	430	0.58
KKRC032	94	98	KK1266	17	27.4	4.35	0.213	330	0.58
KKRC032	98	102	KK1267	18.2	27.1	4.2	0.295	320	0.98
KKRC032	102	106	KK1268	22.2	24.4	3.76	0.698	460	1.29
KKRC032	106	110	KK1269	13.9	28.3	5.08	1.01	480	1.45
KKRC032	110	114	KK1270	13.4	29.1	5.02	0.466	400	0.77
KKRC032	114	118	KK1271	15	28.5	4.37	1.37	580	1.68
KKRC032	118	123	KK1272	19.3	27	3.75	0.324	700	0.93
KKRC033	88	91	KK1273	28.2	23.6	1.15	0.614	710	0.11
KKRC033	98	102	KK1274	28.3	24.1	1.07	0.874	560	0.03
KKRC033	102	106	KK1275	22.8	26.6	2.22	0.132	320	-0.39
KKRC033	106	110	KK1276	32.3	23.1	0.47	0.011	430	-0.94
KKRC033	110	114	KK1277	29.6	23.8	0.92	0.062	460	-0.86
KKRC033	114	118	KK1278	31	23.8	0.22	0.172	530	-0.81
KKRC033	118	122	KK1279	27.7	25.2	0.77	0.136	400	-0.44
KKRC033	122	126	KK1280	33.3	22.5	0.19	0.045	500	-1
KKRC033	126	130	KK1281	20.5	26.8	3.53	0.159	710	-0.09
KKRC033	148	153	KK1282	14.4	33.9	0.79	0.23	280	0.68
KKRC033	153	158	KK1283	16.6	29.8	2.25	0.876	490	1.03
KKRC033	158	162	KK1284	24.6	24.8	1.72	0.213	530	0.53
KKRC033	162	166	KK1285	32	21.7	1.06	0.106	680	-0.79
KKRC033	166	170	KK1286	29.1	22.7	1.61	0.166	730	0.33

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC034	5	15	KK1359	13.9	na	na	na	na	na
KKRC034	66	71	KK1360	7.3	na	na	na	na	na
KKRC034	80	84	KK1287	19.6	27.1	3.52	0.464	480	0.71
KKRC034	84	88	KK1288	32.5	22.8	0.41	0.027	400	-0.96
KKRC034	88	92	KK1289	31.1	23.5	0.48	0.052	420	-0.89
KKRC034	92	96	KK1290	29.4	24.2	0.91	0.036	410	-0.92
KKRC034	96	100	KK1291	35.7	21.1	0.14	0.007	600	-1.29
KKRC034	100	106	KK1292	34.2	21.8	0.25	0.116	710	-1.14
KKRC034	117	121	KK1293	35.8	20.1	0.42	0.052	650	-0.94
KKRC034	132	139	NS1002	19	na	na	na	na	na
KKRC035	15	20	KK1294	30.6	23.3	0.93	0.003	240	2.07
KKRC035	20	25	KK1295	21.8	27	2.84	0.001	270	1.11
KKRC035	25	30	KK1296	31.5	23.4	0.5	0.023	420	1.48
KKRC035	30	34	KK1297	28.9	24.7	0.74	0.027	490	0.62
KKRC035	34	38	KK1298	27.8	25.2	1.02	0.05	360	-0.46
KKRC035	38	42	KK1299	30.2	23.9	0.93	0.005	480	-0.76
KKRC035	42	46	KK1300	29.4	23.5	1.39	0.058	650	-0.79
KKRC035	46	49	KK1301	33.9	22.3	0.36	0.065	770	-0.98
KKRC035	64	66	NS1006	19.2	na	na	na	na	na
KKRC035	85	90	KK1302	20.9	25.5	3.66	0.326	560	-0.11
KKRC035	90	94	KK1303	18.7	24.3	3.5	0.186	570	1.2
KKRC035	94	98	KK1304	15.4	30.6	3.02	0.991	480	0.63
KKRC035	98	102	KK1305	17.7	30.1	2.21	0.76	380	0.45
KKRC035	102	106	KK1306	12.1	29.8	5.21	0.221	440	0.36
KKRC036	92	96	KK1307	24.1	25.1	2.2	1.215	590	0.36
KKRC036	96	100	KK1308	26.6	25.5	1.64	0.23	390	-0.9
KKRC036	100	104	KK1309	30.5	23.7	0.85	0.046	490	-1.02
KKRC036	104	108	KK1310	29.8	24.5	0.65	0.011	390	-1.27
KKRC036	108	112	KK1311	26.1	25.1	1.5	0.128	470	-0.92
KKRC036	112	116	KK1312	30.8	23.5	0.7	0.064	570	-0.84
KKRC036	116	119	KK1313	34.2	21.1	0.25	0.057	850	-0.85
KKRC036	156	160	KK1314	31.7	19.6	1.78	0.025	750	-0.92
KKRC037	34	39	KK1315	25.2	23.9	2.76	0.21	640	0.42
KKRC037	39	43	KK1316	23.5	26.4	1.66	1.545	600	1.48
KKRC037	43	48	KK1317	25.5	26.5	1.22	0.7	620	0.45
KKRC037	58	62	KK1318	10.1	27.5	4.06	0.239	480	2.97

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC037	100	105	KK1319	29.6	23.4	1.06	0.079	590	-0.94
KKRC037	105	111	KK1320	14.8	25.3	5.26	0.321	500	0.65
KKRC037	111	116	NS1007	14.4	na	na	na	na	na
KKRC038	74	79	KK1321	24.3	25.6	1.98	0.152	480	0.36
KKRC038	79	84	KK1322	28.8	24.7	0.97	0.076	460	-0.77
KKRC038	84	87	NS1008	16.7	na	na	na	na	na
KKRC038	87	92	KK1323	23.9	26	1.99	0.047	480	-0.38
KKRC038	92	100	NS1009	17.7	na	na	na	na	na
KKRC038	107	111	KK1324	27.4	24.4	1.69	0.194	600	-0.63
KKRC038	111	115	KK1325	29.4	22.5	1.79	0.067	670	-0.46
KKRC038	115	118	KK1326	19	25.4	4.37	1.065	690	0.95
KKRC038	118	121	KK1327	27	24.8	1.69	0.134	610	-0.27
KKRC039	83	87	KK1328	28.1	23.3	2.2	0.122	700	-0.59
KKRC039	87	91	KK1329	28.8	22.7	2.19	0.129	720	-0.57
KKRC039	91	95	KK1330	30.4	22.9	1.61	0.074	680	-0.72
KKRC039	95	99	KK1331	28.6	23.1	1.92	0.108	700	-0.7
KKRC039	99	103	KK1332	23.6	24.2	3.66	0.152	870	-0.39
KKRC039	103	107	KK1333	29.5	22.7	1.78	0.142	680	-0.74
KKRC039	107	111	KK1334	30	23	1.75	0.105	680	-0.75
KKRC039	111	115	KK1335	23.1	26.9	1.76	0.347	620	-0.44
KKRC039	115	119	KK1336	14	28.6	3.97	0.743	410	0.97
KKRC039	129	133	KK1337	27.5	23.8	1.78	0.036	590	-0.79
KKRC039	133	137	KK1338	33.2	22.5	0.27	0.011	560	-1.31
KKRC039	140	144	KK1339	30.9	23.6	0.68	0.063	390	-1.09
KKRC039	144	148	KK1340	31.1	23.8	0.56	0.675	480	-0.65
KKRC039	148	152	KK1341	24	23.7	2.66	0.231	710	-0.28
KKRC039	152	159	NS1012	14.9	na	na	na	na	na
KKRC039	159	164	KK1342	20.1	23.7	3.98	1.785	440	2.07
KKRC040	6	12	KK1356	8.2	na	na	na	na	na
KKRC040	12	17	KK1357	10	na	na	na	na	na
KKRC040	17	22	KK1358	16.8	na	na	na	na	na
KKRC040	22	25	NS1013	6.9	na	na	na	na	na
KKRC040	25	30	KK1343	21.4	27.3	2.51	0.395	410	-0.12
KKRC040	30	35	KK1344	25.4	25.3	1.77	0.188	580	-0.53
KKRC040	35	41	KK1345	20	na	na	na	na	na
KKRC040	41	47	KK1346	15.9	na	na	na	na	na

Hole	From m	To m	Sample	Fe %	Si %	Al %	S %	P ppm	LOI %
KKRC040	47	51	KK1347	24.7	na	na	na	na	na
KKRC040	51	55	KK1348	24.2	na	na	na	na	na
KKRC040	55	59	KK1349	22.3	na	na	na	na	na
KKRC040	86	92	NS1014	15.9	na	na	na	na	na
KKRC041	81	85	KK1350	26.1	na	na	na	na	na
KKRC041	85	89	KK1351	22.4	na	na	na	na	na
KKRC041	89	93	KK1352	22.3	na	na	na	na	na
KKRC041	93	97	KK1353	25.1	na	na	na	na	na
KKRC041	97	101	KK1354	23.4	na	na	na	na	na
KKRC041	101	105	KK1355	20	na	na	na	na	na
KKRC041	142	146	NS1015	14.5	na	na	na	na	na

Table 9: Lodestone Reverse Circulation Drilling sample Davis Tube Recovery assay results, Magnetic Susceptibility reading and Calculated Density

Hole	From m	To m	Sample	Magsus 10^{-3} SI	Mass Rec %	CON Fe %	CON Si %	CON Al %	CON S %	CON P ppm	CON LOI %	Density g/cm³
KKRC001	35	39	KK1003	417.3	39.3	66.9	1.86	0.06	0.018	2	-2.7	3.25
KKRC001	56	60	KK1004	368.8	31.2	64.6	3.25	0.08	0.016	41	-3.02	3.13
KKRC001	60	64	KK1005	387.8	30.7	65.9	2.38	0.07	0.036	40	-3.04	3.16
KKRC001	69	73	KK1006	431.3	35.7	65.1	2.81	0.07	0.025	63	-3.02	3.22
KKRC001	73	77	KK1007	413	36.3	66	2.31	0.06	0.001	5	-3.06	3.23
KKRC001	77	81	KK1008	252.5	42.1	67.6	1.27	0.05	<0.001	2	-3.28	3.35
KKRC001	81	86	KK1009	281.2	29.3	66.3	2.11	0.11	0.012	79	-3.01	3.1
KKRC002	94	98	KK1010	547.5	40.4	65.5	2.63	0.08	0.003	13	-2.9	3.28
KKRC002	98	102	KK1014	277.5	30.9	66.6	1.92	0.07	0.014	52	-3.16	3.12
KKRC002	102	106	KK1015	334.8	36.5	65.8	2.38	0.05	0.005	15	-3.28	3.2
KKRC002	106	110	KK1016	291.8	38.3	67.8	1.2	0.1	0.002	2	-3.5	3.24
KKRC002	110	114	KK1017	442	38.5	66.1	2.08	0.16	0.003	39	-3.33	3.28
KKRC002	114	118	KK1018	219.5	22.3	61.2	5.12	0.26	0.017	100	-3.24	3
KKRC002	118	121	KK1019	77.6	10.4	62.7	4.26	0.21	0.021	80	-3.18	2.73
KKRC002	121	124	KK1020	321.7	34.4	65.1	2.88	0.1	0.004	9	-3.25	3.18
KKRC004	40	44	KK1025	169.8	20.9	60.9	6.22	0.28	0.042	213	-2.33	3.24
KKRC005	25	29	KK1033	312.5	40.3	67.6	1.26	0.11	0.013	2	-3.1	3.42
KKRC005	29	33	KK1034	283.5	36.9	67.9	1.15	0.04	0.04	8	-2.09	3.4
KKRC005	33	37	KK1035	488.5	39.6	68.4	0.78	0.1	0.016	2	-3.17	3.34
KKRC005	37	41	KK1036	331.5	33.3	68.3	0.91	0.05	0.014	7	-2.78	3.36

Hole	From m	To m	Sample	Magsus 10^{-3} SI	Mass Rec %	CON Fe %	CON Si %	CON Al %	CON S %	CON P ppm	CON LOI %	Density g/cm³
KKRC005	41	45	KK1037	429.5	33.5	67	1.75	0.03	0.014	2	-3.44	3.17
KKRC005	45	49	KK1038	483	40.7	68.7	0.5	0.1	0.004	2	-3.57	3.34
KKRC005	49	53	KK1039	571	42.2	68.2	0.64	0.25	0.003	19	-3.55	3.41
KKRC005	53	57	KK1043	537.3	43.3	68.5	0.76	0.04	0.004	14	-3.61	3.34
KKRC005	57	61	KK1044	524.5	43.3	68.8	0.5	0.08	0.005	35	-3.69	3.41
KKRC005	61	66	KK1045	297.2	31.7	68.7	0.58	0.08	0.011	64	-3.37	3.38
KKRC006	58	62	KK1046	481.3	40.6	68.4	0.83	0.05	0.003	2	-3.35	3.35
KKRC006	62	66	KK1047	404.3	44.9	68.4	0.8	0.05	<0.001	2	-3.38	3.38
KKRC006	66	70	KK1048	379.5	39.3	68.6	0.73	0.03	0.008	2	-3.27	3.3
KKRC006	70	74	KK1049	460.3	42.9	68.9	0.53	0.01	<0.001	2	-3.38	3.36
KKRC006	74	78	KK1050	374.5	36.6	69.3	1.04	0.05	<0.001	9	-3.42	3.23
KKRC006	78	82	KK1051	480.5	39.5	68.7	0.64	0.02	0.003	2	-3.29	3.32
KKRC006	82	86	KK1052	469	43.7	68.8	0.54	0.03	<0.001	2	-3.33	3.4
KKRC006	86	90	KK1053	436	42.5	68.8	0.53	0.02	0.003	14	-3.36	3.37
KKRC006	90	93	KK1054	460.7	43	68.8	0.48	0.03	0.002	18	-3.35	3.38
KKRC021	50	54	KK1152	498.8	34.5	69.7	1.15	0.02	0.005	30	-2.67	3.35
KKRC021	54	58	KK1153	645.3	37.6	69.3	1.45	0.02	0.041	60	-3.2	3.3
KKRC021	58	62	KK1154	585.3	35.5	68.8	1.73	0.03	0.01	30	-3.21	3.23
KKRC021	62	66	KK1155	653.8	38.1	69.4	1.52	0.02	0.007	40	-3.23	3.31
KKRC021	66	70	KK1156	531.5	40.1	68.3	1.88	0.03	0.017	120	-3.18	3.35
KKRC021	70	74	KK1157	778.8	44.1	71.2	0.89	0.02	0.007	110	-3.29	3.41
KKRC021	74	77	KK1158	493.3	36.8	69	1.61	0.05	0.006	140	-3.23	3.3
KKRC021	108	112	KK1159	430.5	26.8	71.2	0.43	0.04	0.025	40	-3.34	3.15
KKRC022	139	143	KK1160	366.8	19	66.4	2.9	0.12	1.63	70	na	2.96
KKRC022	152	156	KK1161	291.5	16.7	na	na	na	na	na	na	2.92
KKRC023	89	93	KK1162	570	36.5	70.4	1.15	0.02	0.137	30	-3.26	3.29
KKRC023	93	97	KK1163	777.8	41.5	70.7	0.77	0.01	0.015	30	-3.34	3.36
KKRC023	97	101	KK1164	561.6	33.1	70.1	1.22	0.01	0.01	30	-3.29	3.18
KKRC023	101	105	KK1165	595.8	33.6	69.2	1.63	0.03	0.015	50	-3.25	3.21
KKRC023	105	109	KK1166	721.5	43.1	69.3	1.22	0.02	0.005	30	-3.33	3.36
KKRC023	109	113	KK1167	534.3	38.5	69.5	1.23	0.03	0.013	110	-3.26	3.3
KKRC023	113	117	KK1168	662.8	42.6	70.9	0.79	0.02	0.008	200	-3.3	3.39
KKRC023	117	120	KK1169	763.7	46.4	69.1	1.58	0.01	0.006	130	-3.32	3.46
KKRC023	152	157	KK1170	207.9	12.5	70.3	0.85	0.1	0.55	60	-3.22	2.9
KKRC024	71	75	KK1171	15.8	3.8	59.7	2.25	4.01	0.019	110	na	2.69
KKRC024	75	79	KK1172	42.1	9.5	60.8	2.04	3.3	0.013	110	2.75	3.12

Hole	From m	To m	Sample	Magsus 10^{-3} SI	Mass Rec %	CON Fe %	CON Si %	CON Al %	CON S %	CON P ppm	CON LOI %	Density g/cm³
KKRC024	79	82	KK1173	18.4	7.6	59.6	2.07	4.06	0.015	120	2.17	3.39
KKRC024	97	102	KK1174	1.2	0.2	na	na	na	na	na	na	3
KKRC024	102	106	KK1175	78.8	6.7	61.3	6.62	0.21	0.031	150	na	2.98
KKRC024	106	111	KK1176	38.4	4.8	66.2	3.42	0.29	0.044	170	na	2.99
KKRC024	176	180	KK1177	687	32.1	70.8	0.69	0.13	0.338	50	-3.16	3.28
KKRC024	180	184	KK1178	378.5	17.4	70.1	0.85	0.13	0.081	70	-3.2	3.05
KKRC024	184	189	KK1179	103.1	13.5	69.6	1.27	0.08	0.153	130	-3.26	2.93
KKRC025	60	64	KK1180	2.5	0.2	na	na	na	na	na	na	2.77
KKRC025	64	68	KK1181	5	5.6	67.2	1.8	0.08	0.004	30	na	2.95
KKRC025	68	72	KK1182	4.2	0.7	na	na	na	na	na	na	3.04
KKRC025	72	76	KK1183	1.8	0.2	na	na	na	na	na	na	3.02
KKRC025	76	80	KK1184	2.6	0.2	na	na	na	na	na	na	3.01
KKRC025	80	84	KK1185	7	0.8	na	na	na	na	na	na	3.02
KKRC025	84	88	KK1186	71.5	14.7	70.4	0.74	0.01	0.009	50	-1.15	3.06
KKRC025	88	92	KK1187	196.7	20.4	69.9	0.66	0.01	0.007	40	-1.25	3.32
KKRC025	92	96	KK1188	304	29	70.6	0.6	0.01	0.003	20	-2.45	3.3
KKRC025	96	100	KK1189	506.3	35.2	71	0.37	0.01	0.007	30	-3.18	3.3
KKRC025	100	104	KK1190	475.5	36	71.9	0.34	0.02	0.013	40	-3.37	3.34
KKRC025	104	108	KK1191	405.8	36	71.5	0.32	0.02	0.012	30	-3.46	3.36
KKRC026	102	107	KK1192	0.8	0.3	na	na	na	na	na	na	2.67
KKRC026	107	111	KK1193	524.8	29.9	72	0.51	0.01	0.014	20	-2.99	3.25
KKRC026	111	115	KK1194	869	39.4	71.6	0.32	0.01	0.005	10	-3.5	3.33
KKRC026	115	119	KK1195	871.3	43.3	71.6	0.23	0.01	0.003	10	-3.44	3.4
KKRC026	119	123	KK1196	812.5	36	71.6	0.29	0.01	0.004	20	-3.41	3.26
KKRC026	123	127	KK1197	689.3	31.7	71.3	0.44	0.01	0.013	30	-3.45	3.21
KKRC026	127	131	KK1198	762.5	33.7	70.8	0.77	0.01	0.006	20	-3.46	3.22
KKRC026	131	135	KK1199	780.3	34.4	70.8	0.79	0.01	0.005	20	-3.34	3.24
KKRC026	135	139	KK1200	731.5	38	71.9	0.43	0.01	0.004	20	-3.33	3.31
KKRC026	139	144	KK1201	638.4	37.9	71.7	0.43	0.02	0.006	30	-3.35	3.31
KKRC027	54	58	KK1202	1.1	0.3	na	na	na	na	na	na	2.85
KKRC027	58	62	KK1203	12.5	2.7	na	na	na	na	na	na	3.12
KKRC027	62	66	KK1204	13.6	5.5	68	1.26	0.01	0.006	180	na	3.16
KKRC027	66	70	KK1205	20.7	10.7	69.6	0.89	0.01	0.011	130	0.28	3.1
KKRC027	70	74	KK1206	121.4	15.1	69.7	0.73	0.01	0.007	60	-1.1	3.06
KKRC027	74	78	KK1207	963.8	38.2	71.5	0.57	0.01	0.003	10	-3.16	3.34
KKRC027	78	82	KK1208	730	41.3	71.2	0.61	0.01	0.003	20	-3.34	3.36

Hole	From m	To m	Sample	Magsus 10^{-3} SI	Mass Rec %	CON Fe %	CON Si %	CON Al %	CON S %	CON P ppm	CON LOI %	Density g/cm³
KKRC027	82	86	KK1209	959.3	41.4	71.6	0.38	0.01	0.003	20	-3.33	3.41
KKRC027	86	90	KK1210	716.8	37.1	71.3	0.43	0.01	0.005	30	-3.33	3.34
KKRC027	90	94	KK1211	608	37.1	71.2	0.28	0.01	0.007	30	-3.31	3.35
KKRC027	94	98	KK1212	759.8	38.6	70.8	0.46	0.01	0.006	40	-3.33	3.36
KKRC027	98	102	KK1213	661	37.5	71.1	0.36	0.01	0.008	40	-3.34	3.32
KKRC027	102	106	KK1214	696	36.8	71.9	0.26	0.01	0.004	40	-3.37	3.38
KKRC027	106	110	KK1215	986	43.4	72	0.32	0.01	0.004	50	-3.34	3.42
KKRC027	110	114	KK1216	724	33.7	71.1	0.47	0.01	0.008	50	-3.32	3.21
KKRC027	114	119	KK1217	652	36.3	71.1	0.63	0.01	0.076	70	-3.12	3.32
KKRC028	95	100	KK1218	205.8	16.2	64.9	4.3	0.16	0.066	210	-2.5	3.18
KKRC028	113	117	KK1219	183.8	13.6	66.2	3.37	0.04	0.13	210	-3.06	2.94
KKRC028	134	138	KK1220	551.3	22	69.2	1.12	0.02	3.61	70	-1.62	3.19
KKRC028	138	142	KK1221	841.5	39	71.7	0.48	0.01	0.038	30	-3.37	3.34
KKRC028	142	146	KK1222	640.9	35.9	71.7	0.39	0.01	0.017	20	-3.36	3.27
KKRC028	146	150	KK1223	365.3	27.8	71.5	0.4	0.01	0.012	30	-3.36	3.18
KKRC028	150	154	KK1224	699.8	38.6	71.8	0.29	0.01	0.009	60	-3.26	3.39
KKRC028	154	158	KK1225	396	34.2	72.5	0.39	0.01	0.014	50	-3.31	3.29
KKRC028	158	162	KK1226	251	24.9	71.1	0.78	0.01	0.015	70	-3.32	3.09
KKRC028	162	166	KK1227	371.5	32	71.3	0.49	0.01	0.017	50	-3.31	3.21
KKRC028	166	172	KK1228	406.3	37.1	71.6	0.49	0.01	0.013	50	-3.32	3.3
KKRC029	26	29	KK1229	0.8	0.1	na	na	na	na	na	na	2.61
KKRC029	29	34	KK1230	1.2	0.1	na	na	na	na	na	na	2.82
KKRC029	34	38	KK1231	14	11.4	68	1.24	0.05	0.007	260	0.23	3.11
KKRC029	38	42	KK1232	11.8	10	68.6	1.11	0.04	0.007	230	0.24	3.12
KKRC029	42	46	KK1233	56.4	15.8	68.5	1.07	0.01	0.007	330	-0.13	3.16
KKRC029	46	50	KK1234	12	8.3	67	1.83	0.03	0.006	340	0.25	3.03
KKRC029	50	54	KK1235	31.1	18.1	67.7	1.48	0.01	0.006	330	0.15	3.21
KKRC029	54	59	KK1236	15.4	8.9	68.3	1.21	0.02	0.006	250	na	2.89
KKRC029	66	70	KK1237	294.8	13.6	69.7	1.46	0.06	0.05	40	-3.14	2.85
KKRC030	95	99	KK1238	272.3	23.6	62.1	6.22	0.01	0.022	150	-2.79	3.03
KKRC030	108	112	KK1239	175.5	13.4	68.1	1.92	0.09	1.32	170	-2.55	3.14
KKRC030	112	116	KK1240	591.8	35	71.6	0.47	0.01	0.083	30	-3.2	3.27
KKRC030	116	120	KK1241	753.3	45.9	71.5	0.35	0.01	0.007	50	-2.77	3.46
KKRC030	120	124	KK1242	971.8	47	71.6	0.35	0.01	0.005	20	-3.29	3.48
KKRC030	124	128	KK1243	831.5	43.6	72.3	0.23	0.01	0.015	30	-3.35	3.42
KKRC030	128	132	KK1244	726.5	43.6	72.3	0.24	0.01	0.005	20	-3.37	3.44

Hole	From m	To m	Sample	Magsus 10^{-3} SI	Mass Rec %	CON Fe %	CON Si %	CON Al %	CON S %	CON P ppm	CON LOI %	Density g/cm³
KKRC030	132	136	KK1245	648	39.6	71.6	0.41	0.01	0.006	20	-3.35	3.41
KKRC030	136	140	KK1246	853.5	45.9	72.1	0.26	0.01	0.004	20	-3.36	3.45
KKRC030	140	144	KK1247	869.3	47	72	0.3	0.01	0.004	30	-3.36	3.46
KKRC030	144	148	KK1248	854.3	45.4	72	0.32	0.01	0.01	40	-3.36	3.45
KKRC030	148	152	KK1249	339	18.5	71.8	0.62	0.05	0.007	50	-3.37	2.87
KKRC030	152	156	KK1250	808.5	40.9	72.2	0.25	0.01	0.005	30	-3.34	3.32
KKRC030	162	167	KK1251	271.6	20.6	69.6	1.33	0.02	0.954	30	-2.89	2.92
KKRC031	70	75	KK1252	325.8	20	68.8	1.93	0.04	0.049	300	-2.99	3.09
KKRC031	83	87	KK1253	154.4	10.8	62.3	4.91	0.16	0.975	250	-2.12	3.06
KKRC031	87	91	KK1254	916.5	36.1	69.3	1.59	0.01	0.056	50	-3.22	3.28
KKRC031	91	95	KK1255	1046.3	43.6	69.4	1.55	0.01	0.011	60	-3.25	3.38
KKRC031	95	99	KK1256	1071.3	41	69.7	1.92	0.01	0.008	40	-3.21	3.33
KKRC031	99	103	KK1257	1367.8	46	70.1	1.24	0.01	0.006	70	-3.25	3.45
KKRC031	103	107	KK1258	861.3	40.2	70.8	0.65	0.03	0.013	190	-3.25	3.43
KKRC031	107	110	KK1259	388.3	31.2	69.5	1.26	0.02	0.01	150	-2.96	3.24
KKRC031	120	123	KK1260	475.6	32.6	69.8	1.58	0.01	0.012	120	-3.28	3.32
KKRC031	144	150	KK1261	696.8	36.3	70.9	0.84	0.06	0.045	60	-3.27	3.31
KKRC032	78	82	KK1262	402	25.7	65.5	3.47	0.22	0.058	140	-2.9	3.26
KKRC032	82	86	KK1263	446.8	29.6	63.3	4.79	0.17	0.057	170	-2.77	3.28
KKRC032	86	90	KK1264	419.8	29.7	64.2	4.6	0.16	0.053	150	-2.91	3.18
KKRC032	90	94	KK1265	335.9	26.4	65.6	3.67	0.13	0.049	90	-2.99	3.16
KKRC032	94	98	KK1266	234.5	17.6	67.8	2.48	0.1	0.033	90	-3.14	2.9
KKRC032	98	102	KK1267	377	18.2	67.9	2.35	0.07	0.036	90	-3.14	2.94
KKRC032	102	106	KK1268	260	20.9	65	4.16	0.2	0.11	120	-2.86	3.06
KKRC032	106	110	KK1269	173.5	12.4	64.4	4.1	0.19	0.45	130	-2.64	2.81
KKRC032	110	114	KK1270	160	13.3	69.2	2.2	0.15	0.211	150	-3.09	2.79
KKRC032	114	118	KK1271	137.5	11	67.5	2.44	0.16	0.382	120	-2.87	2.84
KKRC032	118	123	KK1272	205.8	18.7	61.7	5.7	0.26	0.09	150	-2.8	2.97
KKRC033	88	91	KK1273	451.7	29.6	67.3	2.78	0.04	0.042	300	-3.05	3.18
KKRC033	98	102	KK1274	325.4	22.3	67.4	2.34	0.08	1.01	160	-2.55	3.18
KKRC033	102	106	KK1275	333.8	28.8	68.9	1.79	0.03	0.014	40	-3.25	3.08
KKRC033	106	110	KK1276	661.5	41.3	70.2	1.33	0.01	0.006	20	-3.29	3.37
KKRC033	110	114	KK1277	684.8	39.1	70.1	1.28	0.01	0.016	40	-3.26	3.29
KKRC033	114	118	KK1278	655.5	40.2	69.1	1.75	0.01	0.051	50	-3.13	3.33
KKRC033	118	122	KK1279	542.5	34	69.8	1.66	0.01	0.026	30	-3.22	3.23
KKRC033	122	126	KK1280	833.5	44.2	70.2	1	0.01	0.007	30	-3.27	3.4

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KKRC033	126	130	KK1281	615	25.6	69.2	1.79	0.04	0.019	180	-3.26	3.01
KKRC033	148	153	KK1282	231	14.6	69.9	1.38	0.01	0.07	40	-3.36	2.82
KKRC033	153	158	KK1283	179.4	12.7	70.5	0.8	0.05	0.239	50	-3.21	2.89
KKRC033	158	162	KK1284	482.8	25.2	70.3	0.94	0.03	0.029	70	-3.29	3.13
KKRC033	162	166	KK1285	734.3	35.1	70.6	0.94	0.03	0.013	70	-3.31	3.36
KKRC033	166	170	KK1286	691.5	30.5	70.4	0.84	0.01	0.016	60	-3.31	3.27
KKRC034	80	84	KK1287	340.8	17.7	68.1	2.5	0.05	0.054	100	-3.04	2.98
KKRC034	84	88	KK1288	945.5	42	70.5	1.06	0.01	0.007	30	-3.3	3.38
KKRC034	88	92	KK1289	818.5	40.8	69.6	1.39	0.01	0.009	30	-3.27	3.33
KKRC034	92	96	KK1290	707	37.7	69.3	1.66	0.01	0.008	30	-3.23	3.28
KKRC034	96	100	KK1291	920.3	46	71.4	0.8	0.01	0.007	50	-3.32	3.47
KKRC034	100	106	KK1292	669.3	41.1	69.7	1.44	0.01	0.034	140	-3.21	3.43
KKRC034	117	121	KK1293	738.3	45.2	65.3	4.17	0.01	0.015	150	-3.06	3.48
KKRC035	15	20	KK1294	36.1	15.1	65.2	3.04	0.01	0.007	140	0.22	3.06
KKRC035	20	25	KK1295	36.4	14.7	63.6	4.07	0.03	0.005	130	0.41	2.89
KKRC035	25	30	KK1296	46	18	65.9	2.56	0.01	0.009	140	0.33	3.08
KKRC035	30	34	KK1297	315.5	27.9	67.9	2.04	0.01	0.011	60	-1.24	3.27
KKRC035	34	38	KK1298	585.3	34.3	68.3	2.04	0.01	0.018	40	-2.83	3.23
KKRC035	38	42	KK1299	771.5	39.8	69.7	1.5	0.01	0.006	30	-3.09	3.3
KKRC035	42	46	KK1300	537.5	38.4	67.8	2.44	0.01	0.009	80	-2.98	3.28
KKRC035	46	49	KK1301	503	42.2	68.3	2.4	0.01	0.01	150	-2.7	3.42
KKRC035	85	90	KK1302	261.6	22	67.9	1.99	0.26	0.222	150	-3.07	3.02
KKRC035	90	94	KK1303	189.5	15.4	70.3	1.34	0.03	0.074	90	-3.25	2.96
KKRC035	94	98	KK1304	162.4	12.1	69.9	1.21	0.04	0.336	60	-3.13	2.85
KKRC035	98	102	KK1305	187	12	68.6	1.43	0.06	1.26	60	-2.54	2.92
KKRC035	102	106	KK1306	126.8	10.1	67.5	2.49	0.21	0.204	80	-3.05	2.75
KKRC036	92	96	KK1307	129.4	13.5	62.3	4.42	0.13	3.74	200	-0.98	3.08
KKRC036	96	100	KK1308	592.8	34.3	68	2.55	0.03	0.175	50	-3.08	3.19
KKRC036	100	104	KK1309	714.8	41.4	68.8	2.07	0.01	0.017	40	-3.19	3.31
KKRC036	104	108	KK1310	671.8	39.7	68.8	1.83	0.01	0.008	40	-3.2	3.29
KKRC036	108	112	KK1311	489.3	33.4	70	1.45	0.03	0.02	20	-3.22	3.18
KKRC036	112	116	KK1312	721.5	40.3	69.6	1.68	0.04	0.008	70	-3.18	3.32
KKRC036	116	119	KK1313	796.3	44.2	68.6	2.13	0.03	0.004	160	-3.13	3.43
KKRC036	156	160	KK1314	740.8	39.2	68.6	2.23	0.11	0.01	150	-3.2	3.35
KKRC037	34	39	KK1315	337.9	25.8	69.8	1.33	0.08	0.034	80	-3.25	3.11
KKRC037	39	43	KK1316	264.8	21.7	70.4	1.24	0.03	0.052	50	-3.28	3.06

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KKRC037	43	48	KK1317	385.2	27.9	70.4	1.44	0.03	0.063	80	-3.2	3.11
KKRC037	58	62	KK1318	134.9	9.5	69.3	1	0.11	0.066	50	-3.12	2.72
KKRC037	100	105	KK1319	563	35.7	71.7	0.33	0.03	0.019	20	-3.35	3.22
KKRC037	105	111	KK1320	112.8	9	71.4	0.6	0.12	0.122	50	na	2.84
KKRC038	74	79	KK1321	497.8	29.7	67.4	3.23	0.1	0.019	60	-2.93	3.13
KKRC038	79	84	KK1322	671	36.3	69.2	1.62	0.03	0.006	30	-3.22	3.26
KKRC038	87	92	KK1323	426.4	30.5	68.3	2.54	0.06	0.006	70	-3.15	3.11
KKRC038	107	111	KK1324	500.8	34.4	66.9	3.2	0.08	0.07	110	-3.06	3.22
KKRC038	111	115	KK1325	408	35.9	66	3.66	0.12	0.039	120	-2.97	3.28
KKRC038	115	118	KK1326	206.7	17.1	62.8	5.31	0.29	0.531	130	-2.56	2.97
KKRC038	118	121	KK1327	404.3	25.6	64.9	4.49	0.14	0.087	110	-3.04	3.21
KKRC039	83	87	KK1328	582.3	37.1	66.2	3.58	0.1	0.049	100	-3.07	3.24
KKRC039	87	91	KK1329	509.3	34.6	67.4	2.88	0.08	0.063	90	-3.12	3.26
KKRC039	91	95	KK1330	547	35.8	66.9	2.96	0.1	0.022	110	-3.16	3.31
KKRC039	95	99	KK1331	502.5	33.2	69.3	2.12	0.08	0.045	90	-3.2	3.26
KKRC039	99	103	KK1332	417.3	26.4	69.2	1.9	0.1	0.114	90	-3.15	3.1
KKRC039	103	107	KK1333	564.5	35.8	69.3	1.78	0.09	0.053	80	-3.18	3.28
KKRC039	107	111	KK1334	515.5	34.4	70.6	1.37	0.07	0.019	60	-3.25	3.3
KKRC039	111	115	KK1335	430.5	26.3	69.2	1.8	0.07	0.383	60	-3.02	3.09
KKRC039	115	119	KK1336	176.5	11.3	68	2.45	0.14	0.872	80	-2.67	2.81
KKRC039	129	133	KK1337	462.8	34.8	71.2	0.66	0.04	0.008	30	-3.32	3.22
KKRC039	133	137	KK1338	616.3	43.2	71.3	0.78	0.01	0.003	20	-3.32	3.4
KKRC039	140	144	KK1339	537	41.1	71.2	0.69	0.02	0.005	10	-3.35	3.33
KKRC039	144	148	KK1340	524.5	39.9	71.6	0.51	0.02	0.482	20	-3.12	3.33
KKRC039	148	152	KK1341	304	26.5	70.7	0.72	0.08	0.069	40	-3.28	3.12
KKRC039	159	164	KK1342	169.3	14.7	70.6	0.79	0.15	0.205	30	-3.14	2.98
KKRC040	25	30	KK1343	334.8	26	69.1	2.2	0.07	0.047	50	-3.13	3.04
KKRC040	30	35	KK1344	500.6	33.6	68.3	2.3	0.09	0.014	50	-3.17	3.16

JORC Code and ASX Listing Rule 5 Disclosures

Mineral Resource Estimate

Killi reports a maiden Mineral Resource Estimate for the Lodestone Iron Project comprising Inferred fresh magnetite material. The estimate has been prepared in accordance with the JORC Code (2012) and is based on geological interpretation, drilling, metallurgical test work, density determinations and estimation parameters considered appropriate for the style of mineralisation and level of data confidence.

Material Information Summary

In accordance with ASX Listing Rule 5, Killi confirms that the material assumptions and technical parameters underpinning the maiden Mineral Resource Estimate include the interpreted continuity of the mineralised BIF units, the application of Davis Tube Recovery data and associated grade relationships, the adopted density assumptions, the estimation methodology, and the current classification of fresh material as Inferred. The partly oxidised material has not been included in the Mineral Resource estimate due to lower confidence and limited sample support.

JORC Code – Checklist of Assessment and Reporting Criteria

A "Checklist of Assessment and Reporting Criteria" (a JORC Code guidelines requirement) relevant to the initial Lodestone Mineral Resource Estimate is appended to this announcement and in the supporting technical report. The Checklist includes information relating to sampling techniques, drilling, geological interpretation, data quality, metallurgical test work, density, estimation methodology, classification criteria and the basis for reporting the Mineral Resource Estimate.

Competent Persons and Consent

The relevant Competent Persons have reviewed and approved the technical information attributed to them in this announcement and have consented to its inclusion in the form and context in which it appears. Their respective responsibilities for geological interpretation, exploration information and Mineral Resource estimation are set out below.

Compliance Statement

The information in this announcement that relates to the Lodestone Iron Project maiden Mineral Resource Estimate has been prepared and reported in accordance with the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code). The supporting technical information is based on material provided by Yukon Resources Pty Ltd and in particular the "Lodestone Iron Project Resource Report" dated March 2025.

The Company confirms that it is not aware of any new information or data that materially affects the information included in the Lodestone Iron Project maiden Mineral Resource Estimate and that all material assumptions and technical parameters underpinning the estimate continue to apply and have not materially changed. The form and context in which the Competent Persons' findings are presented have not been materially modified.

Competent Person's Statement

The information in this announcement that relates to the mineral resource estimate for the Lodestone Iron Ore Project, geology, exploration results and other technical matters is based on, and fairly represents, information compiled by Dr Stuart Owen, Principal Geologist, Matakitaki Minerals Pty Ltd, who is a Member of the Australian Institute of Geoscientists. Dr Owen has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activities undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC Code, and consents to the inclusion in this announcement of the matters based on his information in the form and context in which they appear. Dr Owen does not hold any securities in the Company and does not currently receive any incentive payment dependent on the results of the Mineral Resource Estimate.

Forward Looking Statements

This ASX announcement contains certain statements that may constitute "forward looking statement". Such statements are only predictions and are subject to inherent risks and uncertainties, which could cause actual values, results, performance achievements to differ materially from those expressed, implied or projected in any forward looking statements.

Forward looking statements are statements that are not historical facts. Words such as "expect(s)", "feel(s)", "believe(s)", "will", "may", "anticipate(s)" and similar expressions are intended to identify forward-looking statements. These statements include, but are not limited to statements regarding future production, resources or reserves and exploration results. All such statements are subject to certain risks and uncertainties, many of which are difficult to predict and generally beyond the control of the Company, that could cause actual results to differ materially from those expressed in, or implied or projected by, the forward-looking information and statements.

These risks and uncertainties include, but are not limited to: (i) those relating to the interpretation of drill results, the geology, grade and continuity of mineral deposits and conclusions of economic evaluations, (ii) risks relating to possible variations in reserves, grade, planned mining dilution and ore loss, or recovery rates and changes in project parameters as plans continue to be refined, (iii) the potential for delays in exploration or development activities or the completion of feasibility studies, (iv) risks related to commodity price and foreign exchange rate fluctuations, (v) risks related to failure to obtain adequate financing on a timely basis and on acceptable terms or delays in obtaining governmental approvals or in the completion of development or construction activities, and (vi) other risks and uncertainties related to the Company's prospects, properties and business strategy. Our audience is cautioned not to place undue reliance on these forward-looking statements that speak only as of the date hereof, and we do not undertake any obligation to revise and disseminate forward-looking statements to reflect events or circumstances after the date hereof, or to reflect the occurrence of or non-occurrence of any events.

The Company believes that it has a reasonable basis for making the forward-looking Statements in the announcement based on the information contained in this and previous ASX announcements.

This announcement has been authorised for release by the Board of Killi Resources Limited.

For further information, please contact:

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Appendix A – JORC Code (2012 Edition) | Checklist of Assessment and Reporting Criteria

Section 1: Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Sampling techniques	▪ Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling. ▪ Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. ▪ Aspects of the determination of mineralisation that are Material to the Public Report. ▪ In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	▪ RC drilling; 1-m samples collected from cyclone. Rig-mounted splitter produced 2–5 kg splits per metre for direct submission. ▪ Typically, 4m composite intervals, were collected with 3-5m composite intervals used to accommodate the end of hole, were submitted for DTR and XRF fusion assay. Composites were produced on a volumetrically consistent basis using a volumetric flask. Mean composite weight was c. 3 kg.
Drilling techniques	▪ Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	▪ RC drilling, 4.5" and 5" face sampling hammer.

Drill sample recovery	▪ Method of recording and assessing core and chip sample recoveries and results assessed. ▪ Measures taken to maximise sample recovery and ensure representative nature of the samples. ▪ Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	▪ Bulk 1 m RC chip samples collected from drill rig cyclone. Sample bags routinely weighed after splitting for KKRC021–041 campaign; averaged 28 kg/m and up to 59 kg/m within fresh BIF, indicating 75–80% recovery. ▪ Rig-mounted splitter produced 2–5 kg splits per metre for direct submission. No systematic relationship between sample recovery and grade was identified. ▪ Early campaign (KKRC001–006) recovery was not formally measured but is considered representative of the face-sampling RC hammer methodology.
Logging	▪ Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. ▪ Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography. ▪ The total length and percentage of the relevant intersections logged.	▪ Logging is both qualitative and quantitative in nature. ▪ All logging completed by a suitably qualified geologist or under direct supervision of Competent Person Dr Stuart Owen. All drill holes logged for lithology, weathering, oxidation state, mineralisation and structure. ▪ Magnetic susceptibility recorded at 1 m intervals using a KT-10 meter. Total of 5,019 m (99.9%) logged across 40 RC holes to full depth. ▪ RC chip trays retained.
Subsampling techniques and sample preparation	▪ If core, whether cut or sawn and whether quarter, half or all core taken. ▪ If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry. ▪ For all sample types, the nature, quality and appropriateness of the sample preparation technique. ▪ Quality control procedures adopted for all subsampling stages to maximise representivity of samples. ▪ Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. ▪ Whether sample sizes are appropriate to the grain size of the material being sampled.	▪ Sampling via riffle splits or cone and quarter compositing. Mean composite sample weight of ~3 kg. ▪ Analytical method includes XRF fusion assay (methods XRF12 and XRF21u) and Davis Tube Recovery (“DTR”). ▪ 315 DTR composites submitted to ALS Metallurgy. Field and laboratory DTR duplicates; HRD <10% for key parameters.

Quality of assay data and laboratory tests	▪ The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. ▪ For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. ▪ Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	▪ DTR test work and assaying conducted by ALS Metallurgy, Perth. Feed and concentrate assayed by XRF fusion (methods XRF12 for KKRC001–006; XRF21u for KKRC008–041) for Fe, Si, Al, Ca, Mg, Na, K, Ti, P, Mn, S and other elements, with LOI at 1000°C (and 371°C and 650°C for XRF21u). ▪ DTR procedure: 250 g aliquots ground to P100 at target grind size (predominantly 75 µm), wet-screened, dried, and 20 g subsample subjected to Davis Tube separation at 3000–4000 gauss. Assay quality is considered appropriate and adequate for resource estimation purposes.
Verification of sampling and assaying	▪ The verification of significant intersections by either independent or alternative company personnel. ▪ The use of twinned holes. ▪ Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. ▪ Discuss any adjustment to assay data.	▪ DTR test work and assaying conducted by accredited laboratory ALS Metallurgy, Perth. Three BWI bulk composite samples (c. 30 kg each, representing North, Central and South zones) verified against down-hole DTR data with substantially comparable results. Duplicate DTR tests and field duplicates show HRD <10% for key parameters (DTR Mass Recovery, feed and concentrate Fe and Si). Database compiled in-house by Lodestone Iron and validated prior to resource estimation. No twinned holes drilled. ▪ Assay data was as supplied by ALS, no adjustment to assay data was undertaken. ▪ Mass recoveries were estimated from magnetic susceptibility for incompletely assayed holes via a DTR – magnetic susceptibility regression. <5% of the Mineral Resource Estimate magnetic recovery was derived in this way.
Location of data points	▪ Accuracy and quality of surveys used to locate drill holes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. ▪ Specification of the grid system used. ▪ Quality and adequacy of topographic control.	▪ Drill hole locations were determined by handheld GPS with a nominal accuracy of +/- 5 metres. ▪ All coordinates and maps presented here are in the MGA Zone 50 GDA94 system. ▪ Topographic control is provided by Worldwide 3 arc second SRTM spot height data. ▪ Topographic control is considered adequate.

Data spacing and distribution	▪ Data spacing for reporting of Exploration Results. ▪ Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. ▪ Whether sample compositing has been applied.	▪ The Inferred Mineral Resource represents an interpolation from data on largely 400 m drill section spacing, with 1–3 (typically 2) holes per section spaced to intersect the fresh zone iron ore mineralisation on c. 40-80 m down dip spacings, and clipped to end sections or extrapolated to half section spacing as appropriate. The MRE has been restricted the fresh magnetite zone. Drilling and geological modelling indicates continuity of the magnetite iron formation beyond the MRE which is expected to be upgraded to resource status with further drilling and metallurgical testwork. Approx 20% of the MRE is extrapolated beyond the dominant 400 m drill section spacing. ▪ Drill hole data spacing and distribution supported by magnetic surveying and geological mapping (the iron formation is extensively exposed) is considered adequate to establish the degree of geological and grade continuity for Inferred classification. ▪ 1m samples as collected from the drill rig were composited on a volumetrically consistent basis by suitably qualified Yukon Resources personnel for DTR analysis.
Orientation of data in relation to geological structure	▪ Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. ▪ If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	▪ All holes drilled at -60° plunge towards 073–098° azimuth (MGA Zone 50 GDA94). BIF zones dip 50–65° west. True thickness is generally >80% of downhole thickness. Holes drilled from the hanging wall side of the BIF. This configuration provides acceptable intersection geometry with no material sampling bias identified.
Sample security	▪ The measures taken to ensure sample security.	▪ Samples collected and managed under standard industry procedures. RC chip bags were collected directly from the cyclone and retained on the drill pad under geologist supervision. DTR composite samples were packaged and submitted directly to ALS Metallurgy, Perth under standard chain of custody. No specific sample security concerns identified.
Audits or reviews	▪ The results of any audits or reviews of sampling techniques and data.	▪ No formal external audit of the sampling program has been conducted. Internal review of sampling procedures and database integrity was carried out prior to resource estimation by the Competent Persons.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Mineral tenement and land tenure status	▪ Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. ▪ The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	▪ The reported resource is entirely within Exploration Licence 59/2163-I granted to Yukon Resources Pty Ltd on 13 May 2020. E59/2163-I currently comprises 14 graticular blocks covering approx. 67 km^2. ▪ Tenure is considered secure at the time of reporting.
Exploration done by other parties	▪ Acknowledgment and appraisal of exploration by other parties.	▪ Historical exploration by: Union Homestake Hanna Syndicate (1969) – geological mapping and base metal rock chip sampling; Reynolds Australia Metals Ltd (1991–1997) – RAB and AC drilling for Cu-Zn-Au; Sipa Resources International NL (1991–1997) – RAB, RC and DDH drilling for base metals; Lachlan Resources LN (1995) – RAB drilling; Normandy Exploration Ltd (1993–1997) – AC drilling for Cu-Zn VMS; Julia Corporation Ltd (1998) – geophysics and RAB/AC drilling for Au. First iron ore exploration within the area now covered by E59/2163-I was conducted by Black Peak Holdings Pty Ltd (BPH) in 2010–2014, work included reconnaissance RC drilling, DTR metallurgical test work and initial exploration target modelling. Yukon Resources Pty Ltd continued drill testing the magnetite iron formation following the grant of E59/2163-I in 2020. ▪ Key reference report includes the Lodestone Iron Project Resource Report (March 2025).
Geology	▪ Deposit type, geological setting and style of mineralisation.	▪ Magnetite-quartz BIF; coarsely crystalline. Mineralisation wireframes constructed in Micromine from geological and magnetic susceptibility logging, DTR and assay data.

Drill hole Information	▪ A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: – easting and northing of the drill hole collar – elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar – dip and azimuth of the hole – down hole length and interception depth – hole length. ▪ If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	▪ Within the Lodestone Project there are 40 RC holes (KKRC001–KKRC041, excluding KKRC007) totalling 5,023 m, completed across three drilling campaigns: 6 holes (KKRC001–006) in May–June 2012; 13 holes (KKRC008–020) in October 2021; 21 holes (KKRC021–041) in December 2023–January 2024. ▪ All holes inclined at -60° towards 073–098° azimuth. ▪ Average hole length 158 m (130m within the resource area); maximum 192 m. ▪ Collars located by handheld Garmin GPS (±5 m precision) in MGA Zone 50 GDA94. Down-hole gyroscope surveys conducted for KKRC008–041.
Data aggregation methods	▪ In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated. ▪ Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. ▪ The assumptions used for any reporting of metal equivalent values should be clearly stated.	▪ 4 m composites used for grade estimation (mean 4.1 m, range 2–8 m). ▪ For the MRE, IDW2 weighting applied. DTR Mass Recovery used as the primary cut-off parameter; wireframe lower threshold 15–20% for fresh zone. ▪ Grade-tonnage reported at DTR Mass Recovery cut-off values of 0, 10, 20 and 30%. ▪ No high-grade cutting applied to the dataset. ▪ No metal equivalents are reported.

Relationship between mineralisation widths and intercept lengths	▪ These relationships are particularly important in the reporting of Exploration Results. ▪ If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. ▪ If it is not known and only the downhole lengths are reported, there should be a clear statement to this effect (e.g. 'downhole length, true width not known').	▪ BIF units dip 50–65° west and strike slightly west of north; drill holes inclined at -60° east. True thickness is generally >80% of downhole thickness. All intersections reported are downhole lengths. Simple downhole compositing is considered to produce acceptable sample support given the consistent intersection geometry across the deposit.
Diagrams	▪ Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	▪ Drill hole collar plan and geological maps, drill section plots with DTR data, BIF wireframe oblique views and grade-tonnage tables have been generated and were provided as reference material to the Company. ▪ Diagrams and information provided within this report are appropriate. Refer to Figures 5 and 6 for a section view of the Mineral Resource Estimate and a plan view of all drill hole collar locations.
Balanced reporting	▪ Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	▪ All drill holes and all DTR-tested intervals within the defined mineralisation wireframes are included in the resource estimation. Both low and high DTR mass recovery intersections are represented. Grade-tonnage curves are reported at multiple cut-off grades to demonstrate the range of material quality. All results are included in Tables 8 and 9.
Other substantive exploration data	▪ Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	▪ Magnetic susceptibility data (KT-10) collected at 1 m intervals; strongly correlated with DTR mass recovery (R2 = 0.91 at 75 µm grind). ▪ Aeromagnetic imagery used to confirm BIF continuity between drill sections. Three BWI bulk composite samples tested at ALS Metallurgy confirming grindability and metallurgical performance. ▪ Fresh BIF bulk density 3.3 t/m3 (48 RC chip measurements, relative weights in air and water method). Partly oxidised BIF density 3.0 t/m3; fresh wall rocks 3.1 t/m3.

Further work	▪ The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). ▪ Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	▪ Infill RC drilling recommended on 200–400 m section spacing to upgrade resources to Indicated category. Extension drilling recommended to test 9.9 km additional BIF strike north of current MRE and 9 km south of the southernmost drill line. ▪ WHIMS test work recommended for POX zone material. ▪ Diamond core drilling recommended for bulk density, metallurgical test work validation and additional structural data. ▪ DGPS collar surveying (sub-metre precision) for future resource upgrades. ▪ Detailed magnetic surveying and detailed mapping is required to define additional parallel mineralised horizons.

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Database integrity	▪ Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. ▪ Data validation procedures used.	▪ Drillhole database compiled in-house by Yukon Resource Pty Ltd. ▪ Pre-estimation validation checks included: overlapping interval checks; downhole survey at 0 m depth validation; depth consistency between data tables; data gap checks; replacement of below-detection values with half-detection limits; missing sample intervals flagged as -999; non-assayed intervals flagged as -999.
Site visits	▪ Comment on any site visits undertaken by the Competent Person and the outcome of those visits. ▪ If no site visits have been undertaken indicate why this is the case.	▪ The Competent Persons (Dr Stuart Owen) has directly participated in exploration and resource estimation activities at the Lodestone Iron Project. Dr Owen has supervised all geological aspects of the project including drill campaigns and has made multiple site visits. Site visits confirm that the geological interpretation is consistent with the drill data and surface exposures. ▪ Killi Resources Limited personnel have completed a site visit as part of the acquisition due diligence process.
Geological interpretation	▪ Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. ▪ Nature of the data used and of any assumptions made. ▪ The effect, if any, of alternative interpretations on Mineral Resource estimation. ▪ The use of geology in guiding and controlling Mineral Resource estimation. ▪ The factors affecting continuity both of grade and geology.	▪ Iron mineralisation wireframes (to c. 190 m vertical depth) manually constructed in Micromine via sectional interpretation of drill hole logging, DTR data and magnetic susceptibility. ▪ Five BIF domains wireframed: North BIF (LFE_BIFN; ~6 km strike, 15–50 m thick), North BIF footwall zones 1 and 2 (LFE_BIFN1, LFE_BIFN2), West BIF (LFE_BIFW; ~1 km strike), and Central BIF (LFE_BIFC; ~2.6 km strike, 20–60 m thick). ▪ Each domain subdivided into fresh (FR) and partly oxidised (POX) subzones by a Top of Fresh (TOF) wireframe. ▪ BIF geometry is relatively simple and predictable; continuity strongly supported by magnetic imagery. ▪ Alternative geological interpretations would not materially change the resource estimate.
Dimensions	▪ The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	▪ Total modelled BIF strike length: 9 km (North BIF ~6 km; Central BIF ~2.6 km; West BIF ~1 km). BIF true thickness: North BIF 15–50 m; Central BIF 20–60 m; West BIF 10–30 m. Maximum vertical depth modelled: c. 190 m (maximum drill depth c. 170 m below surface). Deposit is open along strike to the north and south beyond the current MRE boundary.
Estimation and	▪ The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade	▪ IDW2 estimation in Micromine on 4-m composite data. ▪ Three estimation domains (Main Fresh, POX, Secondary Fresh).

modelling techniques	values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used. ▪ The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data. ▪ The assumptions made regarding recovery of by-products. ▪ Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation). ▪ In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed. ▪ Any assumptions behind modelling of selective mining units. ▪ Any assumptions about correlation between variables. ▪ Description of how the geological interpretation was used to control the resource estimates. ▪ Discussion of basis for using or not using grade cutting or capping. ▪ The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.	▪ Estimation techniques are considered appropriate for the current broadly spaced drill hole pattern, the style of mineralisation and the level of geological and metallurgical understanding.
Moisture	▪ Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	▪ LOI has been required for the DTR samples ▪ Tonnages estimated on a dry basis. No moisture content determination conducted. ▪ Fresh BIF is a strongly crystalline, non-porous rock; negligible moisture content is assumed. ▪ Partly oxidised material (POX) does not form part of the Mineral Resource estimate and moisture effects are not material at this stage.
Cut-off parameters	▪ The basis of the adopted cut-off grade(s) or quality parameters applied.	▪ DTR Mass Recovery (%) used as the primary cut-off/quality parameter, reflecting the standard industry approach for magnetite reporting. Resource reported at DTR Mass Recovery cut-off values of 0%, 10%, 20% and 30% to demonstrate sensitivity.

		▪ A 25% DTR Mass Recovery cut-off is considered appropriate as a reasonable proxy for economic viability based on comparable magnetite projects. No formal economic study has been completed.
Mining factors or assumptions	▪ Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	▪ Open pit mining assumed based on deposit geometry (near-surface, tabular, steeply dipping BIF). Minimum mining dimensions and dilution have not been formally assessed at this stage (Inferred resource). The deposit has reasonable prospects for eventual economic extraction based on: – proximity to the operating Karara magnetite mine (~25 km east) and associated infrastructure including rail to Geraldton port; – high-quality magnetite concentrate (>65% Fe) producible at coarse grind; – scale of resource.
Metallurgical factors or assumptions	▪ The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	▪ Davis Tube Recovery (DTR) test work at 75 µm grind used as primary metallurgical indicator. High-quality magnetite concentrate (>65% Fe, typically 68–70% Fe) producible at the 25% DTR MR cut-off. ▪ Silica is the only significant impurity (c. 3.9% SiO_2 at 25% cut-off); all other impurity elements are at low levels. ▪ Bond Work Index tests completed on three bulk composites. ▪ Magnetite grain size increases south, with DTR concentrates >70% Fe achieved readily in the central-southern zones. ▪ Further test work (pilot scale, WHIMS for POX) recommended prior to feasibility studies.
Environmental factors or assumptions	▪ Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	▪ The project is at an exploration and resource definition stage and no formal environmental impact assessment has been completed. ▪ The southern portion of the tenement lies within a DBCA-administered Timber Reserve; a targeted flora and fauna survey has been conducted for Yukon Resources by Ecoscape (Australia) Pty Ltd and a Reserve Activity Management Plan has been submitted to DBCA for drill testing of the Lodestone magnetite iron formation over a strike length of c. 9 km on 200m spaced drill lines with associated access tracks. ▪ No significant environmental constraints are known for the northern and central project areas. Standard rehabilitation of drill pads completed following each campaign.

Bulk density	▪ Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. ▪ The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit. ▪ Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	▪ Some 88 fresh RC chips tested by relative weights in air and water. Mean fresh BIF density 3.3 t/m³; 3.2 t/m³ used in MRE. Fresh Country Rock = 2.80 t/m³.
Classification	▪ The basis for the classification of the Mineral Resources into varying confidence categories. ▪ Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). ▪ Whether the result appropriately reflects the Competent Person's view of the deposit.	▪ The resource classifications have been applied based on consideration of the confidence in the geological interpretation, the quality and quantity of the input data, the confidence in the estimation technique, and the likely economic viability of the material. ▪ Inferred JORC Category: Fresh BIF domains supported by drill data, outcrop and magnetic data. ▪ The partly oxidised (POX) zone does not currently form part of the Mineral Resource estimate due to insufficient sample and metallurgical support.
Audits or reviews	▪ The results of any audits or reviews of Mineral Resource estimates.	▪ Model validated by comparison of block grades against composite means and visual review of sections and plans.
Discussion of relative accuracy/confidence	▪ Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. ▪ The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be	▪ Resource classified as Inferred based on current drill spacing of 400 m between sections. IDW2 global estimates validated by comparison of block grades against composite means and visual review of sections and plans; sensitivity to IDW2 parameters is low. ▪ Omnidirectional variogram range of 25 m (48% nugget) established for main domain (Domain 1). Inferred classification is appropriate given sparse drill spacing and is supported by strong BIF geological continuity confirmed by magnetic data, outcrop expression and consistent DTR results. ▪ The partly oxidised (POX) zone does not currently form part of the Mineral Resource estimate due to insufficient sample and metallurgical testwork support. ▪ Further drilling will be required to upgrade resources to Indicated or higher categories.

relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.

- These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.

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